#### SLAMM MODEL CALIBRATION AND EXAMPLE APPLICATION PROJECT

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## PREPARED FOR: WISCONSIN DEPARTMENT OF NATURAL RESOURCES MADISON, WISCONSIN

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#### Introduction

#### 1.1 PURPOSE

The Stormwater Loading and Management Model (SLAMM) was developed to provide a means for predicting urban watershed runoff and non-point source pollutant loadings and to evaluate various stormwater quality management options. The purpose of this project was to re-calibrate portions of the SLAMM model using existing and newly-collected data and to provide example applications of the model to watersheds typical of those requiring stormwater management decisions. This effort was part of a larger overall stormwater quality management assessment of both groundwater pollution associated with the infiltration of urban stormwater and the source identification of pollutants in urban runoff conducted by the Wisconsin Department of Natural Resources (WDNR).

#### 1.2 SCOPE OF WORK

The scope of work for this project was essentially as described in the Warzyn proposal to DNR dated April 10, 1991. The project activities were divided into three general phases: sub-basin data review and verification, SLAMM model calibration, and use of the calibrated model in example applications to Milwaukee area sub-basins. Work was conducted over the period of June through December, 1991 at Warzyn's Madison, Wisconsin Office. The scope of work included frequent meetings, discussion and data exchanges with WDNR personnel, and, to a lesser extent, with personnel of the U.S. Geological Survey Water Resource Division (USGS), Madison, Wisconsin office.

The original scope of work called for calibration of the SLAMM model for runoff, total suspended solids, and copper and zinc loading rates. However, WDNR later requested that the zinc loading rate be deleted from the analysis due to various problems with the available analytical data. In addition, the original scope of work called for preparation of separate memoranda on each of the three main phases of project activity. The Phase I memorandum was issued on November 13, 1991. As agreed to by WDNR, this final report includes the content of the Phase I Memorandum, and provides a full reporting of the three phases of project activity.

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#### THE STORMWATER LOADING AND MANAGEMENT MODEL

#### 2.1 GENERAL DESCRIPTION

The SLAMM model was developed by Robert Pitt, formerly of the WDNR and currently an Assistant Professor in the Department of Civil Engineering at the University of Alabama in Birmingham. The model was developed to aid in the analysis of the effects of land use and stormwater management on urban runoff quality and quantity. The model requires that the urban watershed be described in terms of specified land uses and source areas. It then calculates total pollutant loadings from each area, and provides maximum, minimum, and average values for those areas. This information can be used to pinpoint critical nonpoint pollution sources.

By using typical land use data, estimates of pollutant loadings can be developed if no pollution control practices are used. The analyst can then apply different control practices to different source areas. From this information, the analyst can determine control practice effects on loading and runoff quantities, and alter specific control practice designs. A control practice design may be analyzed as a retrofit in an established area or as a new practice to reduce pollutants coming from developing areas.

A summary of the Land Use Categories, Source Area Characteristics, Pollution Control Practices and Stormwater Quality Parameters applied in the SLAMM model is presented below:

1. Land Uses:

Residential

Institutional

Commercial

Industrial

Open Spaces

Freeways

2. Source Areas:

Roofs

Undeveloped Areas

Paved Parking/Storage

Small Landscaped Areas · Other Pervious Areas

Unpaved Parking/Storage Playgrounds

Other Areas

Driveways

Freeway Lanes/Shoulders

- · Sidewalks/Walks
- · Streets/Alleys
- · Large Turf Areas
- · Large Landscaped Areas

#### 3. Pollution Control Practices:

- Detention Ponds
- · Infiltration Devices
- · Catchbasin Cleaning
- · Roof Disconnections
- Porous Pavement
- Street Cleaning
- · Grass Swales
- · Paved Area Disconnections

#### 4. Stormwater Quality Parameters:

- · Storm Runoff Volume
- Total Suspended Solids loading
- Dissolved and particle. adsorbed loading of contaminants such as Cu, Zn, BOD, or phosphorus

SLAMM allows the model user to apply runoff and pollutant data from urban non-point studies to determine loadings. To predict runoff, the model uses a series of storm rainfall/runoff coefficients specific to source area types. The model uses a series of particulate solids coefficients to predict solids loadings based upon land use, source area type, and rainfall depth. SLAMM then determines dissolved and adsorbed pollutant loadings from the total runoff runoff volume, total solids loading, and from pollutant concentrations which depend on land use and source area. Pollution control practices are modeled using algorithms which describe how a control practice functions. These algorithms reduce the suspended solids and pollutant loading predictions, based upon the specified control practice. SLAMM model documentation is maintained by WDNR (WDNR, 1989a, b) and by Robert Pitt (Pitt, 1989).

#### 2.2 MODIFICATIONS TO THE SLAMM MODEL

Earlier efforts by WDNR to calibrate the SLAMM Model were only partly successful. Part of this difficulty was due to errors in several sub-basin input data files. However, an additional source of the earlier calibration difficulty, discovered during this project, consisted of a problem in the SLAMM Model data input routines. One subroutine in the data input portion of the model was designed to adjust street pollutant loading coefficients if the street characteristics were changed. However, portions of this subroutine did not operate as originally designed, and street loading coefficients were not changed automatically with changes in street description data input. This error was detected and corrected

soon after project work began. The SLAMM model included with this project report includes this street loading coefficients input routine correction.

#### 2.3 SLAMM MODEL UTILIZATION

The executable code for the the corrected (See Section 2.2) SLAMM Model (designated version 5.3) is included in the diskette contained in Appendix E. Also included in Appendix E are the calibrated pollutant coefficient files as well as study area data files for all study area sub-basins used in this analysis.

The SLAMM Model is designed for use under MSDOS operating systems. A math coprocessor is recommended for prompt model operation.

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# Model Input And Calibration Data Review And Verification

#### 3.1 CALIBRATION SUB-BASIN DESCRIPTION

A total of ten urban study area data sets from southern Wisconsin were used to calibrate the SLAMM model. Six of the study area sub-basins were located in the Milwaukee urban area, and were investigated and sampled as part of EPA's National Urban Runoff Program (NURP) urban stormwater study during the years 1980 - 1982. Two of the Milwaukee NURP sub-basins were resampled by WDNR and the USGS in 1990 to create additional study area data sets. In addition, WDNR and the USGS conducted sampling programs for two sub-basins in Madison, Wisconsin during 1991. The general characteristics of the sub-basins and data used in calibration is summarized in Table 1. The drawings in Appendix D, supplied by USGS, illustrate the layout of each study area.

The sub-basin areas range in size from approximately 12 to 250 acres, and include residential, commercial and industrial areas. Most of the sub-basins included some type of street sweeping and/or regular catch basin maintenance, but included no other stormwater management practices or facilities.

Data collection for the 1980-1982 Milwaukee NURP study areas is documented in the general NURP Project Report (U.S. EPA, 1983). The NURP sub-basin data supplied for this project by WDNR included runoff, suspended solids and metals data from 40 to 80 storm events. The NURP data was collected at a single sub-basin outlet point, so the data represents a combination of the responses from the various land uses and source areas within the study area. The 1990 restudies of two of the NURP area sub-basins, the Hastings and Wood Center study areas, provided data for an additional 13 and 19 storm events, respectively. The WDNR 1991 sampling of the Monroe Street and Syene Road study areas in the Madison, Wisconsin area included both whole sub-basin and some source area water quality sampling. The study area instrumentation and data collection program conducted

by WDNR during 1990 and 1991 is being reported separately as part of the overall WDNR-sponsored project.

#### 3.2 DEVELOPMENT AND VERIFICATION OF STUDY AREA DATA

The first phase of the project was an evaluation of the format and completeness of the data used to calibrate SLAMM. The evaluation included a review of the data for consistency and applicability to the model calibration process, Milwaukee and Madison site visits, and modifications to the model input data files to accurately reflect site conditions. The calibration data file creation/correction process was done in two concurrent steps. One step included site visits to Milwaukee to more accurately characterize certain sections of those sub-basins. The second step was to re-measure source areas at each Site from blueprints of original aerial photographs. New site files were created from the areal and site characterization data developed from these two steps.

The Milwaukee-area site visits were performed by Warzyn and WDNR personnel to characterize site drainage connections for rooftops and driveways. The four sites which contained residential land uses were inspected to evaluate the percentage of rooftops and (for the Hastings and Burbank sites only), driveways which were disconnected from the storm drainage system. A fraction of a driveway or a rooftop was defined as disconnected if it drained to a pervious area. The results of the survey are included in Table 2, and were used to modify the site data input files. Because of the difficulty in evaluating the fraction of disconnected sidewalks, it was assumed that 50% of the sidewalks drained to pervious areas. Area calculations for source areas from each Milwaukee area site were obtained from digitized 1"=100' aerial photos by USGS personnel.

Surveys of the Syene Road site were also performed by Warzyn and WDNR personnel. These surveys included basin area delineation and site drainage connection characterizations. Monroe Street site surveys were performed by WDNR personnel. USGS personnel digitized the source areas for both sites.

The SLAMM site description input data files were developed using source area and impervious area connection data, supplemented with other site characterization information. This information include soil type, street characteristics, industrial and commercial rooftop drainage system connections, and catchbasin and delivery system characteristics. Site description data files for the Madison and Milwaukee area sites were initially developed by WDNR and USGS staff, and were then reviewed and modified where necessary and appropriate by Warzyn and WDNR.

Calibration sub-basin input data files used for SLAMM model calibration for each of the eight calibration study areas is described in the model input files listed in Appendix A.

#### 3.3 RAINFALL DATA

Rainfall data sets for use with the source area description files in the SLAMM model were supplied by WDNR. The data consisted of separate storm duration/rainfall depth files for each of the calibration study areas. The storm rainfall depths were obtained from rainfall gages located within each sub-basin. The storm rainfall data files were reviewed for format and consistency, but were not checked against external data sources as part of this project. Rainfall data collection procedures for the NURP study are described in the overall project report (WDNR, 1983). Rainfall data collection procedures for the 1990 Milwaukee and 1991 Madison area WDNR projects are available from WDNR, and are in the process of being documented. The rainfall data files used in this study are included on the diskette in Appendix D.

#### 3.4 SUB-BASIN RUNOFF, SUSPENDED SOLIDS AND COPPER LOADING DATA

Collected data from the calibration sub-basin sites was provided to Warzyn by WDNR. The Milwaukee NURP (1980-1982) data on runoff volume and suspended solids was taken from EPA project report data summaries. This data consisted of sub-basin outfall samples only. The 1990 restudy data for the Burbank and Wood Center NURP sites also described whole sub-basin runoff and suspended solids data. These 1980-1982 and 1990 data sets represented wholestorm runoff volume and flow-composite suspended solids data. The procedures for data collection and analysis for the 1980-1982 NURP studies is available (WDNR, 1983), and the procedures for the 1990 re-study is available from WDNR.

Data for the 1991 study of the Monroe Street and Syene Road sites was provided by WDNR and USGS. The 1991 study collected both sub-basin outlet and source area data. Sub-basin outlet data was collected on a flow-proportional basis. Source area data was collected by using several techniques. Documentation of these data collection and analytical procedures is being prepared by WDNR.

The collected whole sub-basin runoff volume, suspended solids and copper loading data for each watershed are included in the detailed calibration spreadsheet listings presented in Appendix B.

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#### SLAMM MODEL CALIBRATION

#### 4.1 CALIBRATION PROCEDURE

#### 4.1.1 General Approach

All available data from the 1980-1982 NURP study, from the WDNR-USGS studies of 1990 (for Hastings and Wood Center) in Milwaukee, and the 1991 data for Monroe Street and Syene Road were used in the SLAMM calibration process. Due to the relatively small size of the data sets, they were not divided to permit a verification analysis.

The general approach to calibration was to start with data sets dominated by one source area and land use. Runoff volume was the first parameter to be calibrated, and was followed by suspended solids and, finally, copper. The objective of the calibration process was to reproduce the total (multi-storm) loading as closely as possible, rather than model the range of loadings associated with the largest or smallest storms in the data set. Summary data describing the accuracy of model calibrations for runoff and suspended solids is contained in Table 3, and for copper loading, in Table 4.

The calibration data sets did not include every possible combination of land use and source area. For this reason, only a portion of the runoff, suspended solids and copper loading portions of the SLAMM model were calibrated. The source areas and land use categories which were calibrated are specified in Tables 5, 6 and 7 for runoff, suspended solids and copper loading, respectively.

More detailed descriptions of the calibration procedures are presented in Sections 4.1.2 through 4.1.4, and detailed descriptions of calibration results for each calibration study area presented in Section 4.2.

#### 4.1.2 Runoff Calibration

To predict runoff, SLAMM assumes that runoff is an incrementally linear function of rain depth, for various runoff source areas. Runoff depth is calculated as a specified fraction of rainfall, with the fraction varying by rainfall depth. A total of seventeen rainfall-runoff fractions are used in the model over the rainfall range 0.0 in. to 4.7+ in. The calibration file to predict runoff was developed by determining from the data, for the nine specific source areas and three drainage

area modifiers listed in Table 5, what fraction of rainfall becomes runoff for a given rainfall depth. These fractions, or runoff coefficients, were entered in the runoff coefficient file. The model was then run with the runoff coefficient file, and the resulting model output compared with the observed data. If the residual runoff totals (observed value less predicted value) were large, modifications were made to the runoff coefficient file, the model was re-run and the results reviewed again. This process continued until the results could not be improved upon, or until no additional changes could be made to runoff coefficients without altering previously established coefficients. The final set of event-by-event comparisons for each site can be found in Appendix B. The final runoff coefficient file, MILW00.RSV, is listed in Appendix A and is included on the diskette in Appendix E.

#### 4.1.3 Suspended Solids Calibration

The process used in calibrating suspended solids was similar to the process used for runoff depth. As with runoff, SLAMM assumes that suspended solids concentrations are an incremental linear function of rain depth, source area, and, for suspended solids, land use. The initial calibration file used to predict suspended solids loadings was developed from collected data by determining, for the specified source areas and land uses listed in Table 6, the average suspended solids concentration for a source area in a land use, by rainfall depth. These particulate solids concentrations were entered in the particulate solids concentration file. The model was then run and the resulting output compared with the observed data. The primary calibration criteria was to reproduce the suspended solids loading for the entire data record, as described above. If the residual loading totals were large, then additional modifications were made to the particulate runoff concentration file, the model re-run and the results reviewed. The closure criteria was similar to that for runoff. This process continued until the results could not be substantially improved or until no additional changes could be made to particulate solids concentration values without altering previously established values. The final set of event-by-event comparisons for each site can be found in Appendix B. The final particulate solids concentrations file, MILW00.PSC, is listed in Appendix A and is included on the diskette in Appendix E.

The delivery parameter file is used to predict the reduction in suspended solids loading between the source areas and the outfall which occurs primarily during smaller rainfall events. The model assumes that the efficiency with which the drainage system delivers suspended solids to the outfall is a function of rain depth and the overall delivery system slope and roughness. The final delivery particulate reduction file, MILW00.PRR, was developed to allow the model to reproduce as closely as possible the total suspended solids loading from the study areas. The original pre-calibration delivery file, DELIVERY.PRR, is also

included on the disk in Appendix E for informational purposes. Use of the parameters in the original file DELIVERY.PRR results in slight under-prediction of total suspended solids loading, compared to MILW00.PRR. The final particulate delivery reduction file, MILW00.PRR is listed in Appendix A and is included on the diskette in Appendix E.

#### 4.1.4 Copper Loading Calibration

To predict loading from other contaminants (such as copper), SLAMM assumes that these contaminants are released in two phases: a particulate-adsorbed phase, and a dissolved phase. The particulate-adsorbed phase loading is calculated as a specified fraction of the total suspended solids loading, and the dissolved phase as a concentration value. The calibration file to predict these loadings is developed by determining, for the specified source areas and land uses listed in Table 7, the average concentration values by source area for both the particulate and the dissolved (or filterable) form of the pollutant. Copper data was available for only the Monroe Street and Syene Road sites for only a few storm events (see Table 1). For dissolved copper, the geometric mean of individual storm source area dissolved copper values was entered into the pollutant value parameter file for each available source area. For particulate copper, the geometric mean of the ratio of particulate copper to suspended solids for all storms was entered into the pollutant value parameter file for each available source area. After the initial model run, modifications were made only to parameters developed from the Monroe Street data.

#### 4.2 Calibration Results

#### 4.2.1 Summary of Results

Overall, the SLAMM model was calibrated to accurately reproduce the collected data on a total loading basis: Figures 1, 2 and 3 illustrate the accuracy of observed vs. modeled results for runoff volume, suspended solids loading, and total copper loading.

The total predicted runoff from the six Milwaukee 1980-1982 NURP sites and the Monroe Street site were within 15 percent of the observed total runoff and usually less than 10 percent. The model underpredicted the Syene Road industrial site total runoff by 28%.

The predicted total suspended solids loading from the six Milwaukee sites was, except for the Rustler commercial study area, within 20% of the observed values before outliers were removed. After selected outliers were removed, the predicted value for all six study areas except for the Burbank residential site was within 10% of the observed value. The predicted total suspended solids loading for the

two Madison study areas were within 10% of the observed values. The following discussion summarizes the calibration results for each site.

The predicted total copper loading was, for the residential Monroe Street study area, within 1% of the observed total copper loading. The model predicted the total copper loading for the commercial Syene Road study area to within 11% of the observed loading.

#### 4.2.2 Summary Table Presentation Format

The results of the SLAMM model calibration for each site are summarized in Tables 3 and 4. Table 3 first lists the number of rainfall/suspended solids events recorded at each site and the average depth and the coefficient of variation of the rainfall events for each site. The rainfall information is included to allow the reader to qualitatively compare the average rainfall depth to the average runoff depth.

The next three columns in Table 3 summarize the runoff statistics of total depth, average depth, and the coefficient of variation for each site. Both the observed and the predicted values are listed. The comparison between the observed and predicted values is illustrated by both the residual value and the percent difference between the observed and predicted value. The suspended solids loadings, which are listed in the final three columns, are described in a similar manner.

The statistics in Table 3 are presented for the site data, with and without outliers. Outliers for the 1980 to 1982 NURP data from Milwaukee were selected, by inspection, if the residual was large. Outliers for the 1990 Milwaukee data from Hastings and Wood Center, and the Monroe Street and Syene Road data, were defined by a residual value to observed value ratio greater than 4.0. By this definition, there were no residuals for the Syene Road data.

Table 4 summarizes the results of the copper calibrations for the Monroe Street and Syene Road study areas. These tables list the number of events recorded at each study area and compares the observed and predicted results for total copper, dissolved copper, and particulate copper at each study area.

#### 4.2.3 Post Office Study Area

The post office data set is the largest of the data sets. The average runoff depth was 91% of the average rainfall depth. The percent difference between the observed and predicted runoff total depth and the runoff average depth was 2% for both the entire Post Office data set and the data set less one outlier, indicating that the outlier did not affect model runoff prediction. The coefficient of variation for both sets of runoff data were virtually identical.

The percent difference between the observed and predicted suspended solids total values and the average suspended solids values was 11%. This was reduced to 0% after the one outlier was removed because predicted suspended solids for paved areas (the only Post Office source area) were calibrated to exactly match the observed values once the outlier was removed from the data set. The coefficients of variation for the suspended solids data sets after the outlier was removed were virtually identical.

#### 4.2.4 Rustler Study Area

The Rustler data set, which had paved parking and flat roof commercial source areas, contained 68 runoff values and 67 suspended solids values. The average runoff depth was 87% of the average rainfall depth. The percent difference between the observed and predicted runoff total depth and the runoff average depth was 0% for all data, and 1% for the data set less two outliers, indicating that the outliers did not affect model runoff prediction. The coefficient of variation for both sets of runoff data were virtually identical.

The percent difference between the observed and predicted suspended solids total values and the average suspended solids values for all data was 24%. This was reduced to 4% after two outliers were removed. The coefficient of variation for the observed data set was greater than the predicted value coefficient of variation, indicating that there was greater scatter in the observed data than in the predicted data.

#### 4.2.5 Hastings Study Area, 1980-1982 Data

The 1980 to 1982 Hastings data set, which has source areas associated with residential land uses, contained 44 runoff and suspended solids values. The average runoff depth was 37% of the average rainfall depth. The percent difference between the observed and predicted runoff total depth and the runoff average depth was 7% and 9% respectively, for all data, and 8% and 9% respectively for the data set less one outliers indicating that the outlier only slightly affected model runoff prediction. The coefficient of variation for both sets of runoff data were similar.

The percent difference between the observed and predicted suspended solids total values and the average suspended solids values for all data was 18%. This was reduced to 3% and 2%, respectively, after one outlier was removed. The coefficient of variation for the observed data set was greater than the predicted value coefficient of variation, indicating that there was greater scatter in the observed data than in the predicted data.

#### 4.2.6 Burbank Study Area

The Burbank data set, which has source areas associated with residential land uses, contained 51 runoff and suspended solids values. The average runoff depth was 36% of the average rainfall depth. The percent difference between the observed and predicted runoff total depth and the runoff average depth was 9% and 8% respectively, for all data, and 8% and 6% respectively for the data set less three outliers, indicating that the outliers only slightly affected model runoff prediction. The coefficient of variation for both sets of runoff data were similar.

The model underpredicted the suspended solids total values and the average suspended solids values for all data by 11%, and overpredicted the total and average values by 37% after the three outliers were removed. The coefficient of variation for the observed data set was greater than the predicted value coefficient of variation, indicating that there was greater scatter in the observed data than in the predicted data.

#### 4.2.7 State Fair Study Area

The State Fair data set, which has source areas associated with residential and commercial land uses, contained 46 runoff and suspended solids values. The average runoff depth was 67% of the average rainfall depth. The percent difference between the observed and predicted runoff total depth and the runoff average depth was 9% and 10% respectively, for all data, and 8% and 7% respectively for the data set less one outlier, indicating that the outlier only slightly affected model runoff prediction. The coefficient of variation for both sets of runoff data were similar.

The model underpredicted the suspended solids total values and the average suspended solids values for all data by 4%, and overpredicted the total and average values by 9% after the outlier was removed. The coefficient of variation for the observed data set was greater than the predicted value coefficient of variation, indicating that there was greater scatter in the observed data than in the predicted data.

#### 4.2.8 Wood Center Study Area, 1980-1982 Data

The Wood Center data set, which has source areas associated with residential, commercial, and industrial land uses, contained 61 runoff and suspended solids values. The average runoff depth was 80% of the average rainfall depth. The percent difference between the observed and predicted runoff total depth and the runoff average depth was 15% and 14% respectively, for all data, and 15% and 13% respectively for the data set less two outliers, indicating that the outliers only slightly affected model runoff prediction. The coefficient of variation for both sets of runoff data were virtually identical.

The model underpredicted the suspended solids total values and the average suspended solids values for all data by 16%, and nearly matched the observed total and average values after the two outliers were removed. The coefficient of variation for the observed data set was greater than the predicted value coefficient of variation, indicating that there was greater scatter in the observed data than in the predicted data.

#### 4.2.9 Hastings Study Area, 1990 Data

The 1990 Hastings data set, which has source areas identical to the 1980-1982 data set, contained 13 runoff and suspended solids values. The average observed runoff depth was 48% of the observed average rainfall depth, 11% more than the runoff-to-rain ratio found in the 1980-1982 Hastings data set. The model underpredicted the total and average runoff depths by 28% and 29% respectively, for all data, and 3% and 5% respectively for the data set less two outliers. This indicated that the outliers had an effect on model runoff prediction. The difference between the coefficient of variation for the complete data set was 0.40, while the difference between the coefficient of variation for the data set less outliers was 0.04, indicating that the outliers had a considerable affect upon the data scatter. This is to be expected in a small data set.

The model underpredicted the suspended solids total values and the average suspended solids values for all data by 61%, and overpredicted the suspended solids values by 15% after the two outliers were removed. The coefficient of variation for the observed data set was greater than the predicted value coefficient of variation for both the full and truncated data sets, indicating that there was greater scatter in the observed data than in the predicted data.

#### 4.2.10 Wood Center Study Area, 1990 Data

The 1990 Wood Center data set, which has source areas identical to the 1980-1982 data set, contained 19 runoff and 16 suspended solids values. The average observed runoff depth was 54% of the observed average rainfall depth, 6% more than the runoff-to-rain ratio found in the 1980-1982 Wood Center data set. The model overpredicted the total and average runoff depths by 27% for all data, and 24% and 26% respectively for the data set less four outliers. This indicated that the outliers had little effect on model runoff prediction. The difference between the coefficient of variation for the complete data set less outliers was 0.08, indicating that the outliers had little affect upon the scatter of the data.

The model overpredicted the suspended solids total values and the average suspended solids values for all data by 22%, and underpredicted the suspended solids values by 5% after the four outliers were removed. The coefficient of variation for the observed data set was greater than the predicted value coefficient

of variation for both the full and truncated data sets, indicating that there was greater scatter in the observed data than in the predicted data.

#### 4.2.11 Monroe Street Study Area

The Monroe Street data set contained 10 runoff and 8 suspended solids values. The average observed runoff depth was 12% of the observed average rainfall depth. The model overpredicted the total and average runoff depths by 20% and 25% respectively for all data, and 15% and 0% respectively for the data set less one outlier. This indicated that the outlier had some effect on model runoff prediction. The coefficient of variation for the observed values was similar to the predicted value coefficient of variation for both the complete data set and the truncated data set. This indicated that the predicted runoff scatter was similar to the observed runoff scatter for both the complete data set and the truncated data set.

The model overpredicted the suspended solids total values and the average suspended solids values for all data by 4% and underpredicted the suspended solids values by 9% after the outlier was removed. The coefficient of variation for the observed data set was greater than the predicted value coefficient of variation for both the full and truncated data sets, indicating that there was greater scatter in the observed data than in the predicted data.

The calibrated model nearly exactly reproduced the observed total copper loading for Monroe Street. The calibrated model slightly over-predicted the dissolved copper loading and slightly under-predicted the particulate copper loading. A complete listing of the copper calibration results at the outfall is included in Appendix B.

#### 4.2.12 Syene Road Study Area

The Syene Road data set contained 11 runoff and suspended solids values. The average observed runoff depth was 68% of the observed average rainfall depth. The model underpredicted the total and average runoff depths by 28% and 27% respectively for all data. The coefficient of variation for the observed values was similar to the predicted coefficient of variation for the complete data set, indicating that the predicted runoff scatter was similar to the observed runoff scatter. No outliers were removed from this data set.

The model overpredicted the suspended solids total values and the average suspended solids values for all data by 8%. The coefficient of variation for the observed data set was somewhat greater than the predicted coefficient of variation, indicating that there was greater scatter in the observed data than in the predicted data.

The calibrated model over-predicted the total copper loading at the Syene Road study area by 11% overall, with over-prediction of dissolved copper loading by 21% and over-prediction of particulate copper loading by 5%. A complete listing of the copper calibration results at the outfall is included in Appendix B.

[mad-603-34d]

#### SLAMM MODEL

#### **EXAMPLE APPLICATION**

#### 5.1 OBJECTIVE AND PROCEDURE

The example application of the calibrated SLAMM model is intended to illustrate the use and output of the model, and also to illustrate several of the significant features of stormwater runoff quality using the model output. The test sub-basins were drawn from the same geographic area as the calibration data, and also incorporated many of the land uses and source areas which were calibrated in this project.

The input data for the example applications was generated by WDNR, using available land use, soils and mapping/aerial photography data. The input data files were run using the calibrated model by WDNR and Warzyn, and are presented below with a discussion of results.

#### 5.2 EXAMPLE SUB-BASIN DESCRIPTION

Two example sub-basins in the Menomonee River sub-basin were selected by WDNR to provide demonstration applications for SLAMM. These sub-basins are located in the Lilly Creek sub-basin of the Menomonee River watershed, which is located in the Village of Menomonee Falls near the Milwaukee County - Waukesha County border in southeastern Wisconsin. The Lilly Creek sub-basin has a drainage area of approximately six square miles, of which approximately 50% has undergone some form of development.

The two example sub-basins were labeled as LILLYC and LILLYG for use in the model. LILLYC is a 207 acre mixed-land use sub-basin consisting of approximately 44% residential, 6% commercial, 36% industrial, and 14% open space land uses. LILLYG is a 67 acre residential land use sub-basin.

#### 5.3 SLAMM MODEL INPUT

The source areas within each land use were determined by applying land use description base files to measured land use areas for each sub-basin. These files are based upon average source area characteristics for each land use which were developed by WDNR, and contain average fractional unit-area and other source area-specific information needed to create SLAMM site description data files. These source area fractional unit-area values for each land use are multiplied by the measured areas and entered into a site description file for the sub-basin. The two site description files are included in Appendix C, and electronic copies are also included on the diskette in Appendix E.

The rainfall data used in conjunction with the site description file for the demonstration model runs is developed from rainfall data from 1981 collected at Mitchell Field in Milwaukee. This rainfall data file is included in the diskette in Appendix E.

#### 5.4 RESULTS OF EXAMPLE APPLICATION

The application of the SLAMM model to the two sub-basins results in predictions of total runoff, suspended solids loading and copper loading from the sub-basins, as summarized in Table 8. This table indicates one of the primary uses of the model: direct prediction of stormwater pollutant loading rates to sub-basin steams. The loading rates presented in Table 8 would used in the decision-making process to promote particular retrofit or future development area stormwater management practice strategies. The model output for all source areas for each example application is included in Appendix C.

The model output also illustrates several important features typical of urban stormwater, as illustrated in Figures 4 and 5. These figures illustrate that, for both sub-basins, the following are dominant features of stormwater quality:

- Previous areas such as lawns are a large fraction of the sub-basin area, but produce very low suspended solids and copper loading.
- Street areas dominate in the production of pollutants, substantially in excess of their percentage of area in the sub-basins.
- Roof areas (and, to some extent, parking areas) produce substantial runoff, but much lower suspended solids and copper loading than street areas.

[mad-603-34e]

#### Conclusions

#### 6.1 SLAMM MODEL ACCURACY

The SLAMM Model, as calibrated in this study, was generally accurate in reproducing collected data from the ten sub-basin study areas. Runoff depth data was reproduced to within 15% of the observed-data for all study area sub-basins. The modeled total suspended solids loading was generally within 20% of observed data. Modeled total copper loading for the observed storms for the Syene Road and Monroe Street sub-basins was within 11% of the collected data. These predictive accuracies are appropriate for planning-level analysis of stormwater quality.

#### 6.2 EXTENT OF CALIBRATION

Not all of the source area and land use stormwater quality generation options available in SLAMM could be calibrated given the extent of the study area data. Almost all runoff sources were calibrated, while less than half of the suspended solids and copper sources were calibrated. None of the stormwater management practice algorithms were calibrated due to the lack of data for the practices. Thus, some of the model land use/source area options retain the original parameters developed by WDNR. Further, due to the limited amount of data, none of the source area/land use stormwater quality prediction options that were calibrated were subjected to "blind" verification testing.

#### 6.3 ISSUES TO BE CONSIDERED IN THE FUTURE DEVELOPMENT OF THE SLAMM MODEL

Based on the experience gained during the conduct of this project, the following issues are proposed for consideration as the SLAMM model is further developed. The first set of issues may be regarded as conceptualization issues, which may need much expanded data bases for adequate evaluation. These issues include:

 Adsorption of pollutants to suspended solids may be strongly influenced by the clay mineral and organic matter content of the solids. If data can be obtained for model development, it may be appropriate to model suspended solids generation using several size fractions, and possibly organic matter content classes. Pollutant absorption parameters could then be linked to these size and content classes.

- Because of the general lack of data in many locations in the state, a
  reduction in the number of parameters describing rainfall/runoff and
  rainfall/suspended solids generation may be useful. This simplification
  could take the form of two- or three-parameter analytical expression option
  in addition to the current procedures.
- The addition of a description of the probability distribution of water quality parameters in the model output would aid the interpretation of possible variations in water quality.
- Since runoff water quality from streets is so large a factor in overall subbasin response, additional data collection and the refinement of model algorithms should emphasize street areas. A refinement might include increasing the responsiveness of the street source areas in the model to traffic volume.
- Currently, the model allows infiltration rates for pervious areas associated with A/B soils and pervious areas associated with C/D soils. To increase runoff prediction flexibility as additional data becomes available, a modification to the model would be to increase the model runoff prediction ability by allowing the model to predict runoff based upon additional series of infiltration rates, and possibly accounting for antecedent moisture conditions.
- Add control practices such as swales to individual source areas or land uses.
- Link up SLAMM output with an in-stream concentration prediction model by creating a SLAMM output format that would be compatible with the selected in-stream model.
- The balance of the contaminated runoff not accounted for by runoff either evaporates or infiltrates to groundwater. Therefore, the model might be useful as an indicator of potential sources of stormwater contamination in groundwater.

Additional issues are related to the calibration and verification of the SLAMM model as it is currently configured. These issues include:

· Updating and upgrading the existing model documentation.

- The calibration data utilized in this study represents two communities in southern Wisconsin. As such, soils, traffic, urban design or municipal management practices peculiar to the Milwaukee and Madison areas may be implicitly present in the calibrated parameters. A calibration data base drawn from a much wider geographic extent would tend to remove the potential bias in the current calibration.
- Additional data is needed to calibrate several land use/source area combinations. The model should be able to predict contaminant loadings for such pollutants as zinc, copper, chromium, cadmium, BOD, COD, nitrogen, phosphorus, suspended solids, and ammonia.
- Calibration of many management practice parameters may be difficult given the extent of current databases, because there is little data specifically comparing identical sites with and without management practices. Consequently, additional data and analysis of these practices should be performed.
- Development of a large enough database to allow independent calibration/verification analyses would further enhance documentation of the model.

[mad-603-34f]

#### REFERENCES

- Pitt, Robert, 1989. SLAMM 5 Source Loading and Management Model, Volume I: Model Development and Summary, April, 1989.
- U.S. EPA, 1983. Evaluation of Urban Nonpoint Source Pollution Management in Milwaukee County, Wisconsin, PB 84-114164.
- WDNR, 1989a. SLAMM 5 Source Loading and Management Model, Volume II: Algorithm Documentation, PUBL-WR-218-89, April, 1989.
- WDNR, 1989b. SLAMM 5 Source Loading and Management Model, Volume III: User's Manual, PUBL-WR-219-89, April, 1989.

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Table 1

Description of Watershed Data Used in SLAMM Model Calibration

Stormwater Management Practices used in Calibration	1	1	Street Sweeping/Catchbasins	Street Sweeping/Catchbasins	Street Sweeping/Catchbasins	, Street Sweeping/Catchbasins	Street Sweeping	Street Sweeping
Number of Storm Events	79	89	44 13	51	46	61 19	10	11
Sample <u>Period</u>	1980-1982	1980-1982	1980-1982 1990	1980-1982	1980-1982	1980-1982 1990	1991	1991
Source of Data	NURP	NURP	NURP WDNR-USGS	NURP	NURP	NURP WDNR-USGS	WDNR-USGS	WDNR-USGS
Percent Impervious Area	100%	100%	48%	48%	49% 87% 73%	55% 96% 100% 81%	33% 100% 100% 35%	62%
Total Area [ac]	12.10	12.40	32.40	99.19	10.41 18.64 29.05	16.25 23.17 4.64 44.06	236.43 1.36 7.15 244.95	115.72
Land Use	Commercial	Residential	Residential	Residential	Residential Commercial Total	Residential Commercial Industrial Total	Residential Institutional Commercial Total	Industrial
Study Area	Post Office	Rustler	Hastings	Burbank	State Fair	Wood Center	Monroe Street	Syene Road
Location	Milwaukee, WI	Milwaukee, WI	Milwaukee, WI	Milwaukee, WI	Milwaukee, WI	Milwaukee, WI	Madison, WI	Madison, WI

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Fraction of Roof and Driveway Surfaces not

Directly Connected to Storm Sewer System, from Field Observations

Table 2

		Percent of Source Area Surface not Directly Connected to Storm Sewers							
Study Area	Source Area	Mean Mean	Median						
Hastings	Driveways Garage Roofs	37 87	40 100						
r e	Residence Roofs	77	100						
Burbank	Driveways	36	40						
•	Garage Roofs	78	100						
· ·	Residence Roofs	78	100						
State Fair	Garage Roofs	24	25						
	Residence Roofs (entire roof)	60	70						
	Residence Roofs (front half only)	75	80						
Wood Center	Garage Roofs	16	. 0						
TOOU COILCI	Residence Roofs (entire roof)	45	50						
	Residence Roofs (front half only)	46	50						

#### Notes:

(1) Data collected from site visits on July 19, 1991 and August 1, 1991

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# Table 3 Summary of SLAMM Model Calibration Results for Total Runoff and Suspended Solids

(33)	(20)	<b>200</b>		1.53	1.28	1,	ı	1.28	1.29		ı		1.81	1.15	ı	i	1.47	1.17	-1	ı	2.10	1.48	1	1	1.97	1.53	1	ı
Suspended Colide (CC)	spillon non	Average SS	[sqj]	128	114	14	11%	113	113	0	%0		88	29	2	24%	99	63	က	2%	 114	93	21	18%	89	91	-2	2%
Suchan	odeno	Total SS	[sql]	10096	9001	1095	11%	8088	8827	-19	<b>%</b> 0		5898	4510	1388	24%	4318	4124	194	4%	5018	4107	911	18%	3814	3920	-106	3%
Γ	 T			1.03	1.07			1.05	1.08				1.05	1.02			1.06	1.03			1.83	1.72			1.91	1.77		
		200		 <del>-</del> -	<u>-</u>	1	ı	÷	<u> </u>	I	j		-	<del>-</del>	ı	1	1.(	<del>-</del>	1	1	7	<del>-</del>	ı	ľ	1.	-	ı	1
Bunoff		Average Depth	[in]	0.52	0.53	-0.01	2%	0.51	0.52	-0.01	2%	1	0.47	0.47	00.0	%0	0.44	0.45	-0.01	2%	0.23	0.24	-0.02	%6	0.22	0.24	-0.02	%6
		Total Depth	[ii]	40.83	41.56	-0.73	2%	39.99	40.75	-0.76	2%		31.80	31.89	-0.09	%0	29.25	29.42	-0.17	1%	10.01	10.69	-0.68	7%	9.45	10.23	-0.78	8%
				Observed	Predicted	Residual	% Diff	Observed	Predicted	Residual	% Diff		Observed	Predicted	Résidual	% Diff	Observed	Predicted	Residual	% Diff	Observed	Predicted	Residual	% Diff	Observed	Predicted	Residual	% Diff
fall	3	COV (2)		1.0	•		,	1.03					0.93				0.94	,			1.15				1.18			
Bainfall	ומוו	Average Depth	[in]	0.57				0.57					0.54				0.52			,	0.64				0.62			
,		Number of Events		79				78		-			68/67(1)				66/65(1)				44				43			-
		Study Area		Post Office	(All Data)	-		Post Office	(Less Outliers)		-		Rustler	(All Data)	•		Rustler	(Less Outliers)		-	Hastings - NURP	· (All Data)			Hastings - NURP	(Less Outliers)		

Table 3

Summary of SLAMM Model Calibration Results for Total Runoff and Suspended Solids

	Ť		•	]	1.95	0.70			1.11	0.34			1.14	0.38			0.93	0.39	•			1.40	0.41		-	1.17	0.35		
100	S (22)	) )	)		-	o	ı	ı	-	0	í.	ı		0		1	0	0	i.	, 1	,	<b>*</b>	0	. 1	1		0		
	Suspended Solids (SS)	Average	[sq]]		391	347	44	11%	220	301	₽ 9-	37%	292	280	12	4%	257	279	-25	%6	;	953	803	150	16%	780	269	11	*0
	edsns	Total	[sq]		19942	17676	2266	11%	10543	14431	-3888	37%	13435	12884	551	4%	11578	12571	-993	%6		58156	49005	9151	16%	45996	45391	605	2
		>	• •		1.59	1.69	1.	ı	0.82	0.87	1	ı	0.78	0.83	ĺ	1.	0.79	0.84	ı	-		1.12	1.11	1	1	0.88	0.86	1	
	HUNOTT	Average	[ui]	•	0.24	0.26	-0.02	8%	0.17	0.18	-0.01	%9	0.30	0.27	0.03	10%	0.29	0.27	0.02	7%		0.44	0.38	90.0	14%	0.38	0.33	0.05	7007
		Total	[in]		12.22	13.36	-1.13	%6	7.97	8.58	-0.61	8%	13.66	12.49	1.18	%6	13.21	12.11	1.10	%8		26.87	22.94	3.93	15%	22.44	19.18	3.26	ì
L	l.				Observed	Predicted	Residual	% Diff	Observed	Predicted	Residual	% Diff	Observed	Predicted	Residual	% Diff	Observed	Predicted	Residual	% Diff		Observed	Predicted	Residual	% Diff	Observed	Predicted	Residual	3:0
	tall	(%)	(1)	,	1.19		-		0.69	·	``.		0.71				0.72			, ,		0.94				0.75			
	Haintal	Average	[in]		0.66				0.52				0.45	\$			0.44					0.55				0.49			
		Number of Events			51				48				46		-		45	·				61				59	,		_
		Study Area	Sol Conso		Burbank	(All Data)			Burbank	(Less Outliers)			State Fair	(All Data)			State Fair	(Less Outliers)				Wood Center - NURP	(All Data)			Wood Center - NURP	(Less Outliers)	-	

Table 3
Summary of SLAMM Model Calibration Results for Total Runoff and Suspended Solids

Table 3

# Summary of SLAMM Model Calibration Results for Total Runoff and Suspended Solids

			<u> </u>			0.84	0.59				**		
	s (SS)		<u>}</u>							-			
	Suspended Solids (SS)	Average	SS	[sql]	1	928	1032	-74	8%				
	Suspe	Total	SS	[sql]		10536	11351	-815	8%				
1					1								
			00			0.96	0.84	1	. ·				-
	Runoff	Average	Depth	[in]		0.37	0.27	0.10	27%				
		Total	Depth	[in]		4.12	2.97	1.15	28%				
•						Observed	Predicted	Residual	% Diff	Observed	Predicted	Residual	% Diff
	ıfall		COV (2)	- ,		0.77		-					
	Rainfal	Average	Depth	[iii]		0.54							
		Number	of Events	:		+							-
			Study Area			Syene Road	(All Data)			Syene Road	(Less Outliers)		
			Str.	-		Sye				Sye	(Les	•	-

Notes:

- 66/65 Number of runoff events/Number of Suspended Solids events
   COV Coefficient of Variation, defined as Standard Deviation divided by Mean
   W Diff = Absolute Value of Residual divided by Observed Value

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# Table 4 Summary of SLAMM Model Calibration Results for Copper

		_	***		
	Number		Total	Dissolved	Particulate
Study Area	of Events		Copper	Copper	Copper
			[lbs]	[lbs]	[lbs]
Monroe Street	8	Observed	0.341	0.100	0.241
		Predicted	0.346	0.111	0.233
		Residual	-0.005	-0.011	0.008
		% Diff	1%	11%	3%
Syene Road	6	Observed	0.312	0.117	0.195
		Predicted	0.347	0.141	0.205
		Residual	-0.035	-0.024	-0.010
		% Diff	11%	21%	5%

#### Notes:

- 1) Residuals = Observed value less Predicted value
- 2) % Diff = Absolute Value of Residuals divided by Observed Value

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Table 5

Runoff Sources Areas Calibrated for Runoff Generation in SLAMM

Runoff Source	Calibrated	Not Calibrated
Connected Flat Roofs	X	
Connected Pitched Roofs	Χ .	
Directly Connected Impervious Areas	X	
Directly Connected Unpaved Areas	(1)	•
Pervious Areas - A/B Soils	(1)	
Pervious Areas - C/D Soils	$\mathbf{X}$	*
Smooth Textured Streets	X	•
Intermediate Textured Streets	X	
Rough Textured Streets	7	X
Drainage Modifier:		
C/D Soils, w/o Alleys, Medium to High Density Land Use	X	
C/D Soils, w/Alleys, Medium to High Density Land Use	X	
C/D Soils for Ship Commercial and Shopping Center Land Uses		X

#### NOTES:

- (1) Uncertain calibration only, due to sparse data.
- (2) Note that runoff production is not dependent on land use.

SLAMM Source Areas Calibrated for Suspended Solids Loading

# Land Uses

Source Areas	Residential	Institutional	Commercial	Industrial	Open Spaces	Freeways
Roofs	×	(1)	×	×		
Paved Parking/Storage		(1)	×	×		×
Unpaved Parking/Storage	-		(1)			
Playgrounds			•			
Driveways	×					
Sidewalks	X		×	(1)		
Streets - Smooth (2)	×		×	×		•
Streets - Intermedials (2)	×		×	×		
Streets - Rough (2)						4
Large Landscaped Areas (3)						
Undeveloped Areas						•
Small Landscaped Areas (3)	×		(1)	×		
Freeway Lanes/Shoulders	· ·					

## NOTES:

- 1. Uncertain calibration due to sparse data.
- 2. All street area calibrations included some level of street sweeping; see text.
- All landscaped areas are assumed to generate similar levels of suspended solids.

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# SLAMM Source Areas Calibrated for Copper Loading

# Land Uses

Source Areas	Residential	<u>Institutional</u>	Commercial	Industrial	Open Spaces Freeways
Roofs Paved Parking/Storage Unpaved Parking/Storage Playgrounds Driveways Sidewalks Streets Large Landscaped Areas Undeveloped Areas Small Landscaped Areas	×× × ® × 4 ×	£ 6	×× ©×	X X (2) (2) X (4) (4)	
				. )	

### Notes:

- (1) Calibration based upon commercial roof data.
- ) Calibration based upon commercial paved parking/storage data.
  - Calibration based upon residential driveway data.
- Calibration based upon residential small landscaped area data.
- Calibration based upon industrial paved parking/storage data.

Calibration includes both particulates and dissolved forms of copper.

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TABLE 8

Results of the SLAMM Model Application to Example Watersheds

· · · · · · · · · · · · · · · · · · ·		Mode	l Total Loa	ding Results		
			Total	Suspended Solids	Total Copper	
Lilly Creek Sub-basin	Area (acres)	Rainfall (in.)	Runoff (cf)	Loading ( <u>lbs)</u>	Loading (lbs)	
LILLYC	207.72	30.36	9361171	179600	15.96	
LILLYG	67.02	30.36	1810307	16292	0.86	

## Note:

- 1) Rainfall file used was typical for annual rainfall in the Milwaukee area.
- 2) Runoff and loading values are totals before outfall control reduction or delivery system reductions are applied by the model.

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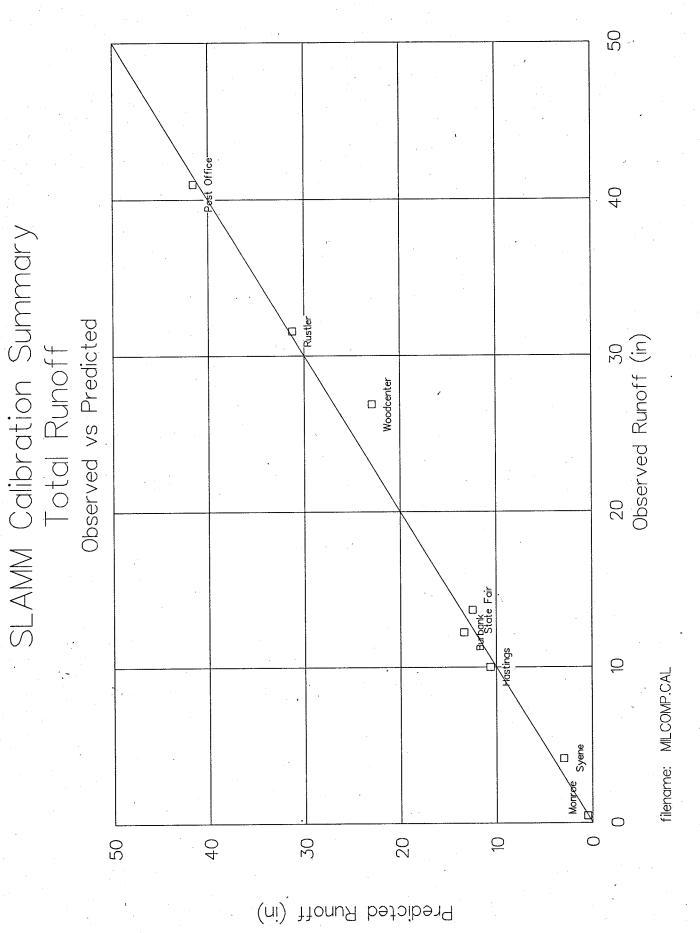
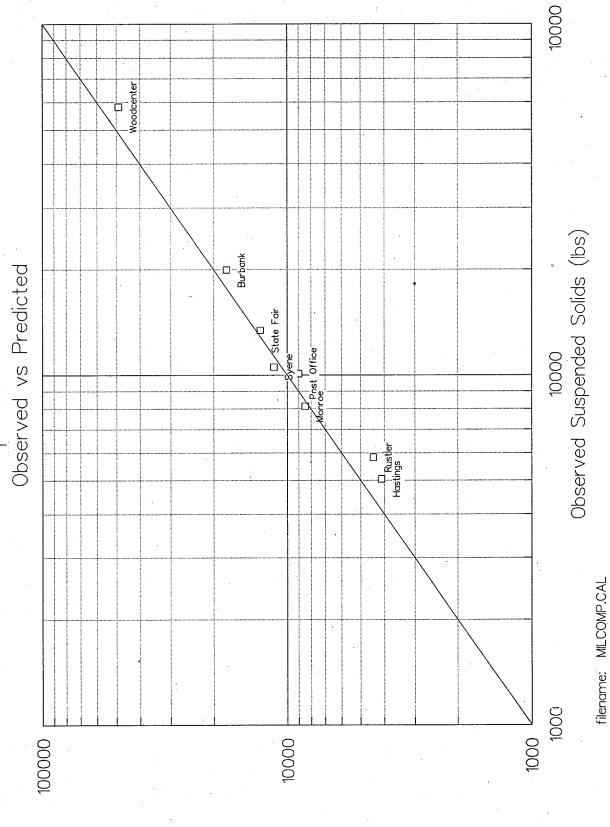


Figure 1: SLAMM Calibration Summary Results: Total Runoff

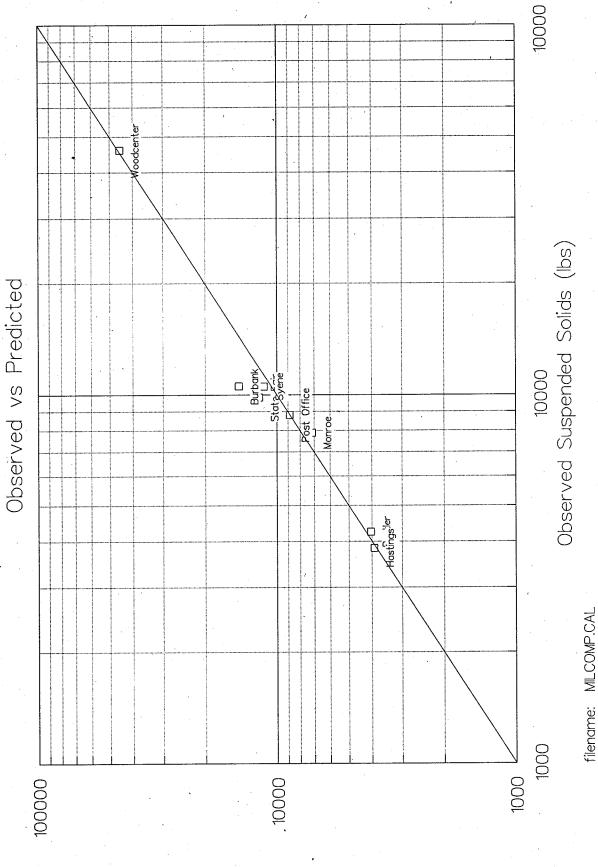
# SLAMM Calibration Summary Suspended Solids



Predicted Suspended Solids (lbs)

Figure 2: SLAMM Calibration Summary Results: Suspended Solids

## Suspended Solids less Outliers SLAMM Calibration Summary



Predicted Suspended Solids (lbs)

Suspended Solids Less Outliers Figure 3: SLAMM Calibration Summary Results:

# Lilly Creek Sub Basin LILLYC

Area, Runoff and Pollutant Loading Distribution from Multiple Land Uses

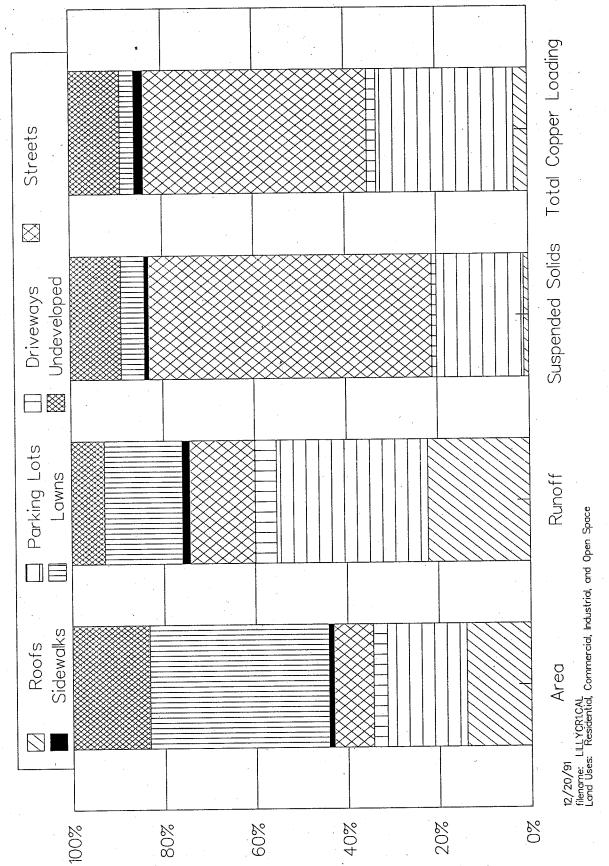


Figure 4: Lilly Creek Sub-Basin LILLYC Demonstration Model Run Results

3

# Lilly Creek Sub Basin LILLYG

Area, Runoff, and Pollutant Loading Distribution from Residential Land Uses

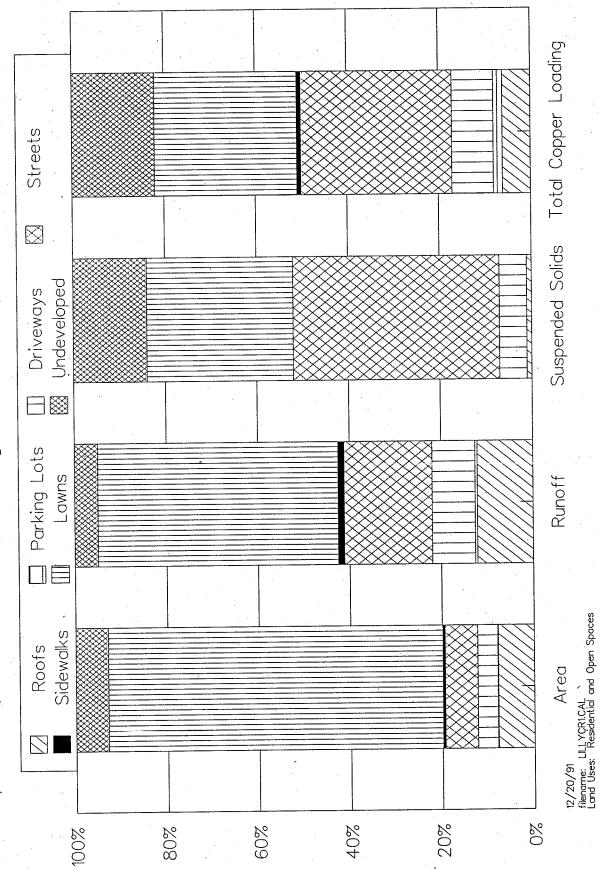


Figure 5: Lilly Creek Sub-Basin LILLYG Demonstration Model Run Results

## Appendix A

**Source Area Description Files and Parameter Files** 

A1 - Source Area Description Files A2 - Parameter Files

## **A1**

Source Area Description Files

Data file name: POSTOO.DAT Rain file name: PFINAL1.RAN

Runoff Coefficient file name: MILW6.RSV.

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 04/01/80

Date: 11-30-1991

Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

2. Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in: 3. Poor condition (or very flat) .25

Fair condition .75
 Good condition (or very steep) 0

Site information: MILW6.RSV, MILW11.PSC, DELIV2.PRR
Areas for each Source (acres)

Source Area	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas	Freeway Source Area
Roofs 1	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 1
Roofs 2	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 2
Roofs 3	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 3
Roofs 4	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 4
Roofs 5	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 5
Paved Parking/Storage	0.00	0.00	12.10	0.00	0.00	Large Turf Areas
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Undeveloped Areas
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Other Pervious Areas
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Directly Connected Imperv Area
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Partially Connected Imperv Area
Playground 1	0.00	0.00	0.00	0.00	0.00	
Playground 2	0.00	0.00	0.00	0.00	0.00	Total
Driveways 1	0.00	0.00	0.00	0.00	0.00	
Driveways 2	0.00	0.00	0.00	0.00	0.00	
Driveways 3	0.00	0.00	0.00	0.00	0.00	
Sidewalks/Walks 1	0.00	0.00	0.00	0.00	0.00	
Sidewalks/Walks 2	0.00	0.00	0.00	0.00	0.00	
Street Area 1	0.00	0.00	0.00	0.00	0.00	
Street Area 2	0.00	0.00	0.00	0.00	0.00	
Street Area 3	0.00	0.00	0.00	0.00	0.00	
Lrg Lndscpd Area 1	0.00	0.00	0.00	0.00	0.00	
Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00	
Undeveloped Area	0.00	0.00	0.00	0.00	0.00	
Smil Lndscpd Area 1	0.00	0.00	0.00	0.00	0.00	
Smll Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00	
Smll Lndscpd Area 3	0.00	0.00	0.00	0.00	0.00	
Isolated Area	0.00	0.00	0.00	0.00	0.00	
Other Pervious Area	0.00	0.00	0.00	0.00	0.00	Programme and the second second
Other Directly Connect	0.00	0.00	0.00	0.00	0.00	
Other Partially Connec	0.00	0.00	0.00	0.00	0.00	
Total	0.00	0.00	12.10	0.00	0.00	
Total of All Source Area	s		12.10			
Total of All Source Area less All Isolated A		,	12.10			

Particulate Solids Concentration file name: MILW11.PSC

Area (

Pollutant Relative Concentration file name: MILW.POL

Study period ending date: 06/30/82

Time: 14:23:39

Source Area Control Practice Information

Commercial Areas

Paved Parking/Storage 1 Source area number: 66

The Source Area is directly connected or draining to a directly conntected area

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Catchbasin or Drainage Controls

Outfall Controls

Data file name: RUSTOO.DAT Rain file name: RUST1.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 04/01/80

Date: 11-30-1991

Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

2. Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in:

3. Poor condition (or very flat) 0

Fair condition 1
 Good condition (or very steep) 0

Site information: MILW6.RSV, MILW11.PSC, DELIV2.PRR Areas for each Source (acres)

	Source Area	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas		Freeway Source Area	Area
	Roofs 1	0.00	0.00	5.26	0.00	0.00		Paved Lane & Shoulder Area 1	
	Roofs 2	0.00	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 2	
	Roofs 3	0.00	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 3	•
	Roofs 4	0.00	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 4	
	Roofs 5	0.00	0.00	0.00	0.00	0.00	1	Paved Lane & Shoulder Area 5	
	Paved Parking/Storage	0.00	0.00	7.14	0.00	0.00		Large Turf Areas	
	Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	•	Undeveloped Areas	
	Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00		Other Pervious Areas	
	Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00		Other Directly Connected Imperv	Area
	Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00		Other Partially Connected Imperv	√ Area
	Playground 1	0.00	0.00	0.00	0.00	0.00			- · ·
	Playground 2	0.00	0.00	0.00	0.00	0.00		Total	
	Driveways 1	0.00	0.00	0.00	0.00	0.00			
	Driveways 2	0.00	0.00	0.00	0.00	0.00			
	Driveways 3	0.00	0.00	< 0.00	0.00	0.00			
	Sidewalks/Walks 1	0.00	0.00	0.00	0.00	0.00			
	Sidewalks/Walks 2	0.00	0.00	0.00	0.00	0.00			
	Street Area 1	0.00	0.00	0.00	0.00	0.00			
	Street Area 2	0.00	0.00	0.00	0.00	0.00		· ·	
	Street Area 3	0.00	0.00	0.00	0.00	0.00		•	
	Lrg Lndscpd Area 1	0.00	0.00	0.00	0.00	0.00			
	Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00			
	Undeveloped Area	0.00	0.00	0.00	0.00	0.00	•		
	Smll Lndscpd Area 1	0.00	0.00	0.00	0.00	0.00			
	Smll Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00		· ·	
	Smll Lndscpd Area 3	0.00	0.00	0.00	0.00	0.00			
	Isolated Area	0.00	0.00	0.00	0.00	0.00			
	Other Pervious Area	0.00	0.00	0.00	0.00	0.00			
•	Other Directly Connect	0.00	0.00	0.00	0.00	0.00			
	Other Partially Connec	0.00	0.00	0.00	0.00	0.00			**
	Total	0.00	0.00	12.40	0.00	0.00			
	.2								

Particulate Solids Concentration file name: MILW11.PSC

Pollutant Relative Concentration file name: MILW.POL

Study period ending date: 06/30/82

Time: 14:24:25

Total of All Source Areas

12.40

Total of All Source Areas

less All Isolated Areas

12.40

### Source Area Control Practice Information

Commercial Areas

Roofs 1 Source area number: 61

The roof is flat

The Source Area is directly connected or draining to a directly conntected area

Source area number: 66 Paved Parking/Storage 1

The Source Area is directly connected or draining to a directly connected area

Catchbasin or Drainage Controls

Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name Pollutant Type Residue Particulate

Data file name: HASTOO.DAT Rain file name: HAST1.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 06/01/80

Date: 11-30-1991

Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in:

3. Poor condition (or very flat) 1

4. Fair condition 0

5. Good condition (or very steep) 0

Site information: HAST9.DAT W/ MILW6.RSV, MILW11.PSC, DELIV2.PRR

Areas for each Source (acres)

Source Area	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas		Freeway Source Area Area (
Roofs 1	1.35	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 1
Roofs 2	5.07	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 2
Roofs 3	0.00	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 3
Roofs 4	0.00	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 4
Roofs 5	0.00	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 5
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00		Large Turf Areas
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00		Undeveloped Areas
Payed Parking/Storage	0.00	0.00	0.00	0.00	0.00		Other Pervious Areas
Unpayed Parking/Storag	0.00	0.00	0.00	0.00	0.00		Other Directly Connected Imperv Area
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00		Other Partially Connected Imperv Area
Playground 1	0.00	0.00	0.00	0.00	0.00		
Playground 2	0.00	0.00	0.00	0.00	0.00		Total
Driveways 1	2.67	0.00	0.00	0.00	0.00		
Driveways 2	1.95	0.00	0.00	0.00	0.00		
Driveways 3	0.00	0.00	0.00	0.00	0.00		
Sidewalks/Walks 1	0.00	0.00	0.00	0.00	0.00		
Sidewalks/Walks 2	0.00	0.00	0.00	0.00	0.00		
Street Area 1	4.40	0.00	0.00	0.00	0.00		
Street Area 2	0.00	0.00	0.00	0.00	0.00		
Street Area 3	0.00	0.00	0.00	0.00	0.00		
Lrg Lndscpd Area 1	0.00	0.00	0.00	0.00	0.00		
Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00		
Undeveloped Area	0.00	0.00	0.00	0.00	0.00		
Smil Lndscpd Area 1	16.79	0.00	0.00	0.00	0.00		
Smil Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00		
Smll Lndscpd Area 3	0.00	0.00	0.00	0.00	0.00		•
Isolated Area	0.17	0.00	0.00	0.00	0.00		•
Other Pervious Area	0.00	0.00	0.00	0.00	0.00		
Other Directly Connect	0.00	0.00	0.00	0.00	0.00		
Other Partially Connec	0.00	0.00	0.00	0.00	0.00		
Total	32.40	0.00	0.00	0.00	0.00	•	
Total of All Source Areas	<b>S</b>		32.40				

Particulate Solids Concentration file name: MILW11.PSC Pollutant Relative Concentration file name: MILW.POL

Study period ending date: 06/30/82

Time: 14:24:38

Total of All Source Areas

less All Isolated Areas

32.23

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### Source Area Control Practice Information

Residential Areas

Roofs 1 Source area number: 1

The roof is pitched

The Source Area is directly connected or draining to a directly conntected area

Roofs 2 Source area number: 2

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are not present

Source area number: 13 Driveways 1

The Source Area is directly connected or draining to a directly connected area

Driveways 2 Source area number: 14

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are not present

Street Area 1 Source area number: 18

1. Street Texture: intermediate

- Total study area street length (curb-miles): 2.25
   Initial Street Dirt Loading (lbs/curb-mi): default value
- 4. Street Dirt Accumulation:

Default value used Control Practice: Street Cleaning

1. Street cleaning schedule:

Begin cleaning on: 04/15/80

Schedule: Every 2 weeks (Wed)

Begin cleaning on: 10/30/80 Schedule: None

Begin cleaning on: 03/13/81 Schedule: 2 Passes/week (Tue, Thur) Schedule: Every 4 weeks (Wed) Begin cleaning on: 05/14/81 Begin cleaning on: 06/28/81

Schedule: 2 Passes/week (Tue,Thur) Schedule: None Begin cleaning on: 07/18/81

Begin cleaning on: 10/05/81 Schedule: 2 Passes/week (Tue, Thur)

Begin cleaning on: 11/14/81

Schedule: None Schedule: Every 2 weeks (Wed) Begin cleaning on: 04/15/82

Final cleaning period ending date: 06/30/82

- 2. Street cleaner productivity: Default
- 3. Parking density: Light
- 4. Parking controls imposed? Yes
- 5. Equation coefficient M (slope): 9.000001E-02
- 6. Equation coefficient B (intercept):

Smil Lndscpd Area 1 Source area number: 24

The SCS Hydrologic Soil Type is C/D

### Catchbasin or Drainage Controls

Control Practice 1: Catchbasin Cleaning Controls

- 1. Total sump volume (cubic feet)= 306
- 2. Area served by catchbasins (acres)= 32.23
- 3. Percent of sump volume full at beginning of study period= 0 %
- 4. Number of times catchbasins cleaned each year= 0

### Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name

Pollutant Type

Residue

Particulate

Data file name: HAST103.DAT

Rain file name: HAST90.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Date: 11-30-1991

Study period starting date: 02/01/90

Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

2. Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in:

3. Poor condition (or very flat) 1

4. Fair condition 0

5. Good condition (or very steep) 0

Site information: HAST102.DAT W/ MILW6.RSV, DELIV2.PRR, MILW11.PSC Areas for each Source (acres)

Source Area	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas	Freeway Source Area	,
Roofs 1	1.35	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 1	
Roofs 2	5.07	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 2	
Roofs 3	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 3	
Roofs 4	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 4	
Roofs 5	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 5	
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Large Turf Areas	
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Undeveloped Areas	
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Other Pervious Areas	
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Directly Connected Imperv Area	
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Partially Connected Imperv Area	
Playground 1	0.00	0.00	0.00	0.00	0.00	,	
Playground 2	0.00	0.00	0.00	0.00	0.00	Total	
Driveways 1	2.67	0.00	0.00	0.00	0.00		
Driveways 2	1.95	0.00	0.00	0.00	0.00		
Driveways 3	0.00	0.00	0.00	0.00	0.00		
Sidewalks/Walks 1	0.00	0.00	0.00	0.00	0.00		
Sidewalks/Walks 2	0.00	0.00	0.00	0.00	0.00	•	
Street Area 1	4.40	0.00	0.00	0.00	0.00	•	
Street Area 2	0.00	0.00	0.00	0.00	0.00		
Street Area 3	0.00	0.00	0.00	0.00	0.00		
Lrg Lndscpd Area 1	0.00	0.00	0.00	0.00	0.00		
Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00		
Undeveloped Area	0.00	0.00	0.00	0.00	0.00		
Smil Lndscpd Area 1	16.79	0.00	0.00	0.00	0.00		
Smil Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00		
Smil Lndscpd Area 3	, 0.00	0.00	0.00	0.00	0.00		
Isolated Area	0.17	0.00	0.00	0.00	0.00		
Other Pervious Area	0.00	0.00	0.00	0.00	0.00		
Other Directly Connect	0.00	0.00	0.00	0.00	0.00	•	
Other Partially Connec	0.00	0.00	0.00	0.00	0.00		
Total	32.40	0.00	0.00	0.00	0.00		

Particulate Solids Concentration file name: MILW11.PSC

Area (

Pollutant Relative Concentration file name: MILW.POL

Study period ending date: 08/30/90

Time: 14:24:50

Total of All Source Areas

32.40

Total of All Source Areas less All Isolated Areas

32.23 =======

Source Area Control Practice Information

Residential Areas

Roofs 1 Source area number: 1

The roof is pitched

The Source Area is directly connected or draining to a directly connected area

Roofs 2 Source area number: 2

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are not present

Driveways 1 Source area number: 13

The Source Area is directly connected or draining to a directly connected area

Source area number: 14

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are not present

Street Area 1 Source area number: 18

1. Street Texture: intermediate

- Total study area street length (curb-miles): 2.25
   Initial Street Dirt Loading (lbs/curb-mi): default value
   Street Dirt Accumulation:

Default value used

Control Practice: Street Cleaning

1. Street cleaning schedule:

Begin cleaning on: 04/15/90 Schedule: Every 4 weeks (Wed) Final cleaning period ending date: 08/30/90

- 2. Street cleaner productivity: Default
- 3. Parking density: Light
  4. Parking controls imposed? No
- 5. Equation coefficient M (slope): .3

6. Equation coefficient B (intercept): 450
Smll Lndscpd Area 1 Source area number: 24

The SCS Hydrologic Soil Type is C/D

### Catchbasin or Drainage Controls

Control Practice 1 : Catchbasin Cleaning Controls
1. Total sump volume (cubic feet)= 306

- Area served by catchbasins (acres)= 32.23
   Percent of sump volume full at beginning of study period= 0 %
   Number of times catchbasins cleaned each year= 0

### Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name

Pollutant Type

Residue

Particulate

Data file name: BURB00.DAT Rain file name: BURB2.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 06/01/80

Date: 11-30-1991

Study period ending date: 05/30/82

Particulate Solids Concentration file name: MILW11:PSC Pollutant Relative Concentration file name: MILW.POL

Time: 14:25:07

Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

2. Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in:

Poor condition (or very flat) 0
 Fair condition 0

Good condition (or very steep) 1

Site information: BURB15.DAT W/ MILW6.RSV, MILW11.PSC, DELIV2.PRR Areas for each Source (acres)

Source Area	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas	Freeway Source Area Area (
Roofs 1	2.44	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 1
Roofs 2	9.05	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 2
Roofs 3	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 3
Roofs 4	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 4
Roofs 5	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 5
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Large Turf Areas
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Undeveloped Areas
Paved Parking/Storage	0.00	0.00	0.00	0.00	·0.00	Other Pervious Areas
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Directly Connected Imperv Area
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Partially Connected Imperv Area
Playground 1	0.00	0.00	0.00	0.00	0.00	•••
Playground 2	0.00	0.00	0.00	0.00	0.00	Total
Driveways 1	4.80	0.00	0.00	0.00	0.00	
Driveways 2	3.36	0.00	0.00	0.00	0.00	
Driveways 3	0.00	0.00	0.00	0.00	0.00	
Sidewalks/Walks 1	0.00	0.00	0.00	0.00	0.00	
Sidewalks/Walks 2	0.00	0.00	- 0.00	0.00	0.00	
Street Area 1	9.64	0.00	0.00	0.00	0.00	
Street Area 2	0.00	0.00	0.00	0.00	0.00	
Street Area 3	0.00	0.00	0.00	0.00	0.00	
Lrg Lndscpd Area 1	0.00	0.00	0.00	0.00	0.00	
Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00	•
Undeveloped Area	0.00	0.00	0.00	0.00	0.00	
Smll Lndscpd Area 1	32.10	0.00	0.00	0.00	0.00	
Smil Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00	
Smil Lndscpd Area 3	0.00	0.00	0.00	0.00	0.00	
Isolated Area	0.27	0.00	0.00	0.00	0.00	
Other Pervious Area	0.00	0.00	0.00	0.00	0.00	
Other Directly Connect	0.00	0.00	0.00	0.00	0.00	
Other Partially Connec	0.00	0.00	0.00	0.00	0.00	
Total	61.66	0.00	0.00	0.00	0.00	
Total of All Source Area	ıs		61.66			

Total of All Source Areas

Total of All Source Areas

less All Isolated Areas

61.39

Source Area Control Practice Information

Residential Areas

Roofs 1 Source area number: 1

The roof is pitched

The Source Area is directly connected or draining to a directly conntected area

Roofs 2 Source area number: 2

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are not present

Driveways 1 Source area number: 13

The Source Area is directly connected or draining to a directly conntected area

Driveways 2 Source area number: 14

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are not present

Street Area 1 Source area number: 18

1. Street Texture: intermediate

- 2. Total study area street length (curb-miles): 4.18
- 3. Initial Street Dirt Loading (lbs/curb-mi): default value
- 4. Street Dirt Accumulation:

### Default value used

Control Practice: Street Cleaning

1. Street cleaning schedule:

Begin cleaning on: 04/15/80 Schedule: Every 4 weeks (Wed)

Schedule: None Begin cleaning on: 11/1/80

Schedule: Every 4 weeks (Wed)
Schedule: None
Schedule: Every 4 weeks (Wed) Begin cleaning on: 04/15/81

Begin cleaning on: 11/1/81

Begin cleaning on: 04/15/82

Final cleaning period ending date: 05/30/82

2. Street cleaner productivity: Default

3. Parking density: Light

4. Parking controls imposed? No

5. Equation coefficient M (slope): .36. Equation coefficient B (intercept): 450

Smil Lndscpd Area 1 Source area number: 24 The SCS Hydrologic Soil Type is C/D

### Catchbasin or Drainage Controls

Control Practice 1 : Catchbasin Cleaning Controls

- 1. Total sump volume (cubic feet)= 583
- 2. Area served by catchbasins (acres)= 61.39
- 3. Percent of sump volume full at beginning of study period= 0 %
- 4. Number of times catchbasins cleaned each year= 0

### Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name

Pollutant Type

Residue

Particulate

Data file name: SF00.DAT

Rain file name: SF1.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 04/15/80

Date: 11-30-1991

Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

2. Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in:

3. Poor condition (or very flat) 0

4. Fair condition 0

5. Good condition (or very steep) 1

Site information: SF9.DAT W/ MILW6.RSV, MILW11.PSC, DELIV2.PRR Areas for each Source (acres)

Source Area	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas		Freeway Source Area	Area
Roofs 1	0.86	0.00	4.72	0.00	0.00		Paved Lane & Shoulder Area 1	
Roofs 2	1.58	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 2	
Roofs 3	0.00	0.00	0.00	0.00	0.00	100	Paved Lane & Shoulder Area 3	
Roofs 4	0.00	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 4	
Roofs 5	0.00	0.00	0.00	0.00	0.00		Paved Lane & Shoulder Area 5	
Paved Parking/Storage	0.00	0.00	4.67	0.00	0.00		Large Turf Areas	
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00		Undeveloped Areas	
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00		Other Pervious Areas	
Unpaved Parking/Storag	0.00	0.00	0.34	0.00	0.00		Other Directly Connected Imperv Area	
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00		Other Partially Connected Imperv Area	į
Playground 1	0.00	0.00	0.00	0.00	0.00			
Playground 2	0.00	0.00	0.00	0.00	0.00		Total	
Driveways 1	0.41	0.00	0.00	0.00	0.00			
Driveways 2	0.00	0.00	0.00	0.00	0.00			•
Driveways 3	0.00	0.00	0.00	0.00	0.00			
Sidewalks/Walks 1	0.20	0.00	1.36	0.00	0.00			
Sidewalks/Walks 2	0.20	0.00	0.00	0.00	0.00			
Street Area 1	1.55	0.00	4.86	√ 0.00	0.00			
Street Area 2	0.28	0.00	0.00	0.00	0.00		•	
Street Area 3	0.00	0.00	0.00	0.00	0.00			
Lrg Lndscpd Area 1	0.00	0.00	0.00	0.00	0.00		*	
Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00			
Undeveloped Area	0.00	0.00	0.00	0.00	0.00			
Smil Lndscpd Area 1	5.32	0.00	2.42	0.00	0.00			
Smil Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00			
Smll Lndscpd Area 3	0100	0.00	0.00	0.00	0.00			•
Isolated Area	0.00	0.00	0.00	0.00	0.00			
Other Pervious Area	0.00	0.00	0.00	0.00	0.00			
Other Directly Connect	0.00	0.00	0.27	0.00	0.00			
Other Partially Connec	0.00	. 0.00	0.00	0.00	0.00			
Total	10.41	0.00	18.64	0.00	0.00			
Total of All Source Area	ıs		29.05				•	
							· · · · · · · · · · · · · · · · · · ·	

Particulate Solids Concentration file name: MILW11.PSC

Pollutant Relative Concentration file name: MILW.POL

Study period ending date: 12/31/82

Time: 14:25:20

### Source Area Control Practice Information

Residential Areas

Total of All Source Areas

less All Isolated Areas

Roofs 1 Source area number: 1

The roof is pitched

The Source Area is directly connected or draining to a directly connected area

29.05

Roofs 2 Source area number: 2

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are present

Source area number: 13 Driveways 1

The Source Area is directly connected or draining to a directly conntected area

Sidewalks/Walks 1 Source area number: 16

The Source Area is directly connected or draining to a directly connected area

Sidewalks/Walks 2 Source area number: 17

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are present

```
Street Area 1
                   Source area number: 18
         1. Street Texture: intermediate
2. Total study area street length (curb-miles): .61
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 03/18/80
                                               Schedule: 2 Passes/week (Tue, Thur)
                Begin cleaning on: 11/01/80
                                               Schedule:
                                                          None
                Begin cleaning on: 03/18/81
                                               Schedule: 2 Passes/week (Tue, Thur)
                Begin cleaning on: 11/14/81
                                               Schedule: None
                Begin cleaning on: 04/01/82
                                               Schedule: 2 Passes/week (Tue, Thur)
                Final cleaning period ending date: 10/15/82
           2. Street cleaner productivity: Default
           3. Parking density: Medium
           4. Parking controls imposed? No
           5. Equation coefficient M (slope): .65
           Equation coefficient B (intercept):
  Street Area 2
                  Source area number: 19
           1. Street Texture: smooth
           2. Total study area street length (curb-miles): .11
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 03/18/80
                                               Schedule: 2 Passes/week (Tue, Thur)
                                               Schedule: None
                Begin cleaning on: 11/01/80
                Begin cleaning on: 03/18/81
                                               Schedule: 2 Passes/week (Tue, Thur)
                Begin cleaning on: 11/14/81
                                               Schedule: None
                Begin cleaning on: 04/01/82
                                               Schedule: 2 Passes/week (Tue,Thur)
                Final cleaning period ending date: 11/01/82
           2. Street cleaner productivity: Default
           3. Parking density: Medium
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           Equation coefficient B (intercept):
  Smil Lndscpd Area 1
                        Source area number: 24
        The SCS Hydrologic Soil Type is C/D
Commercial Areas
             Source area number: 61
        The roof is flat
        The Source Area is directly connected or draining to a directly conntected area
  Paved Parking/Storage 1 Source area number: 66
        The Source Area is directly connected or draining to a directly connected area
  Unpaved Parking/Storage 1 Source area number: 69
        The Source Area is directly connected or draining to a directly connected area
  Sidewalks/Walks 1
                      Source area number: 76
        The Source Area is directly connected or draining to a directly connected area
  Street Area 1
                  Source area number: 78

    Street Texture: intermediate
    Total study area street length (curb-miles): 1.48

           3. Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 03/18/80
                                               Schedule: 2 Passes/week (Tue, Thur)
                Begin cleaning on: 11/01/80
                                               Schedule: None
                Begin cleaning on: 03/18/81
                                               Schedule: 2 Passes/week (Tue,Thur)
                                               Schedule: None
                Begin cleaning on: 11/14/81
                Begin cleaning on: 04/01/82
                                               Schedule: 2 Passes/week (Tue, Thur)
                Final cleaning period ending date: 10/15/82
           2. Street cleaner productivity: Default
           3. Parking density: Extensive (short term
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept):
  Smil Lndscpd Area 1 Source area number: 84
        The SCS Hydrologic Soil Type is C/D
Catchbasin or Drainage Controls
```

Control Practice 1: Catchbasin Cleaning Controls

- Total sump volume (cubic feet)= 100
   Area served by catchbasins (acres)= 29.05
- 3. Percent of sump volume full at beginning of study period= 0 %
- 4. Number of times catchbasins cleaned each year= 0

### Outfall Controls

### Pollutants to be Analyzed and Printed:

Pollutant Name Residue Pollutant Type Particulate Data file name: WCENOO.DAT

Rain file name: WCEN1.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 02/01/80

Date: 11-30-1991 Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

2. Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in:
3. Poor condition (or very flat) 0

4. Fair condition 0

5. Good condition (or very steep) 1

Site information: WCEN6.DAT W/ MILW6.RSV, MILW11.PSC, DELIV2.PRR Areas for each Source (acres)

Source A	lrea	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas	Freeway Source Area
Roofs 1		2.74	0.00	4.24	1.20	0.00	Paved Lane & Shoulder Area 1
Roofs 2	,	1.89	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 2
Roofs 3		0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 3
Roofs 4		0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 4
Roofs 5		0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 5
Paved Pa	rking/Storage	0.00	0.00	4.66	2.73	0.00	Large Turf Areas
Paved Pa	rking/Storage	0.00	0.00	0.00	0.00	0.00	Undeveloped Areas
Paved Pa	arking/Storage	0.00	0.00	0.00	0.00	0.00	Other Pervious Areas
Unpaved	Parking/Storag	0.90	0.00	0.89	0.00	0.00	Other Directly Connected Imperv Area
Unpaved	Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Partially Connected Imperv Area
Playgrou	und 1	0.00	0.00	0.00	0.00	0:00	
Playgrou	und 2	0.00	0.00	0.00	0.00	0.00	Total
Driveway	/s 1	0.68	0.00	0.00	0.00	0.00	$\mathbf{I}_{i} = \mathbf{I}_{i} + \mathbf{I}_{i}$
Driveway	/s 2	0.00	0.00	0.00	0.00	0.00	
Driveway	/s 3	0.00	0.00	0.00	0.00	0.00	
Sidewall	cs/Walks 1	0.21	0.00	3.08	0.21	0.00	
Sidewalk	cs/Walks 2	0.21	0.00	0.10	0.00	0.00	
Street A	rea 1	2.00	0.00	7.90	0.43	0.00	
Street A	Area 2	0.35	0.00	1.40	0.07	0.00	•
Street A	\rea 3	0.00	0.00	0.00	0.00	0.00	
Lrg Lnds	scpd Area 1	0.00	0.00	0.00	0.00	0.00	
L'rg Lnds	scpd Area 2	0.00	0.00	0.00	0.00	0.00	
Undevelo	oped Area	0.00	0.00	0.00	0.00	0.00	
Smll Lnd	dscpd Area 1	7.27	0.00	0.90	0.00	0.00	
Smil Lno	dscpd Area 2	0.00	0.00	0.00	0.00	0.00	
Smll Lnc	dscpd Area 3	0.00	0.00	0.00	0.00	0.00	
Isolated	d Area	0.00	0.00	0.00	0.00	0.00	
Other Pe	ervious Area	0.00	0.00	0.00	0.00	0.00	
Other Di	rectly Connect	0.00	0.00	0.00	0.00	0.00	
Other Pa	artially Connec	0.00	0.00	0.00	0.00	0.00	
Total		16.25	0.00	23.17	4.64	0.00	
Total of	f All Source Area	s		44.06			
Total of	f All Source Area	S					

Particulate Solids Concentration file name: MILW11.PSC

Area (

Pollutant Relative Concentration file name: MILW.POL

Study period ending date: 12/31/82

Time: 14:25:37

Source Area Control Practice Information

Residential Areas

Roofs 1 Source area number: 1

The roof is pitched

less All Isolated Areas

The Source Area is directly connected or draining to a directly connected area

44.06 =======

Roofs 2 Source area number: 2

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are present

Unpaved Parking/Storage 1 Source area number: 9

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are present

Driveways 1 Source area number: 13

The Source Area is directly connected or draining to a directly connected area

Sidewalks/Walks 1 Source area number: 16

The Source Area is directly connected or draining to a directly connected area

```
Source area number: 17
  Sidewalks/Walks 2
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is C/D
        The building density is medium or high
        Alleys are present
                  Source area number: 18
  Street Area 1
           1. Street Texture: intermediate
           Total study area street length (curb-miles): .69
           Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 04/15/80
                                              Schedule: Every 4 weeks (Wed)
                                              Schedule: None
                Begin cleaning on: 11/01/80
                Begin cleaning on: 03/18/81
                                              Schedule: Every 4 weeks (Wed)
                Begin cleaning on: 11/14/81
                                              Schedule: None
                                              Schedule: Every 4 weeks (Wed)
                Begin cleaning on: 04/01/81
                Final cleaning period ending date: 10/15/82
           2. Street cleaner productivity: Default
           3. Parking density: Medium
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept): 220
  Street Area 2
                 Source area number: 19
           1. Street Texture: smooth
           2. Total study area street length (curb-miles): .12
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                                             Schedule: Every 4 weeks (Wed)
                Begin cleaning on: 04/15/80
                Begin cleaning on: 11/01/81
                                              Schedule: None
                                              Schedule: Every 4 weeks (Wed)
                Begin cleaning on: 03/18/81
                Begin cleaning on: 11/14/81
                                              Schedule: None
                Begin cleaning on: 04/01/82
                                              Schedule: Every 4 weeks (Wed)
                Final cleaning period ending date: 10/15/82
           2. Street cleaner productivity: Default
           3. Parking density: Medium
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           Equation coefficient B (intercept):
  Smil Lndscpd Area 1 Source area number: 24
        The SCS Hydrologic Soil Type is C/D
Commercial Areas
             Source area number: 61
  Roofs 1
        The roof is flat
        The Source Area is directly connected or draining to a directly conntected area
  Paved Parking/Storage 1 Source area number: 66
        The Source Area is directly connected or draining to a directly conntected area
  Unpaved Parking/Storage 1 Source area number: 69
         The Source Area is directly connected or draining to a directly conntected area
   Sidewalks/Walks 1 Source area number: 76
         The Source Area is directly connected or draining to a directly conntected area
   Sidewalks/Walks 2 Source area number: 77
        The Source Area is directly connected or draining to a directly conntected area
   Street Area 1 Source area number: 78
            1. Street Texture: intermediate
            2. Total study area street length (curb-miles): 2.75

    Initial Street Dirt Loading (lbs/curb-mi): default value
    Street Dirt Accumulation:

                 Default value used
     Control Practice: Street Cleaning
            1. Street cleaning schedule:
                Begin cleaning on: 04/15/80
                                               Schedule: 1 Pass/week (Wed)
                                               Schedule: None
                 Begin cleaning on: 11/01/80
                                               Schedule:
                                                         1 Pass/week (Wed)
                 Begin cleaning on: 03/18/81
                Begin cleaning on: 11/14/81
                                               Schedule: None
                                               Schedule: 1 Pass/week (Wed)
                 Begin cleaning on: 04/01/82
                 Final cleaning period ending date: 11/15/82
            2. Street cleaner productivity: Default
            3. Parking density: Medium
            4. Parking controls imposed? No
            5. Equation coefficient M (slope):
            6. Equation coefficient B (intercept): 220
   Street Area 2
                  Source area number: 79
            1. Street Texture: smooth
```

2. Total study area street length (curb-miles): .48

```
Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
            1. Street cleaning schedule:
                                                Schedule: 1 Pass/week (Wed)
Schedule: None
                Begin cleaning on: 04/15/80
                 Begin cleaning on: 11/01/80
                Begin cleaning on: 03/18/81
                                                Schedule: 1 Pass/week (Wed)
                                                Schedule: None
                 Begin cleaning on: 11/14/81
                 Begin cleaning on: 04/01/82
                                                Schedule: 1 Pass/week (Wed)
                Final cleaning period ending date: 10/15/82
           2. Street cleaner productivity: Default
           3. Parking density: Medium
4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept): 70
  Smil Lndscpd Area 1 Source area number: 84
        The SCS Hydrologic Soil Type is C/D
Industrial Areas
  Roofs 1
            Source area number: 91
        The roof is flat
         The Source Area is directly connected or draining to a directly conntected area
                              Source area number: 96
  Paved Parking/Storage 1
        The Source Area is directly connected or draining to a directly connected area
  Sidewalks/Walks 1
                      Source area number: 106
        The Source Area is directly connected or draining to a directly connected area
  Street Area 1 Source area number: 108
            1. Street Texture: intermediate
           2. Total study area street length (curb-miles): .193. Initial Street Dirt Loading (lbs/curb-mi): default value
            4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
            1. Street cleaning schedule:
                                                Schedule: 1 Pass/week (Wed)
Schedule: None
                 Begin cleaning on: 04/15/80
                 Begin cleaning on: 11/01/80
                 Begin cleaning on: 03/18/81
                                                Schedule: 1 Pass/week (Wed)
                 Begin cleaning on: 11/15/81
                                                Schedule: None
                 Begin cleaning on: 04/01/82
                                                Schedule: 1 Pass/week (Wed)
                 Final cleaning period ending date: 10/15/82
            Street cleaner productivity: Default
            3. Parking density: Extensive (short term
            4. Parking controls imposed? No
            5. Equation coefficient M (slope):
            6. Equation coefficient B (intercept): 260
  Street Area 2 Source area number: 109
            1. Street Texture: smooth
            2. Total study area street length (curb-miles): .03
               Initial Street Dirt Loading (lbs/curb-mi): default value
               Street Dirt Accumulation:
                  Default value used
     Control Practice: Street Cleaning
            1. Street cleaning schedule:
                 Begin cleaning on: 04/15/80
                                              Schedule: 1 Pass/week (Wed)
                                                Schedule: None
Schedule: 1 Pass/week (Wed)
                 Begin cleaning on: 11/01/80
                 Begin cleaning on: 03/18/81
                 Begin cleaning on: 11/14/81
                                                Schedule: None
                 Begin cleaning on: 04/01/82
                                                Schedule: 1 Pass/week (Wed)
                 Final cleaning period ending date: 10/15/82
            2. Street cleaner productivity: Default
            3. Parking density: Extensive (short term
            4. Parking controls imposed? Extensive (short term
            5. Equation coefficient M (slope): .68
            6. Equation coefficient B (intercept): 80
Catchbasin or Drainage Controls
      Control Practice 1: Catchbasin Cleaning Controls
```

- 1. Total sump volume (cubic feet)= 280
- 2. Area served by catchbasins (acres)= 44.06
- 3. Percent of sump volume full at beginning of study period= 0°%
- Number of times catchbasins cleaned each year= 0

### Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name Pollutant Type Residue Particulate

Data file name: WCEN103.DAT

Rain file name: WCEN90.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 12/01/89

Date: 11-30-1991

Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

Undeveloped roadside 0 Curb and Gutters, 'valleys', or sealed swales in:

3. Poor condition (or very flat) 0

4. Fair condition 0

5. Good condition (or very steep) 1

Site information: WCEN102.DAT W/ MILW11.PSC, MILW6.RSV, DELIV2.PRR
Areas for each Source (acres)

	Resi- dential	tional	Commercial Areas	Industrial Areas	Spaces				
Source Area	Areas	Areas		,	Areas				
Roofs 1	2.74	0.00	4.24	1.20	0.00				
Roofs 2	1.89	0.00	0.00	0.00	0.00				
Roofs 3	0.00	0.00	0.00	0.00	0.00				
Roofs 4	0.00	0.00	0.00	0.00	0.00				
Roofs 5	0.00	0.00	0.00	0.00	0.00				
Paved Parking/Storage	0.00	0.00	4.66	2.73	0.00				
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00				
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00				
Unpaved Parking/Storag	0.90	0.00	0.89	0.00	0.00				
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00				
Playground 1	0.00	0.00	0.00	0.00	0.00				
Playground 2	0.00	0.00	0.00	0.00	0.00				
Driveways 1	0.68	0.00	0.00	0.00	0.00				
Driveways 2	0.00	0.00	0.00	0.00	0.00				
Driveways 3	0.00	0.00	0.00	0.00	0.00				
Sidewalks/Walks 1	0.21	0.00	3.08	0.21	0.00				
Sidewalks/Walks 2	0.21	0.00	0.10	0.00	0.00				
Street Area 1	. 2.00	0.00	7.90	0.43	0.00				
Street Area 2	0.00	0.00	1.40	0.07	0.00				
Street Area 3	0.00	0.00	0.00	0.00	0.00				
Lrg Lndscpd Area 1	0.00	0.00	0.00	0.00	0.00				
Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00				
Undeveloped Area	0.00	0.00	0.00	0.00	0.00				
Smll Lndscpd Area 1	7.27	0.00	0.90	0.00	0.00				
Smil Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00				
Smll Lndscpd Area 3	0.00	0.00	0.00	0.00	0.00				
Isolated Area	0.00	0.00	0.00	0.00	0.00				
Other Pervious Area	0.00	0.00	0.00	0.00	0.00				
Other Directly Connect	0.00	0.00	0.00	0.00	0.00				
Other Partially Connec	0.00	0.00	0.00	0.00	0.00				
Total	15.90	0.00	23.17	4.64	0.00				
Total of All Source Areas	S		43.71	•					
Total of All Source Areas			43.71	,					
tess att isotated a		43./1							

Source Area Control Practice Information

Residential Areas

Roofs 1 Source area number: 1

The roof is pitched

The Source Area is directly connected or draining to a directly conntected area

Roofs 2 Source area number: 2

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are present

Unpaved Parking/Storage 1 Source area number: 9

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are present

Driveways 1 Source area number: 13

The Source Area is directly connected or draining to a directly connected area

Sidewalks/Walks 1 Source area number: 16

The Source Area is directly connected or draining to a directly connected area Sidewalks/Walks 2 Source area number: 17

Pollutant Relative Concentration file name: MILW.POL Study period ending date: 12/31/90

Particulate Solids Concentration file name: MILW11.PSC

Time: 14:26:34

Area (

Paved Lane & Shoulder Area 1 Paved Lane & Shoulder Area 2 Paved Lane & Shoulder Area 3

Paved Lane & Shoulder Area 4 Paved Lane & Shoulder Area 5

Large Turf Areas Undeveloped Areas

Freeway Source Area

Other Pervious Areas Other Directly Connected Imperv Area Other Partially Connected Imperv Area

Total

```
The Source Area is draining to a pervious area (partially connected impervious area)
         The SCS Hydrologic Soil Type is C/D
         The building density is medium or high
         Alleys are present
   Street Area 1
                   Source area number: 18
            1. Street Texture: intermediate
            2. Total study area street length (curb-miles): .69
            3. Initial Street Dirt Loading (lbs/curb-mi): default value
            4. Street Dirt Accumulation:
                  Default value used
      Control Practice: Street Cleaning
            1. Street cleaning schedule:
                 Begin cleaning on: 04/15/90
                                               Schedule: Every 4 weeks (Wed)
                 Final cleaning period ending date: 10/15/90
            2. Street cleaner productivity: Default

    Parking density: Medium
    Parking controls imposed? No

            5. Equation coefficient M (slope):
            6. Equation coefficient B (intercept): 220
   Smil Lndscpd Area 1 Source area number: 24
         The SCS Hydrologic Soil Type is C/D
Commercial Areas
   Roofs 1
              Source area number: 61
         The roof is flat
         The Source Area is directly connected or draining to a directly connected area
   Paved Parking/Storage 1
                             Source area number: 66
         The Source Area is directly connected or draining to a directly conntected area
   Unpaved Parking/Storage 1
                               Source area number: 69
         The Source Area is directly connected or draining to a directly connected area
   Sidewalks/Walks 1 Source area number: 76
         The Source Area is directly connected or draining to a directly connected area
   Sidewalks/Walks 2 Source area number: 77
         The Source Area is directly connected or draining to a directly connected area
   Street Area 1
                   Source area number: 78

    Street Texture: intermediate

            Total study area street length (curb-miles): 2.75
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
            4. Street Dirt Accumulation:
                 Default value used
      Control Practice: Street Cleaning
            1. Street cleaning schedule:
                Begin cleaning on: 04/15/90
                                               Schedule: 1 Pass/week (Wed)
                 Final cleaning period ending date: 11/15/90
            2. Street cleaner productivity: Default
           3. Parking density: Medium
            4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept): 220
   Street Area 2 Source area number: 79
           1. Street Texture: smooth
           2. Total study area street length (curb-miles): .48
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
      Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 04/15/90
                                              Schedule: 1 Pass/week (Wed)
                Final cleaning period ending date: 10/15/90
           2. Street cleaner productivity: Default
           3. Parking density: Medium
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept): 70
  Smil Lndscpd Area 1 Source area number: 84
        The SCS Hydrologic Soil Type is C/D
Industrial Areas
             Source area number: 91
        The roof is flat
        The Source Area is directly connected or draining to a directly conntected area
  Paved Parking/Storage 1 Source area number: 96
        The Source Area is directly connected or draining to a directly conntected area
  Sidewalks/Walks 1
                     Source area number: 106
        The Source Area is directly connected or draining to a directly conntected area
```

Street Area 1 Source area number: 108

1. Street Texture: intermediate

4. Street Dirt Accumulation:

Total study area street length (curb-miles): .19
 Initial Street Dirt Loading (lbs/curb-mi): default value

Default value used Control Practice: Street Cleaning 1. Street cleaning schedule: Schedule: 1 Pass/week (Wed) Begin cleaning on: 04/15/90 Final cleaning period ending date: 10/15/90 2. Street cleaner productivity: Default 3. Parking density: Extensive (short term 4. Parking controls imposed? No 5. Equation coefficient M (slope): 6. Equation coefficient B (intercept): 260 Street Area 2 Source area number: 109 1. Street Texture: smooth Total study area street length (curb-miles): .03
 Initial Street Dirt Loading (lbs/curb-mi): default value
 Street Dirt Accumulation: Default value used

Control Practice: Street Cleaning

1. Street cleaning schedule: Begin cleaning on: 04/15/90 Schedule: 1 Pass/week (Wed) Final cleaning period ending date: 10/15/90 2. Street cleaner productivity: Default

W C-101- 11

3. Parking density: Extensive (short term

4. Parking controls imposed? Extensive (short term

5. Equation coefficient M (slope): .68

6. Equation coefficient B (intercept): 80

### Catchbasin or Drainage Controls

Control Practice 1: Catchbasin Cleaning Controls

1. Total sump volume (cubic feet)= 280

Area served by catchbasins (acres)= 43.71
 Percent of sump volume full at beginning of study period= 0 %

4. Number of times catchbasins cleaned each year= 0

### Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name Pollutant Type Particulate Residue

Data file name: MONROE00.DAT Rain file name: MONROE92.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 04/01/91

Date: 11-30-1991

Study period ending date: 07/09/91

Particulate Solids Concentration file name: MILW11.PSC Pollutant Relative Concentration file name: MILW.POL

Area (

Time: 14:26:47

Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

Undeveloped roadside .18

Curb and Gutters, 'valleys', or sealed swales in:

3. Poor condition (or very flat) 0

4. Fair condition 0

5. Good condition (or very steep) .82

Site information: MONROE2.DAT W/ MILW6.RSV, MILW11.PSC, DELIV2.PRR Areas for each Source (acres)

	Source Area	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas	Freeway Source Area
	Roofs 1	0.59	0.95	1.46	0.00	0.00	Paved Lane & Shoulder Area 1
	Roofs 2	0.15	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 2
	Roofs 3	0.50	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 3
	Roofs 4	27.03	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 4
	Roofs 5	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 5
	Paved Parking/Storage	0.46	0.20	-3.16	0.00	0.00	Large Turf Areas
	Paved Parking/Storage	0.00	0.21	0.00	0.00	0.00	Undeveloped Areas
	Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Other Pervious Areas
٠	Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Directly Connected Imperv Area
	Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Partially Connected Imperv Area
	Playground 1	0.00	0.00	0.00	0.00	0.00	•
	Playground 2	0.00	0.00	0.00	0.00	0.00	Total
	Driveways 1	7.73	0.00	0.00	0.00	0.00	
	Driveways 2	3.42	0.00	0.00	0.00	0.00	
	Driveways 3	0.00	0.00	0.00	0.00	0.00	· ·
	Sidewalks/Walks 1	3.04	0.00	0.08	0.00	0.00	
	Sidewalks/Walks 2	3.04	0.00	0.00	0.00	0.00	
	Street Area 1	11.79	0.00	1.62	0.00	0.00	*
	Street Area 2	20.16	0.00	0.83	0.00	0.00	
	Street Area 3	0.00	0.00	0.00	0.00	0.00	
	ing indscpd Area 1	21.19	0.00	0.00	0.00	0.00	
	Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00	
	Undeveloped Area	0.00	0.00	0.00	0.00	0.00	
	Smll Lndscpd Area 1	131.47	0.00	0.00	0.00	0.00	
	Smll Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00	
	Smil Lndscpd Area 3	0.00	0.00	0.00	0.00	0.00	
	Isolated Area	0.00	0.00	0.00	0.00	0.00	
	Other Pervious Area	5.86	0.00	0.00	0.00	0.00	
	Other Directly Connect	0.00	0.00	0.00	0.00	0.00	
	Other Partially Connec	0.00	0.00	0.00	0.00	0.00	
	Total	236.43	1.36	7.15	0.00	0.00	

Total of All Source Areas

244.95

Total of All Source Areas

less All Isolated Areas

244.95 =======

### Source Area Control Practice Information

Residential Areas

Roofs 1 Source area number: 1

The roof is flat

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is A/B

Source area number: 2

The roof is flat

The Source Area is directly connected or draining to a directly conntected area

Roofs 3 Source area number: 3

The roof is pitched

The Source Area is directly connected or draining to a directly conntected area

Roofs 4 Source area number: 4

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is A/B

Paved Parking/Storage 1 Source area number: 6

The Source Area is directly connected or draining to a directly connected area

Driveways 1 Source area number: 13

The Source Area is directly connected or draining to a directly conntected area

```
Drivewavs 2
                 Source area number: 14
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is A/B
  Sidewalks/Walks 1 Source area number: 16
        The Source Area is directly connected or draining to a directly connected area
  Sidewalks/Walks 2 Source area number: 17
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is A/B
  Street Area 1
                   Source area number: 18

    Street Texture: intermediate
    Total study area street length (curb-miles): 4.66

           3. Initial Street Dirt Loading (lbs/curb-mi): default value
            4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
            1. Street cleaning schedule:
                Begin cleaning on: 04/01/91
                                                Schedule: Every 4 weeks (Wed)
                 Final cleaning period ending date: 11/15/91
            2. Street cleaner productivity: Default
            3. Parking density: Light
            4. Parking controls imposed? No
            5. Equation coefficient M (slope): 9.000001E-02
            6. Equation coefficient B (intercept): 580
  Street Area 2
                 Source area number: 19
            1. Street Texture: intermediate
            2. Total study area street length (curb-miles): 11.12

    Initial Street Dirt Loading (lbs/curb-mi): default value
    Street Dirt Accumulation:

                 Default value used
     Control Practice: Street Cleaning
            1. Street cleaning schedule:
                                                Schedule: Every 4 weeks (Wed)
                 Begin cleaning on: 04/01/91
                 Final cleaning period ending date: 11/15/91
            2. Street cleaner productivity: Default
            3. Parking density: Light
            4. Parking controls imposed? No

    Equation coefficient M (slope): 9.000001E-02

            6. Equation coefficient B (intercept):
                       Source area number: 21
  Lrg Lndscpd Area 1
         The SCS Hydrologic Soil Type is A/B ndscpd Area 1 Source area number: 24
  Smil Lndscpd Area 1
         The SCS Hydrologic Soil Type is A/B
                         Source area number: 28
  Other Pervious Area
         The SCS Hydrologic Soil Type is A/B
Institutional Areas
   Roofs 1
              Source area number: 31
         The roof is flat
         The Source Area is directly connected or draining to a directly conntected area
                            Source area number: 36
   Paved Parking/Storage 1
         The Source Area is draining to a pervious area (partially connected impervious area)
         The SCS Hydrologic Soil Type is A/B
                              Source area number: 37
   Paved Parking/Storage 2
         The Source Area is directly connected or draining to a directly conntected area
Commercial Areas
  Roofs 1 Source area number: 61
         The roof is flat
         The Source Area is directly connected or draining to a directly conntected area
                              Source area number: 66
   Paved Parking/Storage 1
         The Source Area is directly connected or draining to a directly conntected area
   Sidewalks/Walks 1 Source area number: 76
         The Source Area is directly connected or draining to a directly connected area
   Street Area 1 Source area number: 78
            1. Street Texture: smooth

    Total study area street length (curb-miles): .56
    Initial Street Dirt Loading (lbs/curb-mi): default value

            4. Street Dirt Accumulation:
                  Default value used
      Control Practice: Street Cleaning
            1. Street cleaning schedule:
                                                 Schedule: 1 Pass/week (Wed)
                 Begin cleaning on: 04/01/91
                 Final cleaning period ending date: 11/15/91
            2. Street cleaner productivity: Default
            3. Parking density: Light
            4. Parking controls imposed? No
            5. Equation coefficient M (slope):
                                                  .45
            6. Equation coefficient B (intercept): 125
```

Source area number: 79

1. Street Texture: intermediate

Street Area 2

2. Total study area street length (curb-miles): .36

Initial Street Dirt Loading (lbs/curb-mi): default value
 Street Dirt Accumulation:

Default value used Control Practice: Street Cleaning

1. Street cleaning schedule:

Begin cleaning on: 04/01/91 Schedule: Every 4 weeks (Wed) Final cleaning period ending date: 11/15/91

2. Street cleaner productivity: Default
3. Parking density: Light
4. Parking controls imposed? No
5. Equation coefficient M (slope): .3

6. Equation coefficient B (intercept): 450

Catchbasin or Drainage Controls

Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name

Pollutant Type

Residue

Particulate

Data file name: SYENEOO.DAT Rain file name: SYEN91V2.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 04/01/91

Date: 11-30-1991

Time: 14:27:09

Pollutant Relative Concentration file name: MILW.POL

Area (

Study period ending date: 07/09/91

Particulate Solids Concentration file name: MILW11.PSC

Freeway Source Area

Large Turf Areas Undeveloped Areas Other Pervious Areas

Total

Paved Lane & Shoulder Area 1 Paved Lane & Shoulder Area 2 Paved Lane & Shoulder Area 3 Paved Lane & Shoulder Area 4 Paved Lane & Shoulder Area 5

Other Directly Connected Imperv Area Other Partially Connected Imperv Area

Fraction of each type of Drainage System serving study area:

1. Grass Swales 0

2. Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in:

3. Poor condition (or very flat) 0

4. Fair condition .25

5. Good condition (or very steep) .75

Site information: SYENE7.DAT W/ STREET 2 SMOOTH INSTEAD OF INTERMEDIATE Areas for each Source (acres)

Source Area	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas	
Roofs 1	0.00	0.00	0.00	6.91	0.00	
Roofs 2	0.00	0.00	0.00	0.70	0.00	
Roofs 3	0.00	0.00	0.00	10.41	0.00	
Roofs 4	0.00	0.00	0.00	6.10	0.00	
Roofs 5	0.00	0.00	0.00	0.00	0.00	
Paved Parking/Storage	0.00	0.00	0.00	30.84	0.00	
Paved Parking/Storage	0.00	0.00	0.00	2.46	0.00	
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	
Unpaved Parking/Storag	0.00	0.00	0.00	4.53	0.00	
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	
Playground 1	0.00	0.00	0.00	0.00	0.00	
Playground 2	0.00	0.00		0.00	0.00	
Driveways 1	0.00	0.00	0.00	0.70	0.00	
Driveways 2	0.00	0.00	0.00	0.08	0.00	
Driveways 3	0.00	0.00	0.00	0.00	0.00	
Sidewalks/Walks 1	0.00	0.00	0.00	0.00	0.00	
Sidewalks/Walks 2	0.00	0.00	0.00	0.00	0.00	
Street Area 1	0.00	0.00	0.00	1.33	0.00	
Street Area 2	0.00	0.00	0.00	1.23	0.00	
Street Area 3	0.00	0.00	0.00	6.09	0.00	
Lrg Lndscpd Area 1	0.00	0.00	0.00	0,00	0.00	
Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00	
Undeveloped Area	0.00	0.00	0.00	0.00	0.00	
Smil Lndscpd Area 1	0.00	0.00	0.00	22.17	0.00	
Smll Lndscpd Area 2	0.00	0.00	0.00	22.17	0.00	
Smll Lndscpd Area 3	0.00	0.00	0.00	0.00	0.00	
Isolated Area	0.00	0.00	0.00	0.00	0.00	
Other Pervious Area	0.00	0.00	0.00-	0.00	0.00	
Other Directly Connect	0.00	0.00	0.00	0.00	0.00	
Other Partially Connec	0.00	0.00	0.00	0.00	0.00	
Total	0.00	0.00	0.00	115.72	0.00	

Total of All Source Areas

Total of All Source Areas

less All Isolated Areas

115.72

115.72

### Source Area Control Practice Information

Industrial Areas

Roofs 1 Source area number: 91

The roof is flat

The Source Area is directly connected or draining to a directly conntected area

Source area number: 92 Roofs 2

The roof is flat

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are not present

Roofs 3 Source area number: 93

The roof is pitched

The Source Area is directly connected or draining to a directly conntected area

Source area number: 94

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is medium or high

Alleys are not present

```
Paved Parking/Storage 1
                            Source area number: 96
        The Source Area is directly connected or draining to a directly conntected area
  Paved Parking/Storage 2 Source area number: 97
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is C/D
        The building density is medium or high
        Alleys are not present
  Unpaved Parking/Storage 1 Source area number: 99
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is C/D
        The building density is medium or high
        Alleys are not present
                Source area number: 103
  Driveways 1
        The Source Area is directly connected or draining to a directly conntected area
  Driveways 2 Source area number: 104
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is C/D
        The building density is medium or high
        Alleys are not present
  Street Area 1 Source area number: 108
           1. Street Texture: intermediate
           2. Total study area street length (curb-miles): .5
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 04/01/91
                                               Schedule: Every 2 weeks (Wed)
                Final cleaning period ending date: 11/15/91
           2. Street cleaner productivity: Default
           3. Parking density: Light
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept): 450
  Street Area 2 Source area number: 109
           1. Street Texture: smooth
           2. Total study area street length (curb-miles): .5.
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning

    Street cleaning schedule:

                Begin cleaning on: 04/01/91
                                              Schedule: Every 2 weeks (Wed)
                Final cleaning period ending date: 11/15/91
           2. Street cleaner productivity: Default
           3. Parking density: Light
4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           Equation coefficient B (intercept): 170
  Street Area 3
                 Source area number: 110
           1. Street Texture: smooth
           2. Total study area street length (curb-miles): 2.95

    Initial Street Dirt Loading (lbs/curb-mi): default value
    Street Dirt Accumulation:

                 Default value used
     Control Practice: Street Cleaning

    Street cleaning schedule:

                Begin cleaning on: 04/15/91
                                               Schedule: Every 2 weeks (Wed)
                 Final cleaning period ending date: 11/15/91
           2. Street cleaner productivity: Default
           3. Parking density: Light
           4. Parking controls imposed? No
           5. Equation coefficient M (slope): .27
           6. Equation coefficient B (intercept):
  Smil Lndscpd Area 1
                        Source area number: 114
         The SCS Hydrologic Soil Type is A/B
                       Source area number: 115
  Smll Lndscpd Area 2
         The SCS Hydrologic Soil Type is C/D
Catchbasin or Drainage Controls
```

Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name Pollutant Type Residue Particulate

**A2** 

Parameter Files

```
Runoff Coefficient file name: MILWOO.RSV
Runoff Coefficient file description: CALIBRATED 12/6/91 FROM MILWAUKEE AND MADISON DATA
Date: 12-06-1991
    Area Types:
 1: Connected flat roofs
 2: Connected Pitched Roofs
 3: Directly connected impervious areas
 4: Directly connected unpaved areas
5: Pervious areas - A/B soils
6: Pervious areas - C/D soils
```

```
Drainage efficiency coefficients (fractions)
10: C/D soils, w/o alleys, medium to high density land use
```

7: Smooth textured streets 8: Intermediate textured streets 9: Rough textured streets

11: C/D soils, w/ alleys, medium to high density land use

12: C/D soils for strip commercial and shopping center land use

```
Volumetric Runoff Coefficients for Rains (in & mm)
        in: .04 .08 .12 .20 .39 .59 .79 .98 1.2 1.6 2.0 2.4 2.8 3.2 3.5 3.9 4.9 mm: 1 2 3 5 10 15 20 25 30 40 50 60 70 80 90 100 125 Rain #: 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17
Area
Type
       Rain #: 1
                 .00 .15 .45 .64 .77 .79 .83 .84 .86 .88 .90 .91 .93 .94 .94 .95 .96 .25 .63 .75 .85 .93 .95 .96 .97 .98 .98 .99 .99 .99 .99 .99 .99
 1:
 2:
                 .50 .72 .75 .82 .90 .92 .93 .94 .94 .95 .96 .96 .96 .96 .96 .96
 3:
                 .00 .00 .00 .00 .47 .64 .72 .77 .81 .86 .89 .91 .92 .93 .94 .94 .95 .00 .00 .00 .00 .01 .02 .02 .03 .04 .07 .10 .13 .15 .20 .22 .25
 5:
                 .00 .00 .00 .10 .15 .19 .20 .21 .22 .23 .26 .29 .32 .33 .36 .39 .45
                 .35 .49 .54 .59 .65 .69 .72 .76 .80 .85 .88 .90 .91 .93 .93 .94 .95 .26 .43 .49 .55 .60 .64 .67 .70 .73 .80 .84 .86 .88 .90 .91 .92 .93
 8:
                 .18 .39 .47 .53 .60 .64 .67 .70 .73 .80 .84 .86 .88 .90 .91 .92 .93
Drainage efficiency coefficients (fractions):
10: .00.00.00.11.16.20.21.22.22.24.27.30.33.34.37.40.46
                 .00 .05 .12 .22 .53 .73 .85 .92 .96 .99 %1.00
11 :
                                                                                %1.00
                                                                                      %1.00
                                                                                           %1.00
                                                                                                 %1.00
                                                                                                             %1.00
12 :
```

Particulate Solids Concentration file name: MILW00.PSC Particulate Solids Concentration file description: CALIBRATED 12/6/91 FROM MILWAUKEE AND MADISON DATA Date: 12-06-1991

### Area Types:

- : Roofs
- : Paved Parking
- : Unpaved parking, driveways, and walkways С
- : Paved playgrounds
- : Paved driveways
- : Paved sidewalks and walks
- : Large landscaped areas : Small landscaped areas
- : Undeveloped areas
- J : Other pervious areas
- K : Other directly connected impervious areas
- L : Other partially connected impervious areas
- M : Paved lane and shoulder areas

	Particulate Residue (mg/l) for Rains (in & mm)															
	i I		Par	ticul	ate R	tesidu	e (mg,	/l) f	or Ra	ins (	in & I	mm)		•		1.5
Row	Area	.04	.08	.12	.20	.39	.59	.79	.98	1.2	1.6	2.0	2.4	2.8	3.2	:in
No	Type	1	2	3	5	10	15	20	25	30	40	50	60	70	80	: mm
	וייירי	i	2	3	4	5	6	7	- 8	9	10	11	12	13	14	:Rain #
	1 1	•	~	3	. *		0	٠.			10					
_		_														
Resi	dential	Areas														
- 1	A	12	12	12	12	12	12	12	12	. 12	12	12	12	12	12	
. 2	В .	991	528	357	201	77	57	57	57	57	57	57	57	57	-57	
3	Č	440	440	440	440	440	440	377	377	377	377	377	377	377	377	
														57	57	
4	D	126	126	126	126	77	57	57	57	57	57	57	57			
- 5	Ę	276	276	276	201	77	57	57	57	57	57	57	57	57	57	
6	F	12	12	12	12	12	12	12	12	- 12	12	12	12	12	12	
7	G	63	63	63	63	63	63	63	63	63	63	63	63	63	63	
						63	63	63	63	63	63	63	63	63	63	•
8	H	63	. 63	63	63											
9	I	250	250	250	250	250	250	250	250	250	250	250	250	250	250	
- 10	J	158	158	158	158	158	158	158	158	158	158	158	158	158	158	
11	K	991	528	357	201	77	57	57	57	57	57	57	57	57	57	
					201	77	57	57	57	57	57	57	57	57		
12	· L	991	528	357	201	,,		31	"	- 71	31	٠,٠	٠,٠	٠,,		
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13	Α	5	5	5	5	5	5	5	5.	5	5	5	5	5	5	
. 14	В	1630	870	586	332	127	95	95	95	95	95	95	95	95	95	
		800	800	800	800	800	700	600	600	600	600	600	600	600	600	
. 15	C															
. 16	D	1581	844	568,		123	92	92	92	92	92	92	92	92	92	
17	Ε	400	400	400	322	123	92	92	92	92	92	92	92	92	92	
18	F	50	50	50	50	50	50	50	50	50	50	50	50	50	50	
19	Ġ	300	300	300	300	300	300	300	300	300	300	300	300	300	300	
					300	300	300	300	300	300	300	300	300	300	300	
20	, H	300	300	300												
21	I	500	500	500	500	500	500	500	500	500	500	500	500	500	500	
22	J	250	250	250	250	250	250	250	250	250	250	250	250	250	250	
23	ĸ	1630	870	586	332	127	95	95	95	95	95	95	95	95	95	
						127	95	95	95	95	95	95	95	95	95	
24	L	1630	870	586	332	121	70	70	72	73	73	73	73	73	7.3	
Comm	ercial	Areas														
25	A	5	- 5	5	5	5	5	5	5 .	5	5 -	5	5	5	5	
26	В	1630	870	586	332	127	95	95	95	95	95	95	95	95	95	
27				5000			1000	700	600	600	600	600	600	600	600	
	C															
28	D	1581	844	568	322	123	92	92	92	92	92	92	92	92	92	
29	Ε	400	400	400	322	123	92	92	92	92	92	92	92	92	92	
30	F	50	50	50	50	50	50	50	50	50	50	50	50	50	50	
31	G	300	300	300	300	300	300	300	300	300	300	300	300	300	300	
32	H		300	300	300	300	300	300	300	300	300	300	300	300	300	
33	I			3300			700	600	600	600	600	600	600	600	600	
34	J	250	250	250	250	250	250	250	250	250	250	250	250	250	250	
35	K	1630	870	586	332	127	95	95	95	95	95	95	95	95	95	
36	L	1630	870	586	332	127	95	95	95	95	95	95	95	95	95	
50	-	.550	٥, ٥				,,									
الد ــ ۲	احتصفت	Ances														
	strial		_	<u>.</u>		_		_	_			_		_		
37	, А	5	5.	5	5	5	5	5	. 5	• 5	5	5	5		. 5	
38	В.	1630	870	586	332	127	95	95	95	95	95	95	95	95	95	
39	С			2500			500	350	300	300	300	300	300	300	300	
40	Ď	300	200	150	100	100	100	100	100	100	100	100	100	100	100	
				170												
41	E	300	200		100	100	100	100	100	100	100	100	100	100	100	Y
42	F	300	200		100	100	100	100	100	100	100	100	100	100	100	
43	G	300	300	300	300	300	300	300	300	300	300	300	300	300	300	
44	Ĥ	300	300			300	300		300	300	300	300	300		300	
45	ï	500	500		500		500	500	500	500	500	500	500	500	500	
			200	200	200	200		200	200							
46	j	250	250		250	250	250	250	250	250	250	250	250	250	250	
47	Κ.	300	200		100			100	100	100	100	100	100	100	100	
- 48	L	300	200	150	100	100	100	100	100	100	100	100	100	100	100	

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0	C	1													
	Space	Areas 5	5	5	5	5	5	5	5	5	5	5	5	5	5
49 50	A B	1630	870	586	332	127	95	95	95	95	95	95	95	95	95
51	C	2500	2500	2500	2200	1100	700	600	600	600	600	600	600	600	600
52	D	1581	844	568	322	123	92	92	92	92	92	92	92	92	92
53	E	400	400	400	322	123	92	92	92	92	92	92	92	92	92
54	F	50	50	50	50	50	50	50	50	50	50	50	50	50	50
55	Ġ	300	300	300	300	300	300	300	300	300	300	300	300	300	300
56	H	300	300	300	300	300	300	300	300	300	300	300	300	300	300
57	ï	500	500	500	500	500	500	500	500	500	500	500	500	500	500
58	J	250	250	250	250	250	250	250	250	250	250	250	250	250	250
59	K	1630	870	586	332	127	95	95	95	95	95	95	95	95	95
60	L	1630	870	586	332	127	95	95	95	95	95	95	95	95	95
Free	ways											•			
61	M	200	200	200	200	200	200	200	200	200	200	200	200	200	200
62	G	300	300	300	300	300	300	300	300	300	300	300	300	300	300
63	I	500	500	500	500	500	500	500	500	500	500	500	500	500	500
64	J	250	250	250	250	250	250	250	250	250	250	250	250	250	250
65	K	1630	870	586	332	127	95	95	95	95	95	95	95	95	95
66	L	1630	870	586	332	127	95	95	95	95	95	95	95	95	95

Particulate Residue Reduction due to Delivery file name: MILWOO.PRR Size distribution file description: CALIBRATED 12/6/91 FROM MADISON AND MILWAUKEE DATA Date: 12-06-1991

> Particulate Residue Reduction due to Delivery (fraction) for Rains (in & mm) Rain (in) : .04 .08 .12 .20 .39 .59 .79 .98 1.2 1.6 2.0 2.4 2.8 3.2 Rain (mm) : 1 2 3 5 10 15 20 25 30 40 50 60 70 80

For 1. Grass Swales:

0.99 0.98 0.97 0.94 0.85 0.74 0.61 0.44 0.25 0.07 0.02 0.00 0.00 0.00

For 2. Undeveloped roadside:

0.99 0.98 0.97 0.94 0.85 0.74 0.61 0.44 0.25 0.07 0.02 0.00 0.00 0.00

For 3. Curb and Gutters, 'valleys', or sealed swales in poor condition (or very flat): 0.98 0.96 0.92 0.85 0.61 0.46 0.31 0.22 0.13 0.04 0.01 0.00 0.00 0.00

For 3. Curb and Gutters, 'valleys', or sealed swales in fair condition: 0.98 0.95 0.90 0.80 0.48 0.32 0.16 0.11 0.07 0.02 0.00 0.00 0.00

Pollutant Relative Concentration file name: MILWOO.POL File description: CALIBRATED 12/6/91 FROM MILWAUKEE AND MADISON DATA Date: 12-06-1991

### Source Areas:

1: Roofs 2: Paved Parking/Storage

3: Unpaved Parking/Storage

4: Playground 5: Driveways

6: Sidewalks/Walks

7: Street Area

8: Large Landscaped Area

9: Undeveloped Area

10: Small Landscaped Area

11: Isolated Area

12: Other Pervious Area
13: Other Dir Conctd Imperv Area
14: Othr Partially Conctd Imperv Area

15: Paved Lane & Shoulder Area

16: Large Turf Areas

		l an	d Uses			Λ .
Source Area #	Resident- ial Areas	Institut- ional Areas	Commercial Areas	Industrial Areas	Open Spaces	Freeways
Particu	late Polluta	nt: Phospho	rus (mg/kg)			
1:	1600	1000	1000	1,600	1600	0
2:	580	2960	2960	580	580	0
3:	570	570	570	570	570	0
4:	500	500	500	500	500	0
5:	580	580	580	580	580	0
6:	995	995	995	995	995	0
7:	650	650	940	670	650	0
8:	2800	2800	2800	2800	2800	0
9:	695	695	695	695	695	695
10:	1250	1250	1250	1250	1250	0
11:	. 0	0	0	0	0	0
12:	1600	1600	1600	1600	1600	1600
13:	500	500	500	500	500	500
14:	500	500	500	500	500	500
15:	0	0	0	0	0	1000 2800
16:	0	0		0	0	2600
	late Polluta	nt: Chemica	l Oxygen Dem		913000	0
1:	913000	1520000	1520000	963000	512000	0
2:	512000	512000	1470000 695000	540000 733000	695000	0
3:	695000	695000 507000	507000	535000	507000	ŏ
4:	507000	507000	507000	535000	507000	Ŏ,
5:	512000 664000	659000	659000	701000	659000	ŏ
6:	304000	304000	1170000	428000	304000	ŏ
7:	1115000	1115000	1115000	1180000	1115000	ŏ
8 : 9 :	276000	276000	276000	292000	276000	284000
10:	507000	507000	507000	535000	507000	0
11:	0	0	0	0	0	0
12 :	761000	761000	761000	803000	761000	782000
13:	304000	304000 °	304000	321000	304000	313000
14	304000	304000	304000	321000	304000	313000
15 :	. 0	0	0	. 0	0	464000
16:	0	0	0	0 -	0	1150000
	ulate Polluta	ant: Copper	(mg/kg)			
1:	51	121	121	104	106	0
2:	87	87	87	60	139	0
3:	151	151	151	60	151	0
4:	82	82	82	249	82	0
5:	38	139	139	_35	139	0
6:	38	131	38	398	131	0
7:	20	375	70	58	375	0
8:	16	41	41	16	41 73	150
9:	73 14	73	73 14	224 16	73 16	0
10:	16	16 0	16 0	0.	. 0	0
11:	0	41	41	125	41	82
12:	16 82	82	82	249	82	165
13 : 14 :	82	82 82	82 82	249	82	165
15:	02	0	0	, <u>-</u> - 0	0	1100
16:	Ö	Ŏ	Ŏ	Ŏ	Ö	150
Partic	ulate Pollut			-		
1:	894	268	268	884	894	0
2 :	670	2240	2240	663	670	. 0
3:	429	429	429	424	429	0
4 :	447	447	447	442	447	0
5 :	671	671	671	663	671	0
6:	742	742	742	734	742	0
7:	740	983	3580	796	983	0
8:	241	241	241	239	271	0
9:	121	121	121	119	121	121
10:	. 45	45	- 45	45	45	0

11 12 13	: 134 : 447	0 134 447	0 134 447	0 134 447	0 134 447	0 134 447		
14 15	: 447 : 0	447 0	447 0	447 0	447 0	447 8630		
16 Pai	: 0 rticulate Pollutant	0 : Zinc	0 : (mg/kg)	0	0	240	•	
1 2	: 983 : 420	983 1070	894 1070	2860 2340	983 420	0 0		
3	: 264	264	264	767	264	Ō		* * * * * * * * * * * * * * * * * * *
5	: 268 : 420	268 420	268 420	780 1200	268 420	0		
6 7	: 773 : 384	773 447	. 773 876	2250 1300	773 384	0		
8	: 179 : 237	179	179	520	179	• 0		
10	: 103	237 103	237 103	. 689 300	237 103	450 0	<u>,                                      </u>	
11 12	: 0 : 179	0 179	0 179	0 520	0 179	0 340		
13 14	: 268 : 268	268 268	268 268	780 780	268	510		
15	: 0	0	0	0	268 0	510 1730		
16 Fil	:	0 Filte	o rable Residue (	(mg/L)	. 0	450		
1 2	: 116 : 223	386 223	386 223	148	116	0	•	
3	: 1240	1240	1240	157 585	223 1240	0		
5	: 223 : 223	223 223	223 223	105 105	223 223	. 0		ı
6 7	: 318 : 151	318 151	318 247	150 263	318 · 151	0		
8	: 861	861	861	406	861	0		
9 .10	: 846 : 861	846 861	846 861	400 406	846 861	627 0		•
11 12	: 0 : 861	0 861	0 861	0 - 406	0 861	0 638		•
13	: 223	223	223	105	223	165		•
14 15	: 223 : 0	223 0	223 0	105 0	22 <b>3</b> 0	165 352		
16 Fil	: 0 terable Pollutant:	0 Phosp	0 horus (Ìg/L)	0	0	638		
1	: 40 : 340	40	40	40	40	0		
3	: 40	340 40	130 40	1000 40	340 40	0		
4 5	: 100 : 100	100 100	100 100	100 100	100 100	0		
6	: 600	600	600	600	600	Ŏ		
8	: 390 : 220	390 220	410 220	470 220	390 220	0		
9 10	: 250 : 220	250 220	250 220	250 220	250 220	250 0		
11 12	: 0	0 220	0	0	0	0		
13	: 100	100	220 100	220 100	220 100	220 100		
14 15		100	100 0	100 0	100 0	100 400		
16		0	0 cal Oxygen Dema	Ō	Ŏ	220		•
1	: 23	84	84	38	23	0		
2	: 107	22 107	55 107	52 113	22 107	0		
4 5	: 17 : 22	17 22	17 22	17 22	17 22	0		10 m
6	: 22	. 22	22	22	22	0		
8	: 40 : 17	40 17	101 17	191 17	40 17	0		•
9 10	: 20 : 17	20 17	20 17	20 17	20 17	20 0		
11	: 0	0	0	0	0	0		
12 13	: 22	17 22	17 22	17 22	17 22	17 22		
14 15		22 0	22 0	22 0	22 0	22 78		
16		0	0	0	Ŏ	18		
1	: 5030	80	Coliform Bact.	5010	5030	0		•
2 3		100000 200000	48000 200000	9800 200000	100000 200000	0		
4 5	: 18000	18000 300000	18000 300000	18000 300000	18000 300000	0		
-			30000	500000	500000	U		

						•
6:	170000	170000	170000	170000	170000 43000	0 0
7:	43000	43000 30000	43000 30000	170000 30000	30000	ő
8:	30000 30000	30000	30000	30000	30000	30000
9:	30000	30000	30000	30000	30000	0
11:	0	0	0	0	0	0
12 :	30000	30000	30000	30000	30000	30000
13 :	18000	18000	18000	18000	18000	18000
14 :	18000	18000	18000	18000	18000	18000
15 :	0	0	0	0	0	43000
16:	. 0	_ 0	0	0	0	30000
	erable Pollutant:	Copper	(1g/L) 6	2	16	0
1:	3 4	4	.4	15	ő	ŏ
2:		47	47	.15	47	Ō
4:		0	Ö	0	0	0
5:		0	. 0	9	0 ,	0
6 :	4	16	4	50	16	0
7 :	4	0	8	18	0	0
8 :	6	0	0	6	0	0 0
9:	. 0	0	0	. 0 6	0	0
10:	: 3 : 0 ·	0	0	0	. 0	ŏ
11 : 12 :	3	0	ő	Ŏ	ŏ	Ō
13	_	Ŏ	Ō	. 0	0	0
14	0	Ō	. 0	0	0	0
15	0	0	´ 0	0	0	0
16:	0	0	0 -	0	0	0
	terable Pollutant:	Lead (		•	20	0
1 :	: 20	20	20 31	2 0	20 0	0
	: Q : O	0,	0	0	Ö	Ŏ
3 :	. 0	Ŏ	. 0	Ŏ	. 0	Õ
5	. 0	ŏ	Ŏ	0.	. 0	0
6	33	33	33	4	33	0
7	: 4	4	21	12	4	0 ′
8	: 3	3	3	0	3	0
9	: 4	4	4	0	4 3	2 0
10	: 3 : 0	. 3	3 0	0	- 0	ŏ
11 12	: U : 3	3	3	Ŏ	3	. 2
13	. 0	ő	Ō	Ö	Õ	0
14	. 0	Ŏ	Ŏ	0	0	0
15	: 0	0	0	0	0	130
16	: 0	0	. 0	0	0	2
	terable Pollutant:		Ìg/L)	. 75	268	0
1	: 268	165 134	165 122	35 110	134	0
2	: 134 : 134	134	134	87	134	ŏ
	: 134	27	27	17	27	0
5	134	134	134	87	134	0
6	: 27	27	27	17	· 27	0
7	: 72	72	97	237	72	0
8	: 3 : 22	3	. 3	·2	3 22	0 19
9	: 22	22	` 22 3	14	22	. 10
10	: 3 : 0	- 3 0	Õ	2	3 0	· ŏ
11 12	: 3	3	3	2	3	2
13	27	27	27	17	27	22
14	: 27	27	27	. 17	27	22
15	: 0	0	0	0	0	204
16	: 0	. 0	0	0	0	2
	terable Pollutant:				ML) 610	0
	18300	610 610	610 610	225 26100	610	Ŏ
3	: 610 : 6100	6100	6100	·63000	6100	0
4	: 610	610	610	610	610	0
5	: 367	610	610	64350	610	0
5 6	: 610	610	610	16200	610	0
7	: 348	348	367	27900	348	0
8	: 1280	1280	1280	9450	1280	5/40
9	: 1280	1280	1280	9450	1280 1280	5460 0
10	: 1280	1280 0	1280 0	9450 0	0	Ö
11 12	: 0 : 1280	1280	1280	9450	1280	5460
13	: 610	610	610	4500	611	2600
14	: 610	610	610	4500	611	2600
15	: 0	0	0	0	0	1560
16		, , 0	0	0	. 0	5460

## Appendix B

## **Calibration Results**

- **B1** Description of Tables and Graphs
- **B2** Post Office Study Area Results
- **B3** Rustler Study Area Results
- **B4** Hastings 1980-1982 Study Area Results
- **B5** Burbank Study Area Results
- **B6** State Fair Study Area Results
- B7 Wood Center 1980-1982 Study Area Results
- **B8** Hastings 1990 Study Area Results
- **B9** Wood Center 1990 Study Area Results
- **B10 Monroe Street Study Area Results**
- **B11 Syene Road Study Area Results**

**Description of Tables and Graphs** 

## **DESCRIPTION OF TABLES AND GRAPHS**

The following sections of this Appendix describe the results of the SLAMM model calibration for the ten runoff and suspended solids calibration data sets and the two copper calibration data sets. Each section contains the following information:

- A calibration result summary table.
- A spreadsheet presenting storm runoff data.
- Runoff calibration plots.
- A spreadsheet presenting suspended solids data.
- Suspended solids calibration plots.
- Copper data spreadsheets and plots (Monroe Street and Syene Road only).

The calibration results summary tables list descriptive statistics for both the runoff and the suspended solids results with delivery. The statistics listed on each table include the mean, the standard deviation, the coefficient of variation, the sum, and the count (number of storm data). The coefficient of variation (COV) (standard deviation divided by the mean) is a measure of the variation or "spread" of the data, and is used to compare the relative scatter of the observed data and the predicted data.

The detailed runoff data spreadsheet lists the observed and predicted runoff and RV values for each event in the data set. The RV is the runoff coefficient, which is defined as the event runoff divided by the event rainfall. The residual (observed value less predicted value) for each value is also listed in these tables. The data summary at the bottom of each table includes the maximum value, the minimum value, the count, the average, the standard deviation, the coefficient of variation, and the sum of the values. Following the spreadsheet, three runoff scatterplots are presented, illustrating the observed runoff vs. the predicted runoff, the predicted runoff vs. the runoff residual for each event.

The detailed suspended solids data spreadsheet lists the observed value, the predicted value without and with the reduction due to delivery at the outfall, and

the residual value without and with the reduction due to delivery at the outfall for each event in the data set. An asterisk next to a data value in the suspended solids tables indicates that the value was selected as an outlier. The data summary at the end of each table includes the maximum value, the minimum value, the count, the average, the standard deviation, the coefficient of variation, and the sum of the observed, predicted, and residual values, and also includes the sums and residuals of the total values less the indicated outliers. Three scatterplots following the suspended solids spreadsheet illustrate the observed suspended solids vs. the predicted suspended solids, predicted suspended solids vs. the suspended solids residual, and the rain depth vs. the suspended solids residual for each event.

The copper calibration results presented for the Monroe Street and Syene Road sites present event-by-event results for the outfall from each study area. The spreadsheet lists observed and predicted data for total, dissolved, and particulate copper at the outfall, followed by a scatterplot showing predicted vs. observed total copper loading values. Summary statistics are the same as for runoff and suspended solids, but also include the geometric mean of each form of copper.

[mad-603-34y]

Post Office Study Area Results

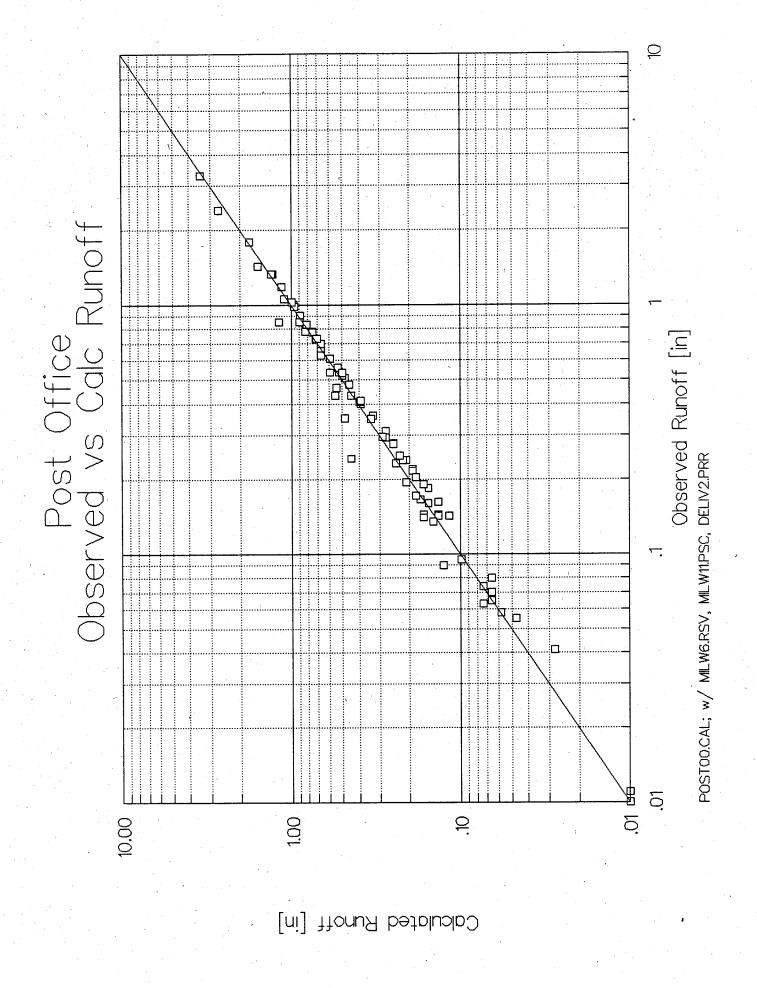
SLAMM Calibration Data Summary Sheet									
Site Data File Name: POS	STØØ. DAT								
Post Office	Observed	Predicted	Residuals						
Runoff [in]									
Average	0.52	0.53	-0.01						
Std Dev	0.53	0.56							
COV	1,03	1,07							
Sum	40.83	41.56	-0.73						
Count	79	•							
Runoff - outliers [in]									
Average	0.51	0.52	-0.01						
Std Dev	0,54	0.56							
COV	[.05	1,08	****						
Sum	39.99	40.75	-0,76						
Count	78								
Rv									
Average	0.87	0.85	0.02						
Std Dev	0.12	0.73	-						
COV	0.14	0.15	-						
SS w/Delivery [lbs]									
Average	128	114	14						
Std Dev	195	145							
COV	1,53	1.28							
Sum	10096	9001	1095						
Count	79								
SS w/Delivery - outliers [lbs]									
Average	113	113	0						
Std Dev	145	146							
COV	1.28	1,29							
Sum	808	8827	-19						
Count	78								

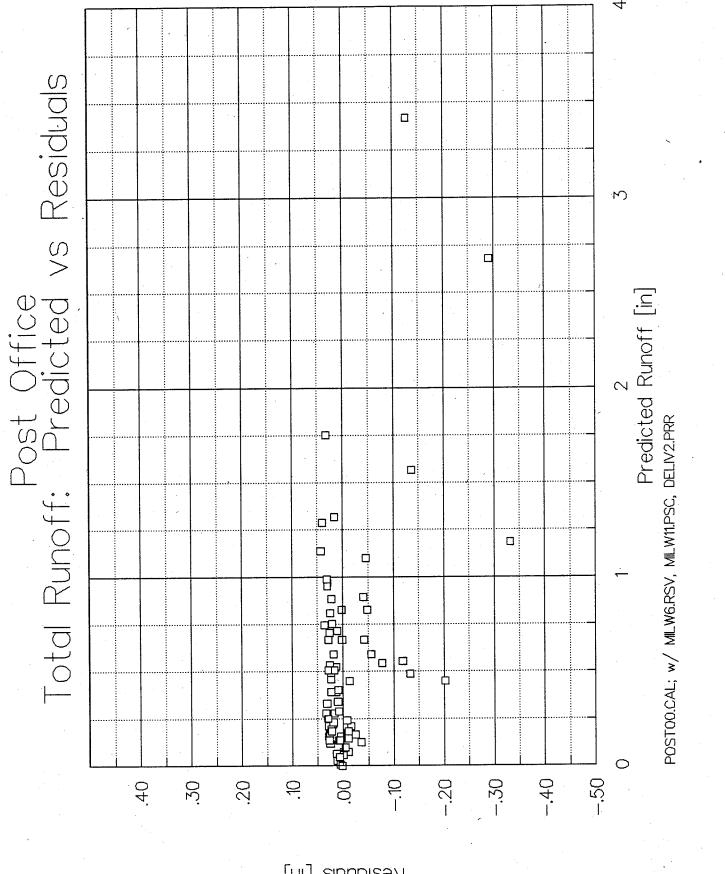
filename: DATASUM.WK1

JGV/RTB

		· ·				,	•			·	*		٠		
10 11 12	A    POSTOO.CAL	B    ; w/ MILW DATE		D   MILW11.F Obsrvd Runoff	0bsrvd		G   Resid Runoff	H   Calc Runoff	Obsrvd Resid F	J    Calc Res % of Obsrvd	K    Obsrvd RV (in/in)		M   sid Rv	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	T. Comments
13 14 15 16 17 18 19 20 21 22	267 269 270 271 272 273 274 275	4/ 3/80 4/ 6/80 4/ 8/80 4/ 9/80 4/14/80 4/28/80 4/28/80 5/13/80	.23 .10 .43 .32 .19 .10 .80	(in) .22 .07 .40 .31 .18 .06 .78	9663 3250 17657 13704 8082 2767 34304 7291	.192 .074 .389 .278 .155 .074 .744	.0283 .0004 .0134 .0336 .0294 0106 .0370 0073	8420 3234 17068 12229 6792 3234 32679 7613	1243 16 589 1475 1290 -467 1625 -322	.13 .01 .03 .11 .16 17 .05	.96 .74 .93 .98 .97 .63 .98	.83 .74 .90 .87 .81 .74 .93	.13 .00 .03 .11 .16 11 .05		Manufacture Assessment Control of the Control of th
23 24 25 26 27 28 29 30 31 32 33	277 278 279 280 281 282 283 284 285 286 287	6/ 1/80 6/ 2/80 6/ 5/80 6/ 6/80 6/ 7/80 6/19/80 7/16/80 8/ 2/80 8/ 2/80 8/ 4/80 8/ 7/80	.29 .25 .89 .72 .60 .09 1.04 .26 .25 2.79	.28 .24 .83 .63 .07 1.00 .24 .19 2.39	12255 10542 36412 27452 19063 2855 43967 10498 8521 104888 39750	.249 .210 .828 .667 .552 .066 .970 .220 .210 2.678	.0302 .0296 .0013 0421 1183 0006 .0308 .0191 0164 2904	10927 9241 36355 29303 24258 2880 42612 9657 9241 117643 38806	1328 1301 57 7-1851 -5195 -25 1355 841 -720 -12755	.11 .00 07 27 01 .03 .08 08	.96 .96 .93 .87 .72 .72 .96 .92 .78	.86 .84 .93 .93 .92 .73 .93 .85 .84 .96	.10 .12 .00 06 20 01 .03 .07 06 10		
35 36 37 38 39 40 41 42 43	288 289 290 292 293 294 295 296 297	8/11/80 8/13/80 8/19/80 9/ 9/80 9/12/80 9/16/80 9/20/80 9/25/80 10/ 2/80	.93 .57 .05 .58 1.26 1.37 .77 .72 .09 .02	.54 .04 .56 .85 1.33 .73 .67	23543 1801 24597 37422 58330 31932 29384 3075 483 6237	.523 .028 .533 1.184 1.288 .715 .667 .066	.0128 .0130 .0270 3324 .0402 .0116 .0019 .0044 .0059	22981 1229 23410 52022 56564 31423 29303	562 572 1187 -14600 1766 509 81 195 260	.02 .32 .05 39 .03	.94 .82 .97 .68 .97 .94 .93 .78	.92 .56 .92 .94 .94 .93 .93 .73	.02 .26 .05 26 .03 .01 .00 .05 .30		Promoteories ( 1997 ) and the second of the
44 45 46 47 48 49 50 51 52 53	299 300 301 302 303	10/16/80 10/24/80 11/13/80 11/23/80 12/ 1/80 12/ 6/80 2/22/81 4/ 4/81 4/ 8/81	.53 .20 .55 .17 .08 .64 .20 .87	.52 .16 .06 .61 .14 .83 .30	22313 8389 22884 7116 2548 26749 6325 36632 12957 15856	.484 .164 .504 .135 .058 .590 .164 .809 .278	.0237 .0267 .0173 .0266 .0003 .0186 0203 .0249 .0166	14470	1039 1174 758 1171 15 817 -890 1094 728 1386	.14 .03 .16 .01 .03 -14 .03	.95 .73 .95 .72 .96 .92	.91 .82 .92 .80 .72 .92 .82 .93 .87	.05 .14 .03 .15 .01 .03 10 .03 .05		The second secon
54 55 56 57 58 59 60 61 62 63	310 311 312 313 314 315 316 317 318 319	4/10/81 4/13/81 5/29/81 5/29/81 6/21/81 7/12/81 7/12/81 7/13/81 7/17/81 7/20/81	1.66 1.21 .16 .22 .89 1.17 .64 3.56	1.18 .09 .17 .78 1.05 .54 3.29	34216 46251 23499	1.564 1.137 .126 .182 .828 1.099 .590 3.418 .543	.0436 0359 0105 0487 0462 0554	49958 5532 8015 36355 48278 25932 150111 23840	-1579 -460	.04 40 06 06 04 10 04	.86 .98 .56 .78 .88 .90 .84 .92 .79	.94 .94 .79 .83 .93 .94 .92 .96 .92	08 .04 23 05 05 04 08 04 13 .07		
64 65 66 67 68 69 70 71 72 73	320 321 322	7/27/81 8/14/81 8/15/81 8/26/81 8/27/81 8/29/81 8/31/81 9/ 8/81 9/25/81 9/26/81	.44 .72 .01 1.02 .23 .19 1.85 .55	.41 .70 .00 .98 .22 .16 1.79 .53	17921 30526 176 43088 9487 7028 78403 23411 3514	.398 .667 .001 .950 .192 .155 1.752 .504	.0279 .0027 .0305 .0243 .0054 .0331 .0293	29303 56 41747 8420 6792 76950 22126 2880	1223 120 1341 1067 236 1453 1285 634	.04 .68 .03 .11 .03 .02 .05	.93 .97 .40 .96 .94 .84 .96 .97 .89	.90 .93 .13 .93 .83 .81 .95 .92 .73	.03 .04 .27 .03 .11 .03 .01 .05 .16		
74 75 76 77 78 79 80 81 82	330 331 332 333 334 335 336 337 338	9/30/81 9/30/81 10/ 6/81 10/14/81 10/17/81 4/ 2/82 4/ 2/82 4/ 2/82 4/ 3/82	1.40 .17 .49 1.06 .81 .28 .38 .43	1.33 .14 .24 1.02 .78 .23 .35 .41	58505 6325 10673 44889 34040 10190 15373 18140 37422	1.316 .135 .446 .990 .753 .239 .340 .389	.0160 .0086 2028 .0321 .0217 0071 .0101 .0244 0408	57803 5945 19581 43478 33087 10500 14929 17068 39214	702 380 -8908 1411 953 -310 444 1072 -1792	.01 .06 83 .03 .03 03 .06	.95 .85 .50 .96 .96 .83 .92 .96	.94 .80 .91 .93 .93 .85 .89	.01 .05 41 .03 .03 02 .03 .06 04		
83 84 85 86	339 340 341 342	5/11/82 5/15/82 5/21/82 5/22/82	.49 .17 .50 .53	.14	6237 21039	.135 .455	.0066 .0236	5945 20003	1036	.05 .05	.84 .96	.91 .80 .91 .91	03 .04 .05 25		1

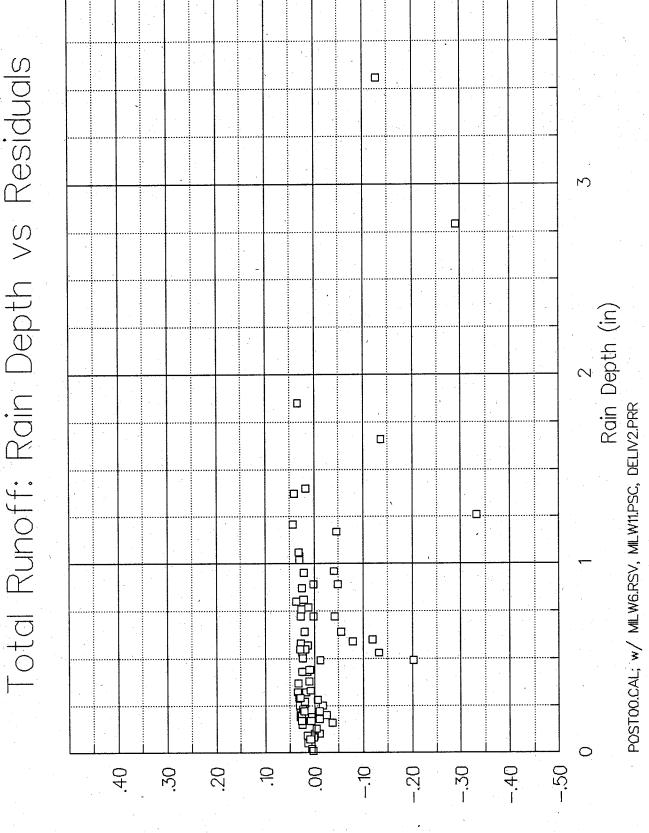
A    B 10 POSTOO.CAL; W/ MI	C    D	E    F PSC, DELIV2.PRR	G    H	I    J   Obsrvd Calc	K      Obsrvd	L    M   Calc
11 DATE	RAIN Obsrvd	Obsrvd Calc	Resid Calc	Resid Res % of	F RV	RV Resid Rv
	(in) Runoff	Runoff Runoff	Runoff Runoff	Runoff Obsrvd		in/in)
12 Code #				[cu ft]	(11.7 11.7 (	
13	(in)	(cu ft) [in]	filia (ca i c)	[Cu it]		
14				0/5 1/	.93	.83 .10
87 343 5/26/8						
88 344 5/27/8	2 .20 .14					.82 - 12
89 345 6/ 7/8	2 .18 .14	5930 .14	50099 6365			.8106
90 346 6/12/8	2 .07 .06	2416 .04	7 .0080 2064	352 .15	79	.67 .12
91 347 6/15/8		32152 .70	.0263 30998	1154 .04	.96	.93 .03
92 348 6/20/8	-		90039 4343	-17004	.73	.7603
93 349 6/25/8				375 _03	.90	.87 .03
	٠ دد. د	, 15045 .20	1825388			,
94			1023300			
95	04 00	47/ 00	1332 56	-14600	.40	.1341
96 Minimum:	.01 .00			1 1 1 1 1	.98	.96 .30
97 Maximum:	3.56 3.29					
98 Average:	.57 .52				.87	.85 .01
99 Count :	79 . 79	7 79 7			79	79 79
100 Std.Dev.:	.58 .53	3 23475 .56	1 .066 24643	2899	.12	.13 .11
101 Sum :	45.34 40.83	3 1793288 41.55	9731 1825388	-3210002	2 ,	1.16
102 COV :	1.01 1.03		7 -7.13 1.07	' -7 <b>.</b> 13:	. 14	.15





[ui] albubiseA

vs Residuals Post Office Total Runoff: Rain Depth



Residual Runoff (Obs—Pred) [in]

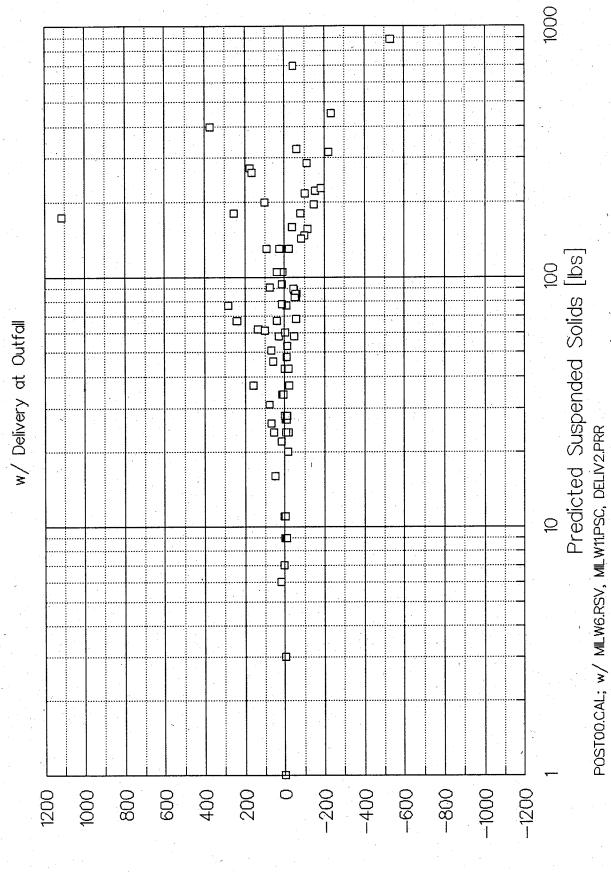
10 11 12 13 14	A   POSTOO.CAL	B    .; w/ MILW DATE	C    6.RSV, RAIN (in)	Υ [	Z /    SS N.FILT. RESID. (mg/l)	AA   SS N.FILT. RESID. (lbs)	SS Calc w/o	AC   SS Calc w/ Delivery [lbs]			AF   Outliers
15	267	4/ 3/80	.23		324	195	156	37	39	158	
16	269	4/ 6/80	.10		81	16	145	- 11	-129	5 239	,
17	270	4/ 8/80	.43 .32		278 15	306 13	129 155	67 58	177 -142	-45	,
18 19	271 272	4/ 9/80 4/14/80	.19		53	27	150	27		Ő	
20	273	4/28/80	.10		46	8	145	11	-137	-3	
21	274	4/28/80	.80		20	43	194	156	-151	-113	
22	275	5/13/80	.21		240	109	151	31	-42	78 -12	
23	277	6/ 1/80	.29		53 63	41 41	160 159	53 43	-119 -118	-12	
24 25	278 279	6/ 2/80 6/ 5/80	.25 .89		192	436	215	180	221	256	
26	280	6/ 6/80	.72		129	221	174	130	47	91	
27	281	6/ 7/80	.60		90	107	144	94		13	
28	282	6/19/80	.09		58	10	142	9		1	
29	283	7/16/80	1.04		25 162	69 106	253 160	222 46		- 153 60	
30 31	284 285	8/ 2/80 8/ 2/80	.26 .25		46	24		43		-19	
32	286	8/ 4/80	2.79		100	654			-43	-43	
33	287	8/ 7/80	. 95		. 19	. 47		196		-149	
34	288	8/11/80	.57		27	40		89		-49 -1	
35	289 290	8/13/80 8/19/80	.05 .58		20 30	2 46	10 <del>9</del> 141	3 90		-44	
36 37	292	9/ 9/80	1.26		75	175	308			-111	
38	293	9/12/80	1.37		26	95	335	316	-240	-221	
39	294	9/16/80	.77		25	50				-97	
40	295	9/20/80	.72		60	110		130 9		-20 -4	
41 42	296 297	9/25/80 10/ 2/80	.09 .02		28 48	5 1	142 12	. 0		1	
43	298	10/16/80	.15		6	2				-18	
44	299	10/16/80	.53		17	24			-115	-59	
45	300	10/24/80	.20		29	15	148			-13	
46	301	11/13/80	.55		18	26				-60 -20	
47 48	302 303	11/23/80 12/ 1/80	.17		· 8 72	4				4	
49	304	12/ 6/80	.64		68	113		105		8	
50	306	2/22/81	.20		74	29	148			. 1	
51	307	4/ 4/81	.87		564	1288		174		1114	*
52	308	4/ 8/81	.32		109 199	88 197				30 135	
53 54	309 310	4/ 8/81 4/10/81	.37 1.66		198	774				375	
55	311	4/13/81	1.21		138	446	296	272	150	174	
56	312	5/29/81	.16	٠,	160					17	•
57	313	5/29/81	.22		104	49 100				15 -80	
58 59	314 315	6/21/81 7/12/81	.89 1.17		47 148	427				166	
60	316	7/12/81	-64		100	147					
61	317	7/13/81	3.56		40					-530	
62	318	7/17/81	.59	•	130					75 - 7	
63 64	319 320	7/20/81 7/27/81	.27 .44		60 10	41 11				-57	
65	321	8/14/81	.72		81	154				24	
66	322	8/15/81	.01		137	2	1	0	1	.2	
67	323	8/26/81	1.02		43	116	247			-100	
68	324	8/27/81	.23		25					-22 -9	
69 70	325 326	8/29/81 8/31/81	.19 1.85		42 45						
71	327	9/ 8/81	.55	·	23					-52	
72	328	9/25/81	.09		9	2					
73	329	9/26/81	.29		53				-120 -77	-13 -59	
74 75	330 331	9/30/81 9/30/81	1.40		73 51					-39	
76	332	10/ 6/81	.49		102						
77	333	10/14/81	1.06		16	45	258	227	-213	-182	
78	334	10/17/81	.81		58	123	196				
79	335	4/ 2/82	.28		190					70 102	
80 81	336 337	4/ 2/82 4/ 2/82	.38 .43		170 94						
82	338	4/ 3/82	.96		128			199			
83	339	5/11/82	.49		304	361	136	77	225	284	
84	340	5/15/82	.17	•	204						
85 86	341 342	5/21/82 5/22/82	.50 .53		70 35						
00	346	27 66/02	در.		رر		. 137	, 33	. 103	7/	

10	A    POSTOO.CAL	B    ; w/ MILW	C     6.RSV,	<b>Y</b> [	z      ss	AA    SS	AB	AC   SS	AD   SS Resid	AE    SS Resid	AF   Outliers
11		DATE	RAIN		N.FILT. N	I.FILT.	Calc w/o	Calc w/	Calc w/o	Calc w/	
12	Code #		(in)		RESID.	RESID.	Delivery	Delivery	Delivery	Delivery	
13					(mg/l)	(lbs)	[lbs]	[lbs]	[lbs]	[lbs]	
14											
87	343	5/26/82	.22		75	42	154	34	-112	. 8	
88	344	5/27/82	. 20		44	17	148	<b>.</b> 28	-131	-11	
89	345	6/ 7/82	.18		254	94	153	.26	-59	68	
90	346	6/12/82	.07		184	28	, 134	6	-106	22	
91	347	6/15/82	.76		29	58	184	143	-126	-85	
92	348	6/20/82	.13		252	66	148	16	-82	50	
93	349	6/25/82	.33		<i>7</i> 3	59	153	60	-94	-1	
94									, ,		
95										100	
96	Minimum :		.01		6	1	1	0	-530	-530	
97	Maximum:		3.56		564	1288	890	890	1077	1114	
98	Average :		.57		95	128	189	- 114	-61	14	
99	Count :		79		79	79	79	79	79	79	
100	Std.Dev.:		.58		92	195	120	145	173	170	
101	Sum :		45.34		7496	10096	14943	.9001	-4847	1095	
102	cov :		1.01		.97	1.53	.63	1.28		1 1	
103	SUM - Outl	ier :				8808		8827		-19	

1000 Post Office Observed vs Calc Suspended Solids [lbs] G 0 0 Observed Suspended Solids [lbs] w/ Delivery POSTOCICAL; w/ MILWG.RSV, MILW11.PSC, DELIV2.PRR Ċ 9 1000 100

Calculated Suspended Solids [lbs]

Post Office Suspended Solids: Predicted v Residuals



Residuals [lbs]

Post Office Suspended Solids: Rain v Residuals \*/ Delivery at Outfall 2 Rain [in] POSTOO.CAL; w/ MILW6.RSV, MILW11.PSC, DELIV2.PRR -1000 -400 009--800 -1200400 800 900 200 -200 1000 1200

Residuals (Obs-Pred)[lbs]

В3

**Rustler Study Area Results** 

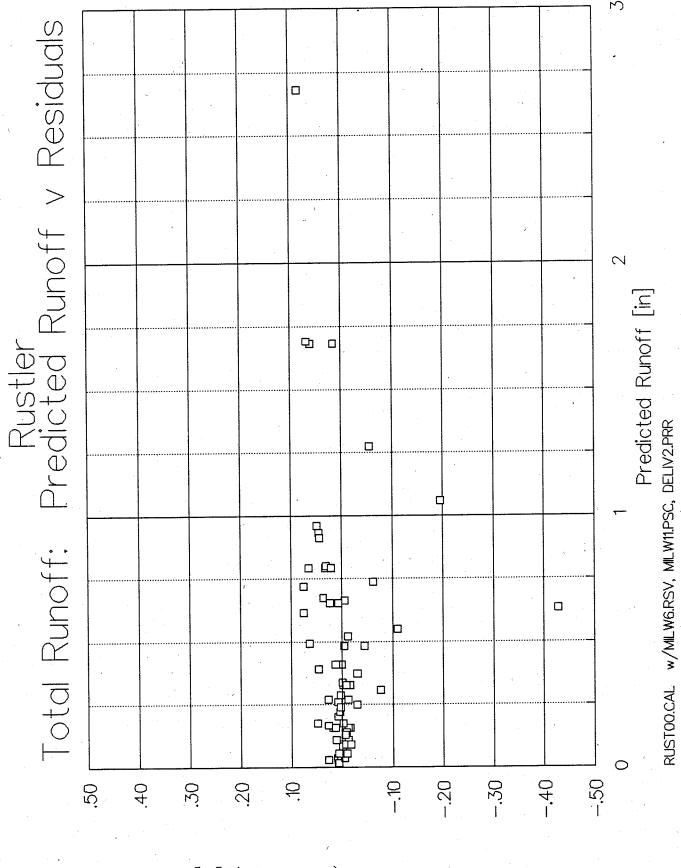
SLAMM Calibration Data Summary Sheet									
Site Data File Name: RUS	TØØ.DAT								
Rustler	Observed	Predicted	Residuals						
Runoff (in)									
Average	0.47	0.47	-0.001						
Std Dev	0,49	0.48	-						
COV	1.05	1.02							
Sum	31.80	31.89	-0.09						
Count	68								
Runoff - outliers [in]		·							
Average	0.44	0.45	-0,003						
Std Dev	0.47	0.46	-						
COV	1.00	1.03							
Sum	29,25	29.42	-0.17						
Count	66								
Av									
Average	0.79	.0,78	0.01						
Std Dev	0.15	0.14	_						
COV	0.19	0.13							
SS w/Delivery (lbs)									
Average	88	67	21						
Std Dev	160	77	-						
COV	1.81	1.15	•••						
Sum	5898	4510	1388						
Count	67								
SS w/Delivery - outliers [lbs]									
Average	60	63	3						
Std Dev	97	74							
COV	1.47	117	_						
Sum	4318	4124	194						
Count	65								
MILLEL DATAMINA UNIX									

filename: DATASUM.WK1

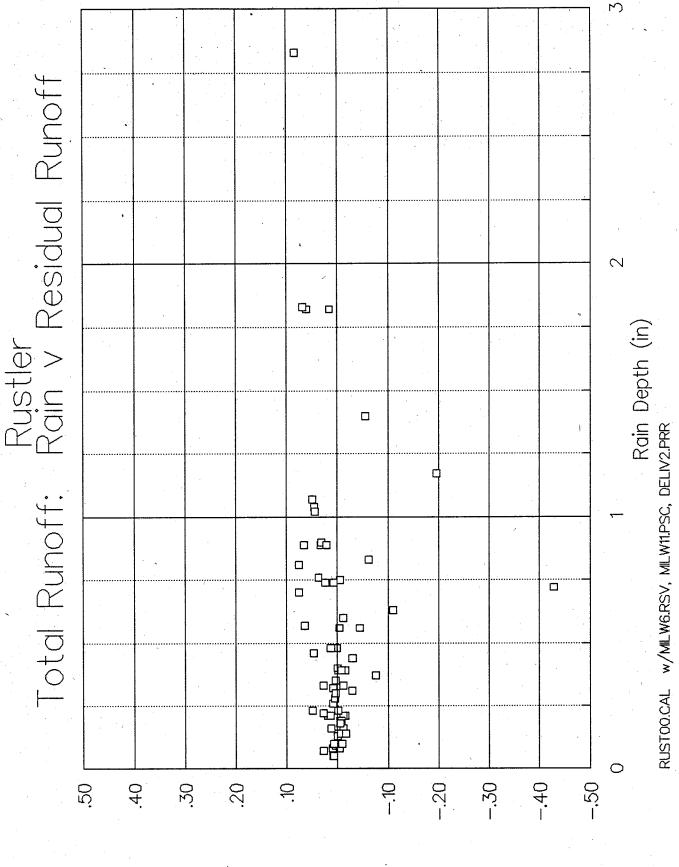
	A	8	C	D ]	E	- e	G	H	1	J	K	L	M     -
10 11	RUSTOO.CA	L W/MIĽŴ	16.RSV, N	IILW11.PS Obs Ttl			CALC TOTAL	RESID TOTAL	RESID/ OBS TTL		OBS TOTAL	CALC TOTAL	RESID TOTAL
12 13	CODE #.	DATE	RAIN (in)	RUNOFF (in)	RUNOFF (cu ft)	RUNOFF [in]	RUNOFF (cu ft)	RUNOFF [in]	,(%)	,	Rv (in/in)	Rv (in/in)	Rv (in/in)
15	196	4/ 4/80	.21	.18	7967	. 16	7093	.02 .01	.11		.84	.75	.09
16. 17	197 198	4/ 9/80° 4/14/80	.32	.27 .13	12018 5987	.26 .14	11623 6270	01	05		.70		03
18	199	5/13/80 6/ 5/80	.21	. 14 . 83	6392 37135	.16 .79	7093 35646	02 .03	11 .04		.68 .93		- 07 .04
19 20	200 201	6/27/80	.89 .39	.31	14134	.33	14798	01	05		.81	.84	03
21	202	7/16/80	1.04	.98 1.74	43977 78366	.93	41937 75648	.05	.05 .03		.94 .96		.04
22 23	203 204	7/26/80 8/ 2/80	1.82 1.82	1.70	76340	1.68 1.68	75648	.02	.03		.93		.01
24	205	8/ 7/80	.90 .70	.83 .69	37450 31058	.80 .61	36055 27648	.03 .08	.04 .11	•	.92		.03 .11
25 26	206 208	8/ 7/80 8/11/80	.56	-48	21561	.48	21722	.00	01		.86	.86	
27 28	209 210	8/13/80 8/16/80	.05 .39	.03 .33	1170 14719	.02 .33	764 14798	.01	.35 01		.52 .84		.18
29	211	8/19/80	.48	.41	18500	.41	18443	.00	01		.86	.85	.01
30 31	213 214	9/20/80 9/22/80	.74 .89	.68 .81	30473 36640	.65 .79	29382 35646	.02	.04 .03		.91 .91	.88 .89	.03 .02
32	215	9/22/80	.26	.21	9498		9083	.01	.04		.81	.78	.03
33 34	216 217	9/25/80 10/ 3/80	.08 .05	.05	2206 1080	.04 .02	1739 764	.01 .01	.21		.61 .48	.48 .34	. 13 . 14
35	218	10/16/80	.09	.05	2251	.05	2105	.00	.06		.56	.52	.04
36 37	219 220	10/17/80 10/24/80	.57 .21	.56 .15	25027 6527	.49 .16	22136 7093	.06 01	.12 09		.98 .69		.12 06
38	221	11/23/80	.14	.09	4096	.09	4136	.00	01		.65	.66	01
39 40	222 223	12/ 8/80 2/22/81	.23	.17 .30	7832 13324	.17	7875 12063	.00	01 .09		.76 .90		.09
41	224	4/22/81	.19	.13	5897	.14	6270	01	06		.69	.73	04
42 43	225 226	5/10/81 5/23/81	.56 .08	.44 .04	19715 1575	.48 .04	21722 1739	04 .00	10 10		.78 .44	.86 .48	08 04
44	227	5/29/81	.16	- 10	4411	.11	4948	01	12		.61	.69	08
45 46	228 229	5/29/81 6/ 8/81	.72 .13	.21 .08	9272 3736	.63	28513 3751	43	-2.08		.29 .64	.88 .64	59
47	230	6/15/81	.10	-05	2116	.06	2504	01	18		.47	.56	09
48 49	231 232	6/21/81 7/12/81	.83 1.17	.68	30428 38845	.74 1.06	33194 47675	06 20	09 23		.81 .74	.89 .91	08 17
50	233	7/12/81	.63	.44	19715	.55	24654	11	25 .03		.70 .98	.87 .95	17
51 52	234 235	7/13/81 8/ 7/81	2.83	2.77 .06	124503 2791	2.68 .06	120769 2504	.08 .01	.10	,	.62	.56	.06
53 54	336 237	8/14/81 8/15/81	.60 .37	.51 .23	22821 10398	.52 .31	23387 13868	01 08	02 33		.85 .62	.87 .83	03 21
55	238	8/26/81	1.02	.96	43076	.91	41064	.04	.05		.94	.89	.05
56 57	239 241	8/27/81 8/31/81	.23 1.83	.22 1.76	10038 79176	.17	7875 76094	.05 .07	.22 .04		.97 .96	.76 .92	.21 .04
58	242	9/21/81	.28	.23	10128	.22	9911	.00	.02		.80	.79	.01
59 60	243 244	9/30/81 10/14/81	1.40 1.07	1.22 1.01	54870 45462	1.28 .96	57395 43252	06 .05	05 .05		.87 .94		04 .04
61	245	10/17/81	.40	.34	15169	.34	15223	.00			.84	.85	01
62 63	246 247	10/17/81 3/12/82	.46 .22	.44	19760 8732	.39 .17	17633 7482	.05 .03	.11		. 95 . 88	.85 .76	.10 .12
64	248	3/16/82	.30	.24	10938	.24	10758	.00	.02		.81	.80	.01
65 66	249 250	3/19/82 4/ 2/82	.35 .31	.29 .22	13098 9903	.29	12956 11188	.00 03	.01 13		.83 .71	.82 .80	.01 09
6.7	251	4/ 2/82	.39	.32	14449	.33	14798	01	02		-82	.84	02
68 69	252 253	4/ 2/82 4/ 3/82	.81	.80 .66	35785 29573	.72 .66	32379 29818	.08 01	.10 01		.98 .88		.09
70	254	4/16/82	.89	.86	38620	.79	35646	.07	.08		.96	.89	.07
71 72	255 256	5/11/82 5/15/82	.39	.32 .09	14404 3826	.33	14798 4136	01 01	03 08	•	.82 .61	.84 .66	02 05
73	257	5/21/82	.44	.34	15484	.37	16826	03	09		.78	. 85	07
74 75	258 259	5/22/82 5/26/82	.48 .21	.42 .17	19040 7697	.41 .16	18443 7093	.01 .01	.03		.88 .81	.85 .75	.03 .06
76 77	260 261	5/27/82	.16 .14	.12 .08	5536 3421	.11	4948 4136	.01 02	.11 21		.77 .54	. 69	.08
78	262	6/ 7/82 6/12/82	.07	.06	2611	.03	1374	.03	.47		.83	.66 .44	12 .39
79 80	263 264	6/15/82 6/20/82	.74 .76	.66 .71	29708 31914		29382 30255	.01 .04	.01 .05		.89	.88	.01
81	265	6/25/82	.33	.26	11523	.27	12063	01	05		.93 .78	.81	.05 03
82 83	266	6/29/82	.18	.12	5536	.13	5816	01	05		. 68		04
84 -			_	_		_							
85 86	Maximum Minimum		2.83	2.77 .02	124503 1080		120769 764	.08 43	34.7% -207.5%		.99 .29		
	and a second	•	,.05		.000			. 73				.54	

. .

	1					•	
	-						•
10 11 12 13 87 88 89 90 91	A    B RUSTOO.CAL w/MII  CODE DATE . # .  Average : Count : Std.Dev.: Sum : COV : Outlier Adj:	RAIN RUNOFF (in) (in)	County Clare (County County Co	c Ttl TOTAL	H    I    RESID RESID/ TOTAL OBS TTL RUNOFF [in] (%)001 -1.9% 68 65 .07 28.3%093%	J    K    OBS TOTAL RV (in/in) .79 68 .15 53.57	L    M   CALC RESID TOTAL TOTAL RV RV (in/in) (in/in) .78 .01 .68 .68 .14 .12 53.20 .37 .18



Residual Runoff (Obs-Pred) [in]



Residual Runoff (Obs-Pred) [in]

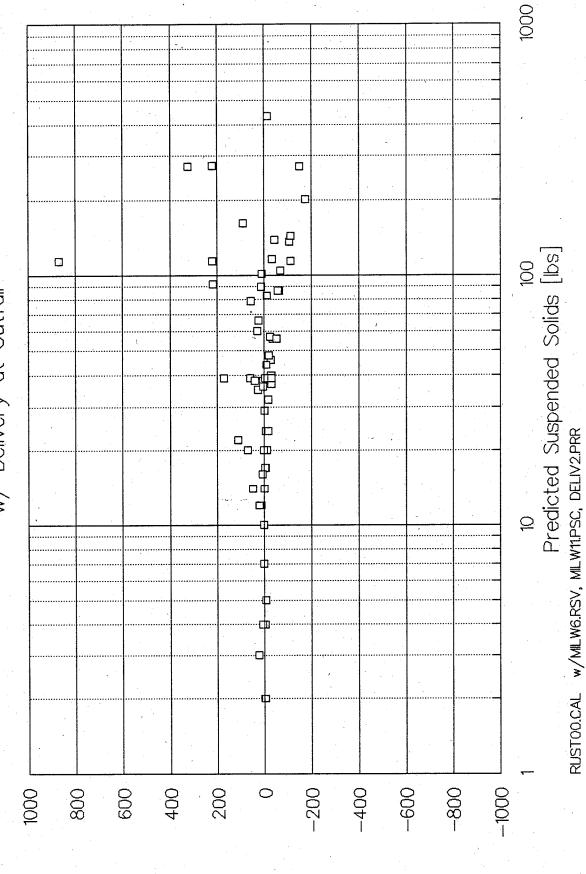
10	A   RUSTOO.C	B    AL w/MILW	C    AC 6.RSV,	AD   Obsvd	Obsvd	Calc SS		SS Resid	SS Resid	AJ
11 ′ 12	CODE	DATE	RAIN	TSS	TSS	w/o Deliv	w/ Deliv	w/o Deliv	w/ Deliv	Outliers
13	. # .		(in)	(mg/l)	(lbs) 14	[lbs] 90	[lbs] 20	[lbs] -76	[lbs] -6	
15 16	196 197	4/ 4/80 4/ 9/80	.21 .32	28 10		93	37	-85	-29	
17	198	4/14/80	.19	31	12	89	17	-77	-5	
18	199	5/13/80 6/ 5/80	.21 .89	228 144		90 132	20 114	1 202	71 220	
- 19 20	200 201	6/27/80	.39	12		76	39	-65	-28	3
21	202	7/16/80	1.04	35		154	139 272	-58 -152	-43 -150	
22 23	203 204	7/26/80 8/ 2/80	1.82 1.82	25 125		274 274	272	322	324	
24	205	8/ 7/80	.90	. 35	82	133	116	-51	-34	
25	206	8/ 7/80	.70	70 14		103 86	79 56	33 -67	57 -37	
26 27	208 209	8/11/80 8/13/80	.56 .05	3		64	2	-64	-2	2
28	210	8/16/80	.39	19		76	39	-59	-22 -19	
29 30	211 213	8/19/80 9/20/80	.48 .74	25 14		82 109	48 87	-53 -82	-60	
31	214	9/22/80	.89	1	2	132	114	-130	-112	2
32	215	9/22/80	.26	46 22		96 80	29 4	-69 -77	-2 -1	
33 34	216 · 217	9/25/80 10/ 3/80	.08 .05	12		64	2	-63	-1	
35	218	10/16/80	.09	8			5	-83	-4	
36 37	219 220	10/17/80 10/24/80	.57 .21	21 19		86 90	57 20	-53 -82	-24 -12	
38.	221	11/23/80	.14							
39	222	12/ 8/80	.23	37		93 92	24 38	-75 -49	-6	
40 41	223 224	2/22/81 4/22/81	.33 .19	52 44		89	17	-73	_7	
42	225	5/10/81	.56	5		86	56	-80	-50	
43	226	5/23/81	.08	142 232		· 80 92	4 14	-66 -28	10 50	
44 45	227 228	5/29/81 5/29/81	.16 .72	122		106	83	-35	- 12	2
46	229	6/ 8/81	.13	48		88	10 · 7	-77 -76		1
47 48	230 231	6/15/81 6/21/81	.10 .83	71 20		85 123	104	-76 -85	-66	
49	232	7/12/81	1.17	104	252	175	162	. 77	90	
50	233	7/12/81 7/13/81	.63 2.83	74 54		92 433		-1 -13	25 - 13	
51 52	234 235	8/ 7/81	.10	47		85	7	-77	•	1
53	336	8/14/81	.60	63		88		2 -70	30 - 28	
54 55	237 238	8/15/81 8/26/81	.37 1.02	19 12		82 151		-119	-104	
56	239	8/27/81	.23	13	8	93	24	-85	-10	
57 58	241 242	8/31/81	1.83 .28	100 28		276 96			221 - 14	
59	242	9/21/81 9/30/81	1.40		27		201	-182	-17	4
60	244	10/14/81	1.07	12		159			-110	0
61 62	245 246	10/17/81 10/17/81	.40 .46	38 14		75. 81	39 46		-2 <sup>-</sup>	
63	247	3/12/82	.22	248	3 135	92	22	43	11:	3
64	248	3/16/82	.30 .35	. 94 . 12				-31 -78	2 <sup>1</sup> -2 <sup>1</sup>	
65 66	249 250	3/19/82 4/ 2/82	.31	70				-51	,	7
67	251	4/ 2/82	.39	110	99	76			6	
68 69	252 253	4/ 2/82 4/ 3/82	.81 .75	5°					1:	
70	254	4/16/82	.89	408	3 984	132	114	852	87	0 * [
71	255	5/11/82	.39	233					17 1	
72 73	256 257	5/15/82 5/21/82	-14 -44	38				-42	4	7
74	258	5/22/82	.48	2	3 27	82		-55	-2	1
75 76	259 260	5/26/82 5/27/82		41						3 0
77	261	6/ 7/82	.14	16	2 35	90	.12	-55	2	3
78	262	6/12/82		177					2 -5	5 7
79 80	263 264	6/15/82 6/20/82		16 15						
81	265	6/25/82	.33	113	2 81	92	38	-11	. 4	3
82 83	266	6/29/82	.18	. 7	2 25	91	16	-66		9
83 84			•	<u> </u>						
.85	Maximum		2.83	40						
86	Minimum	:	.05		1 0	64	. 2	102	- 17	<del>-</del>

10 11 12 13 87 88	CODE # .  Average Count	DAT	C    MILW6.RSV, E RAIN (in) .54 68	AC	AD    Obsvd TSS (mg/l) 68 67		AF    Calc SS w/o Deliv [lbs] 112 67		AH    SS Resid w/o Deliv [lbs] -24 67	AI    SS Resid w/ C Deliv [lbs] 21 67	AJ   Outliers
89 90 91 92	Std.Dev. Sum COV Outlier	:	.50 36.78 .93		74 4542 1.09	160 5898 1.81 4318	60 7476 .53	77 4510 1.15 4124	137 -1578 -5.80	132 1388 6.35 194	
								· ·			

1000 Rustler Suspended Solids Observed vs Calculated Suspended Solids w/ Delivery at Outfall . ... 日 Þ Ċ RUSTOO.CAL W/MILWG.RSV, MILW11.PSC, DELIV2.PRR \_\_ \_ \_ 100 9

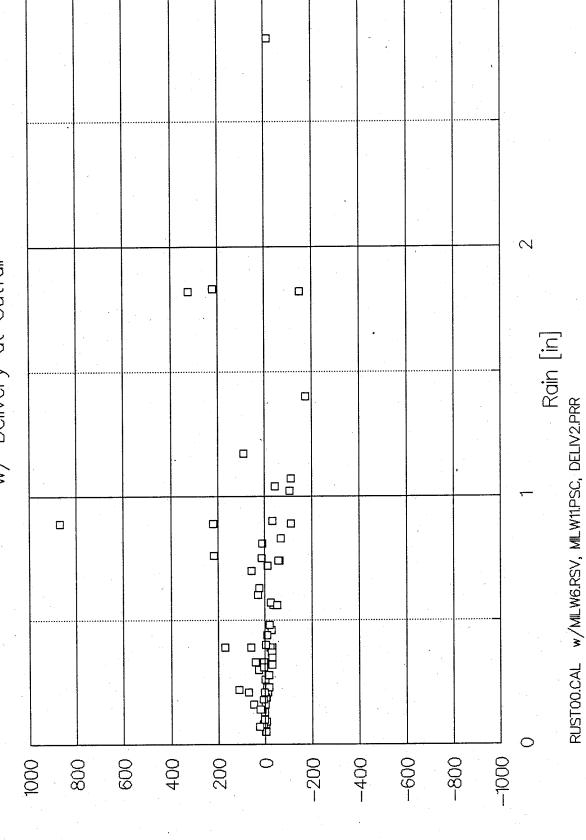
Predicted Suspended Solids [bs]

Rustler Suspended Solids Predicted vs Řesiduals w/ Delivery at Outfall



Residuals [lbs]

Rustler Suspended Solids Rain vs Residuals W/Delivery at Outfall



[sdl] slbubisa9

**B4** 

Hastings 1980-1982 Study Area Results

Site Data File Name: HAS	TØØ, DAT										
		SLAMM Calibration Data Summary Sheet Site Data File Name: HASTØØ, PAT									
Hastings	Observed	Predicted	Residuals								
Runoff [in]	7	Ç.									
Average	0,23	0.24	-0,02								
Std Dev	0.42	0.42	_								
COV	1.83	1.72	-,								
Sum	10,01	10,69	-0.68								
Count	44										
Runoff – outliers [in]											
Average	0.22	0,24	-0.02								
Std Dev	0.42	0.42									
COV	1.91	1.77									
Sum	9.45	10.23	-0.79								
Count	43										
Rv											
Average	0.28	0,31	-0,03								
Std Dev	0.10	0.07									
COV	0.34	0.24									
SS w/Delivery [lbs]											
Average	114	93	21								
Std Dev	240	138									
COV	2.10	i.48									
Sum	5018	4107	911								
Count	44										
SS w/Delivery - outliers (lbs)											
Average	89	91	-2								
Std Dev	175	139									
COV	1.97	1.53									
Sum	3814	3920	-106								
Count	43										

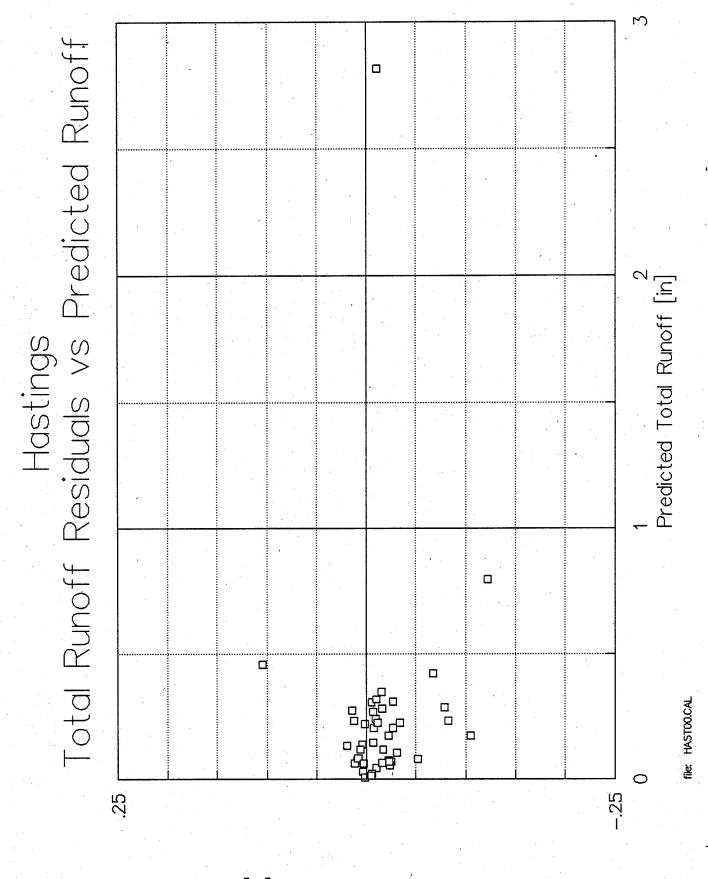
filename: DATASUM.WK1

J6V/RTB

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200													
													•
													1
	A	B	C	D	Ε	F	G	H	I	J	K	L	M
10	file:	HASTOO.CAL	•		OBS	SLAMM	SLAMM	RESID	RESID/		OBS	SLAMM	RESID
11 ′				Obs Ttl	TOTAL	TOTAL	TOTAL	TOTAL	OBS TTL	*	TOTAL	TOTAL	TOTAL
12	CODE	DATE	RAIN	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF		RV	RV	RV ·
13	# .		(in)	(in)	(cu ft)	[in]	(cu ft)	[in]	[]		/(in/in)	(in/in)	(in/in)
14			( 1117	· · · · ·				• • • • •			• • •		
15	404	6/ 2/80	.25	.08	8892	.07	7766	.01	.13		.30	.27	.03
	405	6/ 6/80	.67	.25	28781	.23	27329	.01	.05		.37	.35	.02
16		6/ 7/80	.60	.20	23282	.21	24148	01	04		.33	.34	01
17	406				16730	.14	16191	.01	.03		.33	.31	.02
18	407	6/28/80	.44	.14			49294	07	- 19		.32	.38	06
19	408	7/26/80	1.12	.35	41416	.42			55		.17	.27	10
20	409	8/ 2/80	.26	.05	5265	.07	8160	02	٠.55				10
21	410	8/ 4/80	4.87	2.81	328288	2.82	329536	01	40		.58	.58	- 05
22	411	8/ 7/80	.65	. 19	22463	.23	26412	03	18		.30	.35	05
23	412	8/11/80	.64	.22	26090	.22	25956		.01		.35	.35	
24	· 413	8/16/80	.28	.09	10062	.08	8970	.01	.11		.31	.27	.04
25	414	8/19/80	.24	.08	8775	.06	7378	.01	.16		.31	.26	.05
26	415	9/12/80	.95	.33	38959	.35	40731	02	05		.35	.37	02
27	416	9/16/80	.85	.30	35215	.31	35830	01	02		.35	.36	01
28	417	9/20/80	.69	.23	27143	.24	28252	01	04		.34	.35	01
29	418	9/25/80	.15	.03	3861	.03	3449		.11		.22	.20	.02
30	419	10/16/80	.30	.09	10764	.08	9806	.01	.09		.31	.28	.03
	420	10/16/80	.24	.07	7722	.06	7378		.04		.28	.26	.02
31					16379	.15	17132	01	05		.30	.32	02
32	421	12/ 6/80	.46	.14		.27	31531	01	02		.35	.35	.02
33	424	2/22/81	.76	.26	30770				71		.15	.26	11
34	425	2/27/81	.22	.03	3861	.06	6621	02					
35	426	4/ 4/81	.80	.21	24218	.29	33434	08	38		.26	.36	10
36	427	4/ 8/81	.36	.08	8892	.11	12474	03	40		.21	.30	09
37	428	4/ 8/81	.77	. 29	33695	.27	32006	.01	.05		.37	.36	.01
38	429	4/10/81	1.20	.56	65634	.46	53423	.10			.47	.38	.09
39	430	4/13/81	.53	. 15	18017	.18	20571	02	14		.29	.33	04
40	431	4/22/81	.19	.04	4212	.05	5398	01	28		.19	.24	05
41	432	5/10/81	.67	. 15	17666	.23	27329	08	55		23	.35	12
42	433	5/23/81	.29	.03	3276	.08	9384	05	-1.86		.10	.28	18
43	434	5/29/81	.06		1053	.01	824		.22		.15	.12	.03
44	435	6/ 8/81	.13	.02	1989	.02	2644	01	33		.13	.17	04
45	436	6/13/81	.53			.18	20571	10	-1.48		.13	.33	20
46	437	6/15/81	.88		36151	.32	37285	01	03		.35	.36	01
47	438	6/20/81	.65	.21	25037	.23	26412	01	05		.33	.35	02
	439	7/25/81	.39		14624	.12	13900	.01	.05		.32	.30	.02
48			.28		6318	.08	8970	02			.19	.27	08
49	440	7/27/81			21059	.21	24148	03			.30	.34	04
50	441	3/12/82	.60						53		.10	.15	05
51	443	3/15/82	.10		1170	.02	1793	01					0.05
52	444	3/16/82	.43		18017	.13	15727	.02			.36	.31	.05
53	446	3/20/82	.39			.12		02			.26	.30	04
54	447	4/ 2/82	1.89		789,72	.80	93315	12			36	.42	
.55	448	5/11/82	.86		33227	.31	36314	03			.33	.36	03
56	449	5/22/82	. 25		5967	.07		02			.20	.27	
57	450	5/26/82	.26	.05	5499	.07	8160	02	48		.18	.27	09
58	451	6/15/82	.79		31121	.28	32959	02	06		.34	36	02
59										5			
60	Minimu	m :	.06	.01	1053	.01	824	12	-1.86		.10	.12	20
61	Maximu		4.87					.10			.58	.58	.09
62	Averag		.64		26608	.24		02			.28	.31	03
	Std.De		.73			.42		.04			.10	.07	.06
63		v.:						44			44	44	43
64	Count	•	44	44		44		. 44	44			.24	
65	COV	:	1.15						-8.39		.34 12.45	13.76	-1.25
66	Sum	:	27.94	10.01	1170768	10.09	1250577	68	-0.37		12.43	19.10	-1.60

Hastings Predicted v Observed Observed Total Runoff [in] rotal Runoff file: HASTOO.CAL 5 <u>2</u> ア **Q** 10.00 Predicted Total Runoff [in]

9

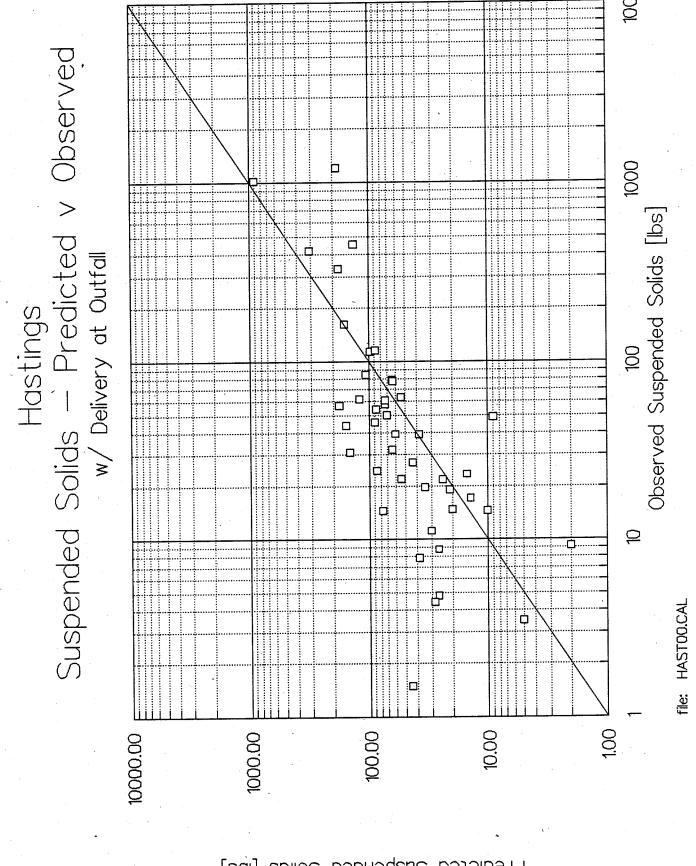


Total Runoff Residuals [in]

2 Hastings Total Runoff: Rain vs Residuals Rain [in] <u>ا.</u> 5 -.20 -.25 -.05 <del>-</del>.10 .05 .20 €. ₽. .25

[ni] albubiseA fronuA lotoT

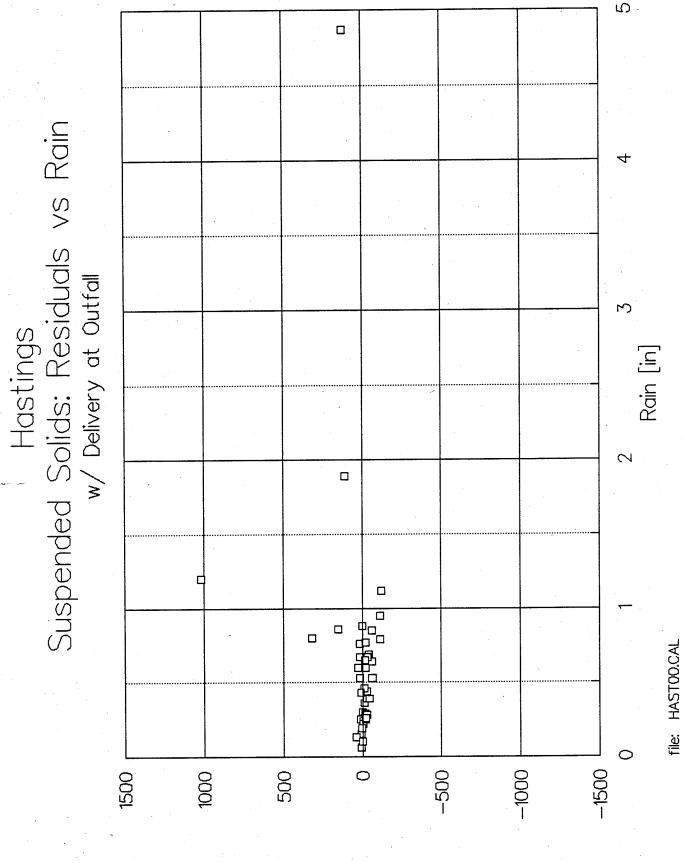
						•					
			- 11		1 11	1		l. an' 11	: AC	AD 11	AE   AF
10		B    IASTOO.CAL	C	X      SS	SS	Calc SS	Calc SS	AB    SS Resid	AC    SS Resid		AE     AF
11				N.FILT.	N.FILT.						
12	CODE	DATE	RAIN			w/o Del		w/o Del	w/ Del [lbs]	w/ Del []	* Outlie
13 14	# .		(in)	(mg/l)	(lbs)	[lbs]	[lbs]	[lbs]	frosi	£ 1	
15	404	6/ 2/80	.25	42	23	105	15	-82	8	.55	
16	405	6/ 6/80	.67	44	79	136	64	-57	15	.24	
17	406	6/ 7/80	.60	27	39	130	60	-91	-21	35	
18	407	6/28/80	.44	21	22	162	54	-140 -216	-32 -121	59 68	
19 20	408 409	7/26/80 8/ 2/80	1.12	22 34	57 11	273 180	178 30	-169	-19	63	
21	410	8/ 4/80	4.87	50	1025	969	906	56	119	.13	
22	411	8/ 7/80	.65	41	57	186		-129	-16	21	
23	412	8/11/80	.64	15	24		86	-161	-62	72	
24	413	8/16/80	.28	14	9	157	26	-148 -132	-17 -5	66 26	
25 26	414 415	8/19/80 9/12/80	.24 .95	27 18	15 44	147 242	20 157	- 132	-113	72	
27	416	9/16/80	.85	28	62	219	120	-157		49	
28	417	9/20/80	.69	27	46	197	90	-151	-44	49	
29	418	9/25/80	. 15	60	14	143	10	-129	4	.45	
30	419	10/16/80	.30	58	39		38	- 155	1	.03	
31	420	10/24/80	.24	45 59	22 60	173 211	24 73	-151 -151	-2 -13	10 17	
32 33	421 424	12/ 6/80 2/22/81	.46 .76	59	113	237	98	-124	15	.16	
34	425	2/27/81	.22	79	19	185	21	-166	-2	09	
35	426	4/ 4/81	.80	300	454	226	133	228	321	2.41	*
36	427	4/ 8/81	.36	49	27		43		-16	37	
37	428	4/ 8/81	.77		84	196	106	-112	-22	21	*
38	429	4/10/81	1.20		1205 78	245 162	187 63	960 -84	1018 15	5.44 .23	•
39 40	430 431	4/13/81 4/22/81	.53	69 65	17	144	14	-127	3	.22	
41	432	5/10/81	.67		54	206	87		-33	38	* .
42	433	5/23/81	.29	96	20		34		-14	42	
43	434	5/29/81	.06	140	9	107			7	3.60	
44	435	6/ 8/81	.13	394	49	150 200	9 77		40 -62	4.44 81	
45 46	436 437	6/13/81 6/15/81	.53 .88		15 162	248	161		1	.01	
47	438	6/20/81	.65	32	50		70			29	
48	439	7/25/81	.39		32	208	64		-32	50	
49	440	7/27/81	.28		8		38		-30	- 79	
50	441	3/12/82	.60		116	220	88		28	.31	
51 52	443 444	3/15/82 3/16/82	. 10 . 43		63	137 184	. 5 54		-1. : 9	30 .17	
53	446	3/20/82	.39	_	1	178				97	
54	447	4/ 2/82	1.89		419				110	.36	
55	448	5/11/82	.86	160	332	270	177		155	.87	
56	449	5/22/82	.25		5		26		-21	81	
57	450	5/26/82	.26		4				-24 -114	84 79	
58 59	451	6/15/82	.79	16	31	250	145	-219	114	19	
60	Minimum		.06	. 2	1	105	2	-219	-121		
61	Maximum		4.87		1205	969	906	960	1018		<b>.</b>
62 ×	Average	:	.64	67	114				21		
63	Std.Dev		.73		240				168	4.4	
64	Count	:	44 1.15		2.10				44		
65 66	COV Sum	* * * * * * * * * * * * * * * * * * *	27.94		5018				911		
67	Juli	•	_, _,		3814		3920		-106		



Predicted Suspended Solids [lbs]

1000 Suspended Solids: Residuals vs Predicted w/ Delivery at Outfall 750 Predicted Suspended Solids [lbs] Hastings 500 250 file: HAST00.CAL -1500-1000 -500 0 500 1000 1500

[sdl] albubias Residuals [babnaqau2]



Suspended Solids Residuals [bs]

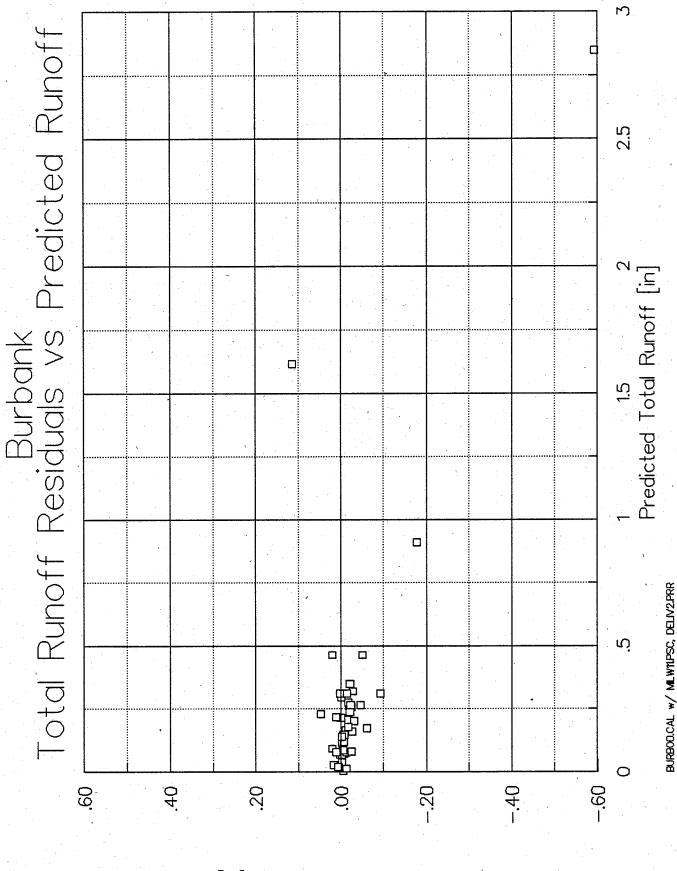
**Burbank Study Area Results** 

SLAMM Calibration Data Summary Sheet									
Site Data File Name: BURB Ø Ø, DAT									
Burbank	Observed	Predicted	Residuals						
Runoff [in]									
Average	0.24	0.26	-0.02						
Std Dev	0.38	0,44	_						
COV	1,59	1.69	_						
Sum	12.22	13.36	-1.13						
Count	51								
Runoff - outliers [in]									
Average ,	0.17	0,18	-0,01						
Std Dev	0.14	0,16							
COV	0.82	0.87							
Sum	7.94	8.58	-0,64						
Count	48								
Rv									
Average	0.30	0,31	-0.02						
Std Dev	0.09	0.08							
COV	0.30	0.27	_						
SS w/Delivery [lbs]									
Åverage	391	347	44						
Std Dev	764	242	~						
COV	1.95	0.70	-						
Sum	19942	17676	2266						
Count	51								
SS w/Delivery - outliers (lbs)			·						
Average	220	301	-81						
Std Dev	244	102	_						
COV	1.11	0.34	(-						
Sum	10543	14431	-3888						
Count	48								

JGV/RTB

9	1 " 1	-						•		· · · · · ·	•		
10	BURBOO.C	AL W/ MILW	111.PSC,			SLAMM	SLAMM	Resid	Resid		0bs	SLAMM	Resid
11		- 4		Obs Ttl		Total	Total	Total	Total		Total Dv	Total Rv	Total Pv
12	CODE	DATE	RAIN	Runoff	Runoff [cu ft]	Runoff [in]	Runoff [cu ft]	Runoff [in]	Runoff [cu ft]			(in/in)	(in/in)
13 14	. # .		(in)	[in]	[Cu Tt]	LIM	ten iti	L I I I I	fon i'r		(111/1117	(1117 1117	(117)
15	350	6/ 6/80	.73	.24	53929	.26	58099	02	-4170		.33	.36	03
16	351	6/ 7/80	.65	.28	61505	.23	50940	.05	10565		.42		.07
17	352	6/28/80	.48	.15	32981	.16	34907	01	-1926		.31	.33	02
18	353	7/ 5/80	.94	.33	73093	.35	77678	02	-4585		.35		02
19	354	7/ 9/80	.16	.03	7131	.03	7584	.00	-453		.20	.21	01
20	355	7/16/80	.72	.23	51923	.26	57193	02	-5270		.32		04
21	356	8/ 2/80	.25	.07	15822	.07	15033	.00	789	• .	.28		.01
22	357	8/ 4/80	4.87	2.26	502740	2.85	634565	59	-131825		.46		12
23	358	8/ 7/80	1.20	.41	92258		103271	05			.35		05
24	360	8/11/80	.85	.22	48358		69150		-20792		.26		11
25	361	9/16/80	.81	.29	65294		65435	.00			.36		.00
26	362	9/20/80	.67	.22	48135	.24	52711	02			.32		03
27	363	9/25/80	.13	-02	4903	.02			-274		.17		01
28	364	10/ 3/80	.05	.00		.01	1179	.00	-956		.02		09 .05
29	365	11/23/80	.12	.03	5794				1315		.22		
30	366	12/ 6/80	-46	.14	31867	.15	33059		-1192		.31	.32	01 03
31	367	12/ 8/80	.27	.07	14931	.07 .27	16567 60834		-1636 -3786		.25 .34		02
32	368	2/22/81	.76	.26	57048 53929		59007				.33		03
<b>33</b>	369	4/, 4/81	.74 .74	.24 .22	48803		59007		-10204		.30		06
34 35	370 371	4/ 8/81 4/10/81	1.20	.48	107857		103271	.02		- 1	.40		.01
36	372	4/13/81	.52	.11	25182		38707				.22		11
37	373	4/22/81	.17		8245		8492				.22		.00
38	374	5/10/81	.59	.19			45691	02			.32		03
39	376	6/ 8/81	.11	.02	5125	.02	3971	.01	1154		.21		.05
40	377	6/ 8/81	.14	.04	9805		5927				. 31	.19	.12
41	378	6/13/81	.50		34318				-2472		.31	.33	02
42	379	6/21/81	.49	.14				03	-5760		.28	.33	05
43	380	7/12/81	.87	.29	64625	.32	71025	03	-6400		.33		04
44	381	7/12/81	.61	.21	47243	.21	47434	.00	-191		.35		.00
45	382	7/13/81	3.23	1.73	385746				25481		.54		.04
46	383	7/17/81	.40	.12							.30		01
47	384	7/20/81	.46		31421		33059		-1638		.31		01
48	385	7/25/81	.38								.30		01
49	386	7/27/81	.25	. 07							.26		01
50	387	8/ 7/81	.31	.09							.28	.29	01
51	389	8/14/81	.39		25404			01			.29		02 .06
52	390	8/15/81	.32		24959			.02			.35		.05
53 54	391 303	8/28/81 8/29/81	.12		5794 223				-2857		.01		14
55	392 393	8/31/81	.58								.29		
56	393 394	9/ 7/81	.53						-3801		.30		04
57	395	9/25/81	.44								.31		01
58	396	9/26/81	.28								.32		.04
59	397	9/30/81	2.06								.35		
60	398	10/14/81	.85								.37		
61	399	10/17/81	.28								.23		
62	400	10/17/81	.62						2726		.37		.02
63	401	4/16/82	.30					01	- 1358		.26	.28	02
64	402	5/11/82	.85	.30	66185	.31	69150				.35		
65	403	5/26/82	.29	.06	12702	.08	18152	02	-5450		.20	.28	08
66							, A	. 1			-	,	
67	Minimum		.05						-131825		.01		14
68	Maximum		4.87								.54		
69	Average	:	.66								.30		02
70	Count	:	51								51		51
71	Std.Dev.	r 🕻 💮 🖟 s	.79								.09		- 05
72	Sum		33.83		2723843		2976237		-252394		15.06 .30		
73	COV	:	1.19	1.59	1.59	1.69	1.69				.30	.21	·

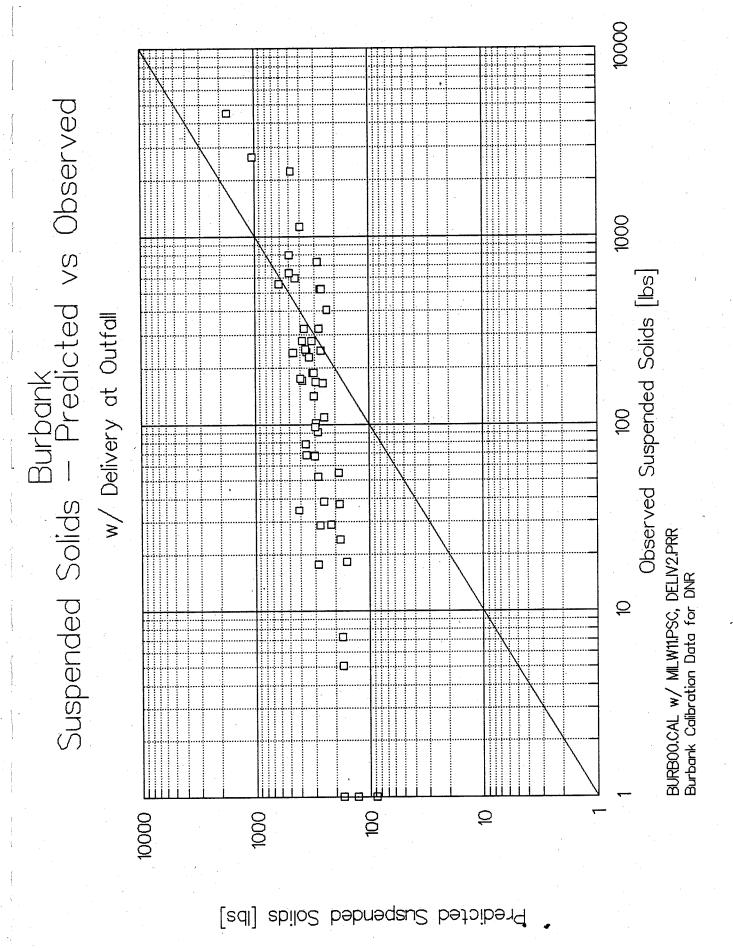
9 Burbank Predicted vs Observed BURBOO.CAL w/ MILW11.PSC, DELIV2.PRR Total Runoff 7 -6 19. 14. <del>--</del> 9 Predicted Total Runoff [in]

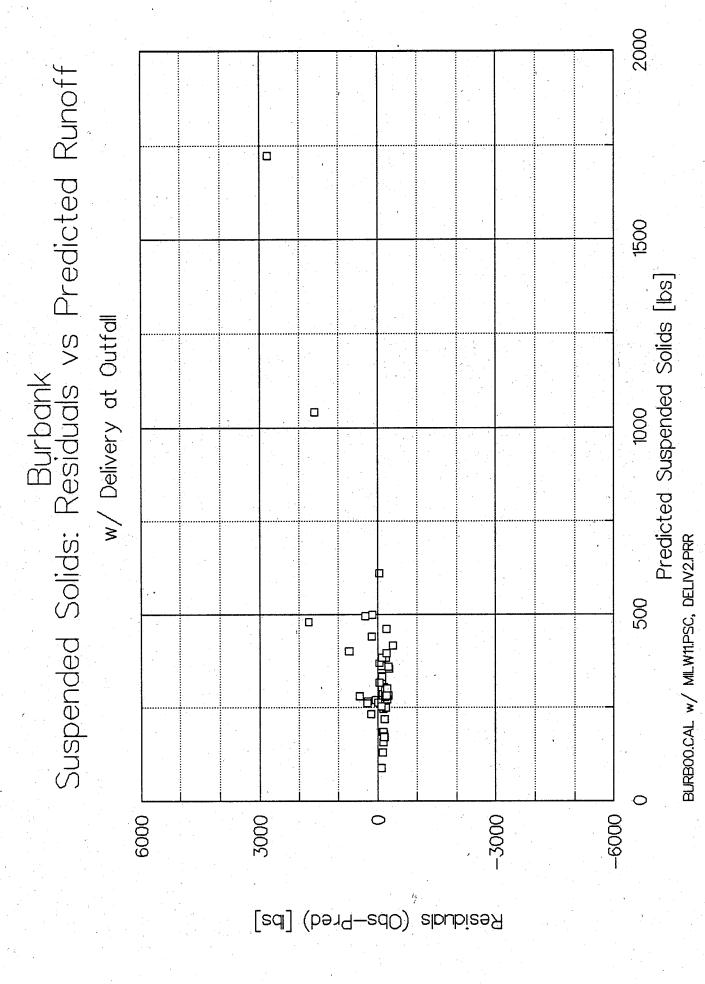


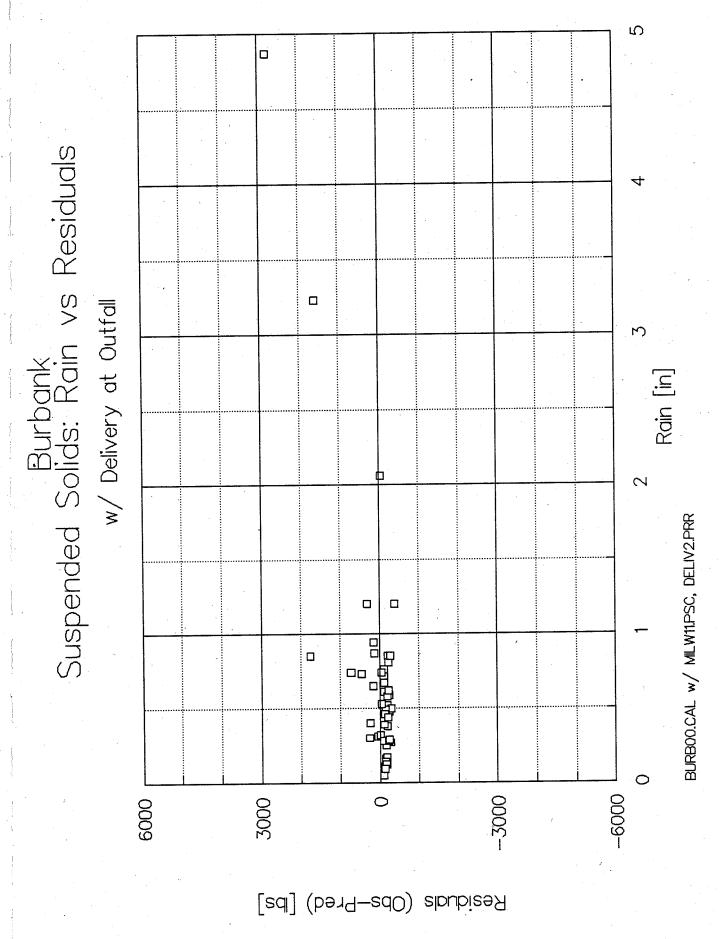
[ni] slaudisesiduals [in]

S Burbank Rain Depth vs Total Runoff Residuals Rain [in] BURBOO.CAL W/ MLW1LPSC, DELIV2.PRR 0 -.40 09. .20 -.20 .40 [ni] albubiseA fronuA lotoT

9 10	BHBBUG C	AL W/ MILW	111 per							
11	BUKBUU.L	AL'W/: MILW	111.736,		SS	Calc SS	Calc SS	SS Resid	≠SS Resid	Outliers
12	CODE	DATE	RAIN			w/o Del	w/ Del	w/o Del	w/ Del	
13	. # .		(in)		(lbs)	[lbs]	[lbs]	[lbs]	[lbs]	
14 15	350	6/ 6/80	.73		727	301	280	426	447	
16	351	6/ 7/80	.65		407		232	149	175	
17	352	6/28/80	.48		68	332	. 301		-233	٠.
18	353	7/ 5/80	.94		598		441	127	157	
19	354	7/ 9/80	.16		18		157	-234	-139	
20	355	7/16/80	.72		243	385	353 704	-142 -227	-110 -162	
.21	356 357	8/ 2/80	.25 4.87		142 4519	369 1844	304 1724	2675	2795	*
22 23	357 358	8/ 4/80 8/ 7/80	1.20		35	475	417		-382	
24	360	8/11/80	.85		172	417	384	-245	-212	
25	361	9/16/80	.81		240	494	461	-254	-221	
26	362	9/20/80	.67		228	404	332	-176	-104	
27	363	9/25/80	.13		24	282	180	-258	-156	
28	364	10/ 3/80	.05		1	174	89	-173	-88	
29	365	11/23/80	.12		1	292	171	-291	-170	
30	366	12/ 6/80	.46		251	386	361	-135	-110	
31	367	12/ 8/80	.27		18		283 314	-330 -250	-265 -125	
32 33	368 369	2/22/81	.76 .74		189 1131	439 446	401	685	730	
34 `	370	4/ 4/81 4/ 8/81	.74	:	323		369	-103	-46	
35	371	4/10/81	1.20		794		496		298	
36	372	4/13/81	.52		102	350	294		-192	
37	373	4/22/81	.17		29		218	-274	-189	
38	374	5/10/81	.59		29	407	272	-378	-243	
39	376	6/ 8/81	.11	4.0	55	281			-130	
.40	377	6/ 8/81	.14		37		184	-254	-147	
41	378	6/13/81	.50		69		355	-323	-286	1
42	379	6/21/81	.49		109		246	-269	-137 139	
43	380 381	7/12/81	.87		637 277		498 383	104 -132	-106	
44 45	382	7/12/81 7/13/81	.61 3.23		2649		1041	1536	1608	*
46	383	7/17/81	.40		522				255	
47	384	7/20/81	.46		169		289		-120	
48	385	7/25/81	.38		91	314	278	-223	-187	
49	, <b>386</b>	7/27/81	.25		7		173		-166	
50	387	8/ 7/81	.31		323	321	271	2	52	
51	389	8/14/81	.39		189		304	-152	-115	
52	390	8/15/81	.32 .12		246 5	292 262	263 171	-46 -257	-17 -166	
53 54	391 392	8/28/81 8/29/81	.09		1	216	129			
55	393	8/31/81	.58		97		296	-249	-199	1.0
56	394	9/ 7/81	.53		278		317		-39	
57	395	9/25/81	.44		38		250	-345	-212	•
58	396	9/26/81	.28		167		253	-171	-86	
59		9/30/81	2.06		559		610			
60	398	10/14/81	.85		78		359			
61 62	399 400	10/17/81 10/17/81	.28 .62		. 52 175		283 395	-300 -248	-231 -220	
63	401	4/16/82	.30		523		261	153	262	
64	402	5/11/82	.85		2231	514	480		1751	*
65	403	· 5/26/82	.29		67		301	-305	-234	
66		-,,	-							
. 67	Minimum	:	.05		1		89	-440	-382	
68	Maximum	:	4.87		4519		1724		2795	
69	Average	:	.66		391		347		44	
70	Count	:	51		51	51		51	51	
71	Std.Dev.	. :	.79		764 19942		17474		554	
72 73	Sum COV		33.83 1.19		1.95		17676 70.		2266	
74	Sum-Out l	-			10543		14431		-3888	
75		,							-529	
									p. 1	



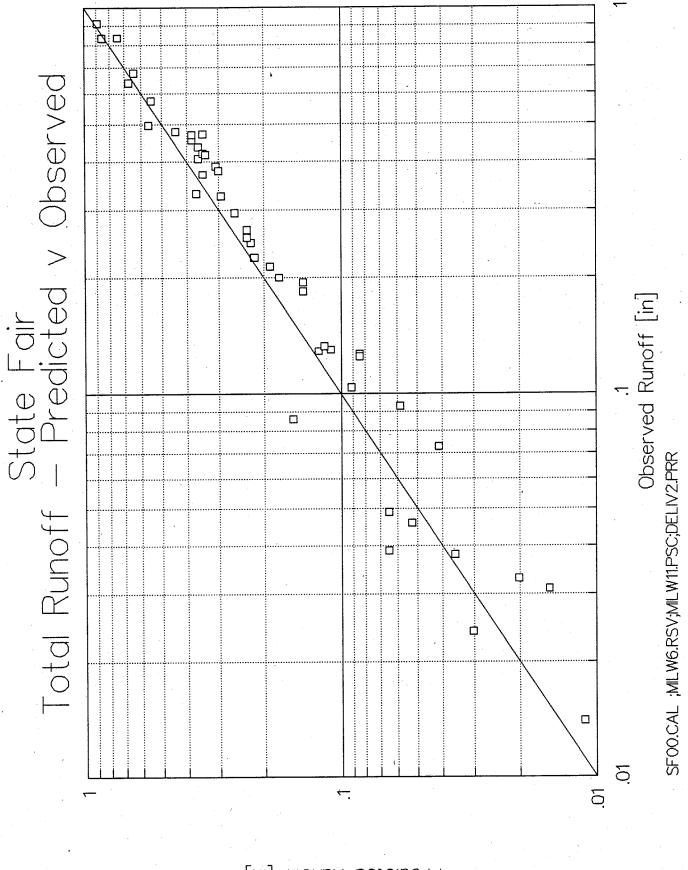




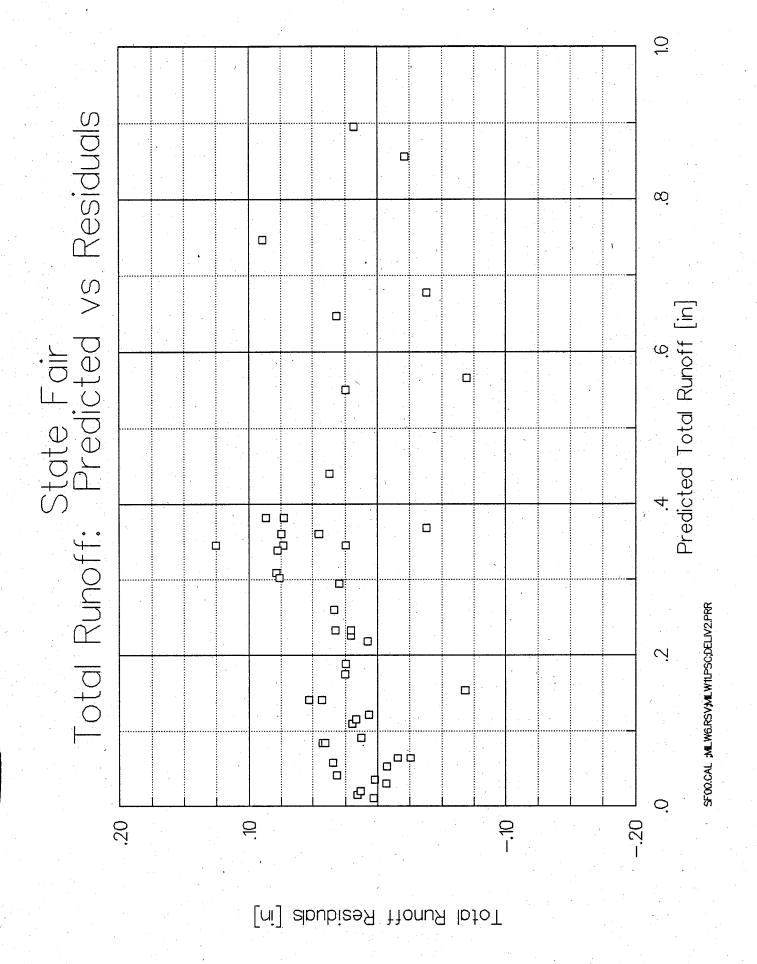
State Fair Study Area Results

SLAMM Calibration Data Summary Sheet										
Site Data File Name: SF	OD. DAT									
State Fair	Observed	Predicted	Residuals							
Runoff (in)										
Average	0.30	0.27	0,03							
Std Dev	0.23	0.22								
COV	0.78	0.83	-							
Sum	13.66	12.49	1.18							
Count	46									
Runoff - outliers [in]										
Average	0.29	0.27	0. <i>0</i> Z							
Std Dev	0,23	0.23								
COV	0.79	0.84								
Sum	13.21	12.11	1.10							
Count	45									
Rv	*									
Average	0.61	0.54	0.07							
Std Dev	0.15	0.12	-							
COV	0.24	0.22	-							
SS w/Delivery [lbs]										
Average	292	280	12							
Std Dev	332	108	-							
COV	1.14	0.38								
Sum	13435	12384	551							
Count	46									
SS w/Delivery - outliers (lbs)										
åverage	257	279	-22							
Std Dev	238	109								
COV	0.92	0.39	_							
Sum	11578	1257/	-993							
Count	45									
filanama: DATACIIMA WAYA		,								

SF00.CA	L ;MILW6.R			OBS TOTAL	SLAMM TOTAL	SLAMM TOTAL	RESID	RESID TOTAL	RESID/ OBS TTL	OBS TOTAL	SLAMM TOTAL	RESID TOTAL
CODE	DATE	RAIN	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RV	· RV	RV
. # .	DATE	(in)	(in)	(cu ft)	[in]	(cu ft)	[in]	(cu ft)	(%)		(in/in)	
2	5/28/80	.86	.50	52304	.57	59607	07	-7303	-14.0%	.58	.66	0
3	8/16/80	.34	.21	22567	.19	19929	.03	2638	11.7%	.63	.56	
4	9/ 9/80	1.24	.84	88052	.86	90294	02	-2242	-2.5%	.67	.69	0
5	9/22/80	.58	.41	42813	.36	38019	.05	4794	11.2%	.70	.62	.0
6	9/22/80	.24	.13	13603	.12	12890	.01	713	5.2%	.54	.51	.0
7	10/16/80	.69	.48	50300	.44	46395	.04	3905	7.8%	.69	.64	
10	3/26/81	.06	.03	3269	.02	1609	.02	1660	50.8%	.52	.25	
11	3/29/81	.07	.03	3480	.02	2120	.01	1360	39.1%	.47	.29	. 1
12	4/ 4/81	.61	.46	47980	.38	40306	.07	7674	16.0%	.75	.63	1
15	4/13/81	1.29	.91	96277	. 89	94354	.02	1923	2.0%	.71	. 69	.0
16	4/22/81	.22	.13	13709	.11	11602	.02	2107	15.4%	.59	.50	.0
17	5/23/81	.18	.13	13392	.08	8896	.04	4496	33.6%	.71	.47	.2
18	5/29/81	.27	.18	19403	. 14	14896	.04	4507	23.2%	.68	.52	
19	6/ 8/81	.27	.19	20458	.14	14896	.05	5562	27.2%	.72	.52	٠.,2
20	6/13/81	.58	.44	45871	.36	38019	.07	7852	17.1%	.75	.62	
21	6/21/81	.56	.47	49668	.35	36450	.13	13218	26.6%	.84	.62	
22	7/17/81	.18	.13	13181	.08	8896	.04	4285	32.5%	.69	.47	
23	7/20/81	.13	.05	4851	.05	5583	01	-732	-15.1%	.35	.41	(
24	7/27/81	.39	.25	26047	.23	23829	.02	2218	8.5%	.63	.58	. (
25	8/ 6/81	.29	.09	9069	.15	16284	07	-7215	-79.6%	.30	.53	
26	8/14/81	.59	.33	34799	.37	38810	04	-4011	-11.5%	.56	.62	
28	8/29/81	1.01	.64	67384	.68	71398	04	-4014	-6.0%	.63	.67	
29	9/21/81	.40	.27	28050	.23	24571	.03	3479	12.4%	.67	.58	
30	9/25/81	.32	.20	21090	.17	18441	.03	2649	12.6%	.63	.55	. (
31	9/26/81	.51	.39	40915	.31	32610	.08	8305	20.3%	.76	.61	_
32	10/17/81	.44	.29	31003	.26	27430	.03	3573	11.5%	.67	.59	
33	10/17/81	.61	.47	49457	.38	40306	.09	9151	18.5%	.77	.63	
34	3/30/82	.23	. 13	14025	.12	12241	.02	1784	12.7%	.58	.50	
35	4/ 3/82	.40	.25	26785	.23	24571	.02	2214	8.3%	.64	.58	
36	4/ 3/82	.56	.42	44184	.35	36450	.07	7734	17.5%	.75	.62	
37	4/ 3/82	.50	.38	39861	.30	31856	.08	8005	20.1%	.76	.60	
38	4/ 4/82	1.10	.84	88157	.75	78769	.09	9388	10.6%	.76	.68	
- 39	4/16/82	.49	.33	34272	.29	31107	.03	3165	9.2%	.66	.60	
40	4/16/82	.11	.07		.04	4371	.03	3327	43.2%	.66	.38	
41	5/11/82	.38	.23	23832	.22	23028	.01	804	3.4%	.59	.57	
42	5/15/82	.15	.04	4113	.06	6829	03	-2716	-66.1%	.26	.43	
43	5/18/82	.05	.01	1476	.01	1169		307	20.8%	.28	.22	
44	5/21/82	.56	.37		.35	36450	.02	2567	6.6%	.66	.62	
45	5/22/82	.84	.58		.55	58070	.02	2565	4.2%	.68	.66	
46	5/26/82	.19	.10	10967	.09	9637	.01	1330	12.1%	.55	.48	
47	5/27/82	.14	.09	9807	.06	6193	.03	3614	36.9%	.66	.42	
48	5/29/82	.10	.04		.04			239		.38	.36	
49	6/15/82	.97	.68		.65	68192	.03		4.6%	.70	.67	
50	6/20/82	.15	.05		.06	6829	02			.33	.43	
51	6/25/82	.55	.42		.34	35673	.08		18.7%	.76	.62	
52	6/29/82	.09	.02		.03	3206	01		-26.7%	.27		
	J, _ J, JE					2200		, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				
Minimum		.05	.01	1476	.01	1169	07	-7303		.26	.22	2
Maximum		1.29	.91		.89	94354	.13			.84	.69	
Average		.45	.30		.27		.03		8.6%	.61	.54	
Std.Dev		.32	.23		.22	23664	.04		J.0%	.15	.12	
Count	• •	46	.23 46		46	46	46			46	46	
COV		.71	.78		.83		0	40		.24	.22	
COA	•	20.49		1440889		1316849	1.18	124040		28.12	24.81	3.3

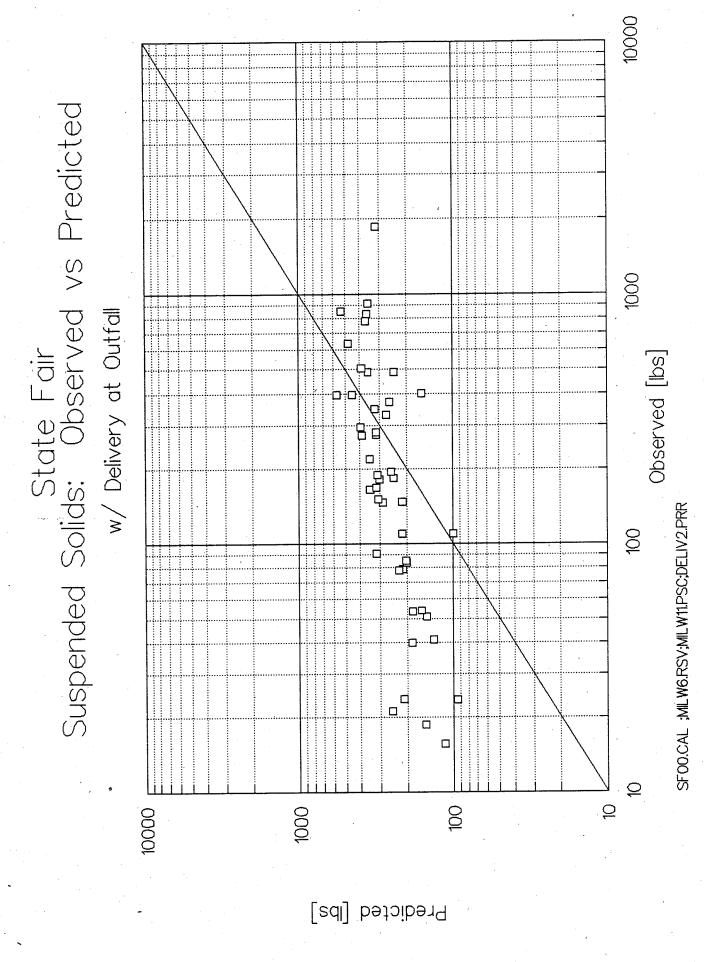


Predicted Runoff [in]



2.0 <u>%</u>: State Fair Total Runoff — Rain vs Residuals <u>1</u>9 1.4 □ 1.0 Rain (in) 9 Ö Ġ SFOO.CAL JALWG.RSVJALW11.PSC,DELIVZ.PRR <u>-</u> 0 -.20 .20 9 [ni] Residuals [in]

CODE	DATE	RAIN	N.FILT. RESID.	N.FILT. RESID.	w/o Del	w/ Del	w/o Del	w/ Del	Outlier
. # .		(in)	(mg/l)	(lbs)	[lbs]	[lbs]	[lbs]	[lbs]	
2	5/28/80	.86	194		518	479	115	154	-
3	8/16/80	.34	56	. 79	337	214	-258	-135	•
4	9/ 9/80	1.24	72	396	608	569	-212	-173	
5	9/22/80	.58	82		397	349	-178	-130	
6	9/22/80	.24	92		309	225	-231	-147	
7	10/16/80	.69	118		388	258	-17	113	
10	3/26/81	.06	536		204	100	-95	9	
11	3/29/81	.07	72		220	114	-204	-98	
		.61	620		358	313	1499		. *
12	4/ 4/81					532	278	321	
15	4/13/81	1.29	142		575	232			
16	4/22/81	.22	128		292	215	-182	-105	· .
17	5/23/81	.18	479		291	159	109	241	
18	5/29/81	.27	272		328	272	1	57	
19	6/ 8/81	.27	144	184	342	243	-158	-59	
20	6/13/81	.58	. 51		341	286	-195	-140	
21	6/21/81	.56	157	487	370	241	117	246	
22	7/17/81	.18	102		276	201	-192	-117	
23	7/20/81	.13	132		280	186	-240	-146	
24	7/27/81	.39	13		362	250	-341	-229	
25		.29	320		357	302		-121	
	8/ 6/81						-9	27	
26	8/14/81	.59	160		357	321			
28	8/29/81	1.01	70		448	397	-154	-103	
29	9/21/81	.40	94		392	346	-227	-181	
30	9/25/81	.32	18	24	346	212	-322		
31 ,	9/26/81	.51	59		356	306	-205	- 155	- L
32	10/17/81	.44	142	275	359	315	-84	-40	
33	10/17/81	.61	158		384	355	104	133	- *
34	3/30/82	.23	192	168	414	317	-246	-149	
35	4/ 3/82	.40	302		428	392	77	113	
36	4/ 3/82	.56	102		384	317	-103	-36	
			76		360	311	-171	-122	
37	4/ 3/82	.50							
38	4/ 4/82	1.10	72		488	452	-92	-56	
39	4/16/82	.49	428		393	354	523	562	•
40	4/16/82	.11	106		246	150	- 195	-99	
41	5/11/82	.38	560		412	362	421	471	
42	5/15/82	. 15	332		271	204	-186	-119	
43	5/18/82	.05	256		187	94	-163	-70	
44	5/21/82	.56	80		329	254	-134	-59	
45	5/22/82	.84	24		378	317	-287		
46	5/26/82	-19	78	53	257	185	-204	-132	
47		.14	88		238	161	-184		
	5/27/82								•
48	5/29/82	.10	164		204	134	-163	-93	
49	6/15/82	.97	61		472	390	-200	-118	
50	6/20/82	.15	456		283	213	-136	-66	
51	6/25/82	.55	284	778	390	365	388	413	
52	6/29/82	.09	118	19	252	152	-233	- 133	
	1			4 22					1.01
Minimum		.05	13.00	16	187	94	-341	-229	
Maximum		1.29	620.00		608	569	1499	1544	
Average		.45	179.61		352	280	-60		
		.32	151.93		90	108	301	292	
Std.Dev	• •								
Count	:	46	46		46	46	46	46	
COV	:	.71	.85		.26	.38			
Sum	:	20.49	8262		16181	12884	-2746	551	
	liers:			11578		12571		-993	



State Fair Suspended Solids: Predicted vs Residuals w/ Delivery at Outfall 8 中 Ф 2000 1500 1000 -500 -1000500 0

1000

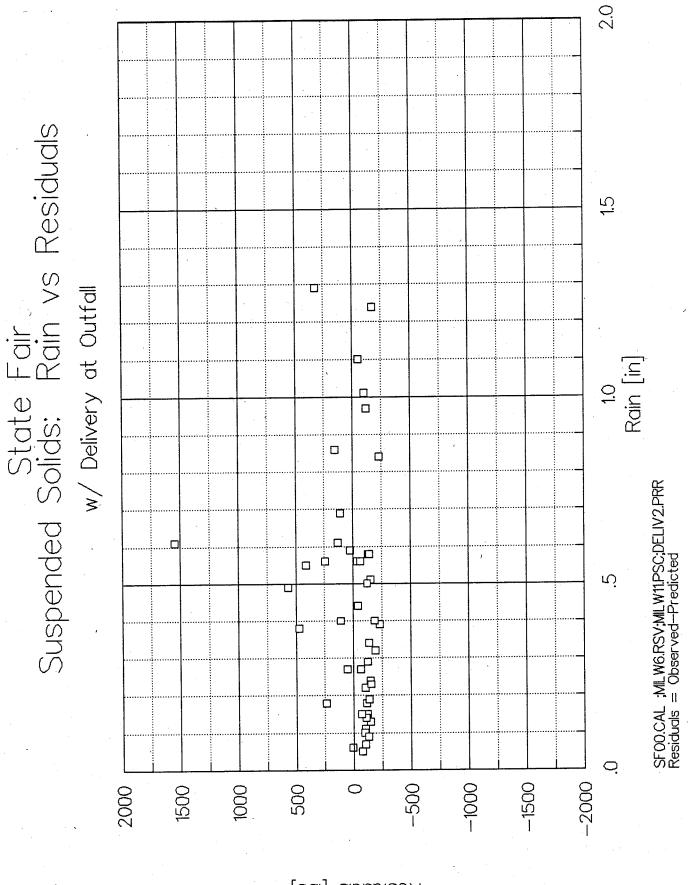
Predicted [lbs]

SFOO.CAL ;MILWG.RSV;MILW11.PSC;DELIV2.PRR Residuals = Observed-Predicted

-1500

[edi] albubiseA

-2000



Residuals [bs]

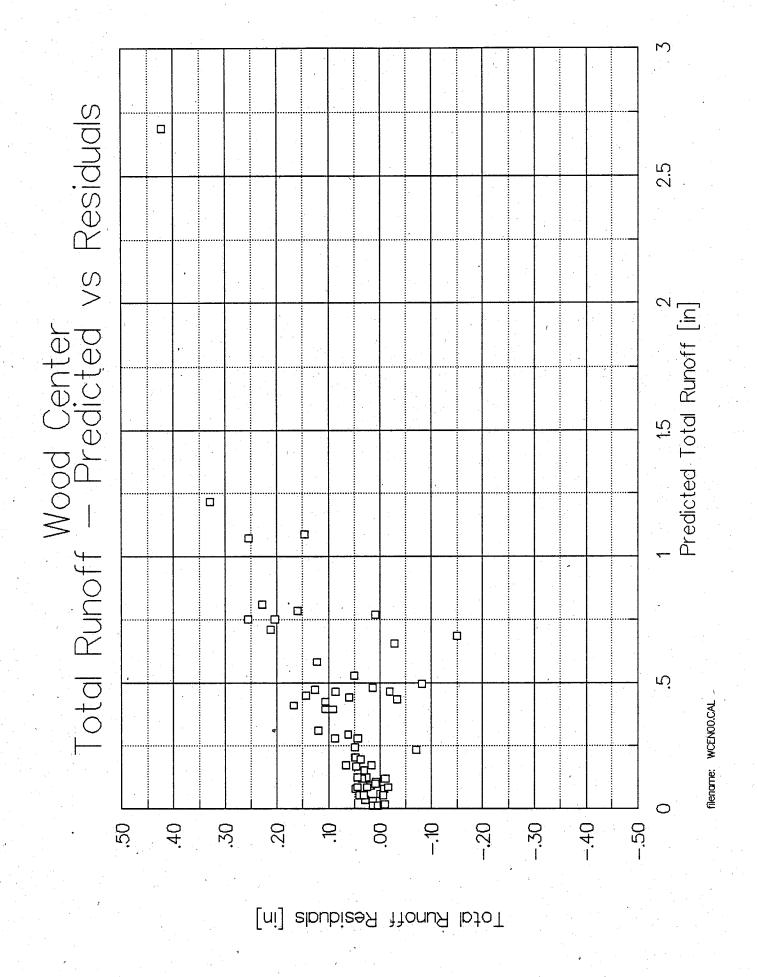
Wood Center 1980-1982 Study Area Results

SLAMM Calibration Data Summary Sheet										
Site Data File Name: WCENグダ. DAT										
Wood Center	Observed	Predicted	Residuals							
Runoff [in]			•							
Average	0.44	O.38	0.06							
Std Dev	0.49	0.42	<u> </u>							
COV	1.12	1.11								
Sum	26,87	22.94	3,93							
Count	61									
Runoff - outliers (in)										
Average	0.38	0.33	0.04							
Std Dev	0.34	0.28								
COV	0.38	0.86	_							
Sum	22.44	19,18	3,25							
Count	59									
Rv										
Average	0.71	0.60	0.11							
Std Dev	0.17	0.13	_							
COV	0.24	0.21	-							
SS w/Delivery [lbs]										
Average	953	803	150							
Std Dev,	1330	333								
COV	1.40	0.41	_							
Sum	58154	49005	9151							
Count	61									
SS w/Delivery - outliers (lbs)			`							
Average	780	769	10							
Std Dev	909	271								
COV	1.17	0.35								
Sum	45996	95391	605							
Count	59		7-							

				Obs Ttl	Obs Ttl	TOTAL	TOTAL	TOTAL	TOTAL	OBS TTL	TOTAL	TOTAL	TOTAL
CODE		DATE	RAIN (in)	RUNOFF	RUNOFF (cu ft)	RUNOFF [in]	RUNOFF (cu ft)	RUNOFF [in]	RUNOFF (cu ft)	RUNOFF (%)	RV (in/in)	RV (in/in)	RV (in/in)
53		3/15/80	.23	.15	24151	.13	20055	.03	4096	17.0%	.66	.55	.11
54		4/ 3/80	.16	.13	20152		12507	.05	7645	37.9%	.79	.49	.30
55		4/ 4/80	.34	.25	40304	.20	32515	.05		19.3%	.74	, 60	.14
56		4/ 6/80	.08	.04	6877				2101	30.6%	.54	.37	.17 .16
57 60		4/ 9/80 5/28/80	.29 .76	.21 .58	34067 92444	.17 .53	26607 84382	.05 .05		21.9% 8.7%	.73 .76	.57 .69	.07
- 61		6/ 1/80	.30	.24		.17	27755	.07		27.7%	.80	.58	.22
62		6/ 2/80	.59	.50		.39	63164	.11	16965	21.2%	.85	.67	.18
63		6/ 5/80	1.11	1.04	166175	.81	129681	.23		22.0%	.94	.73	.2
64		6/ 6/80	.66	.59	94683	.45	71736	.14		24.2%	.90	.68	.22
65		6/ 7/80	1.04	1.01	161217	.75	120273	.26	40944 1239	25.4% 6.8%	.97 .57	.72 .53	.25
66 47		6/19/80	.20 .70	.11	18233 79009	.11 .48	16994 76736	.01 .01	2273	2.9%	.71	.69	.02
67 68		7/ 5/80 7/ 9/80	.72	.41	66054	.50	79265	08		-20.0%	.57	.69	12
69		7/15/80	.13	.06		.06		.00		4%	.45	.46	01
70		7/16/80	.06	.01	1439	.02	2884	01	-1445	-100.4%	.15	.30	15
71		7/26/80	1.59	1.55	247264	1.22	194704	.33		21.3%	.97	.77	.20
72		8/ 2/80	.18	.11	17433	-09	14711	.02		15.6%	.61	.51	.10
73		8/ 2/80	.17	.13		.08	13591 429714	.04		33.6% 13.6%	.75 .96	.50 .83	.25
74 75		8/ 4/80 8/ 7/80	3.24 1.44	3.11 1.23	497247 197203	2.69 1.09	174012	.42 .15		11.8%	.86		.10
76		8/ 7/80	.48	.43		.31	49446			27.8%	.89	.64	.25
78		8/16/80	.34	.25	40144	.20	32515	.05		19.0%	.74	.60	. 14
80		4/ 8/81	1.08	.95		.79	125628				/ <b>.88</b>	.73	. 1!
81		4/13/81	1.42	1.33		1.07				19.2%	.93	.75	.18
82		4/22/81	.22	.15		.12	19019			22.8%	.70	.54	. 10
83		5/23/81	.23	.17		.13	20055	.04		26.2%	.74	.55	.19
84 85		5/29/81 6/-8/81	.27 .30	.18 .19		.15 .17	24358 27755	.03 .02		16.8% 8.7%	.68 .63	.56 .58	.0
. 86		6/13/81	.59	.49	A	.39	63164	.09		18.9%	.83	.67	.10
88		6/20/81	.16	.07		.08	12507		-1471	-13.3%	.43	.49	0
89		7/12/81	.44	.32		.28	44688			13.5%	.73	.64	.09
90		7/17/81		.11		.09	14711	.02			.62	.51	.1
91		7/20/81	.05	.03		.01	2104	.01		53.0%	.56	.26	.30
92 93		7/27/81 8/14/81	.39 .65	.29 .50		.24 .44		.05 .06		16.8% 12.0%	.75 .77	.62 .68	.1:
94		8/15/81	.33	.23	\	.20	31300			16.4%	.71	.59	.1:
95		8/26/81	.68	.55		.46	74226			15.8%	.81	.68	.1
96		8/29/81	.99	.92	147623	.71	113655	.21	33968	23.0%	.93	.72	.2
97		8/31/81	1.04	.96		.75	120273			21.3%	-92	.72	.2
98		9/ 7/81	.63	.53		.43		.11		20.0%	.84	.68	.1
99		9/21/81	.46 .69	.36 .60		.29 .47	47052 75479			17.4% 21.1%	.77 .87	.64 .68	.13
100		10/ 6/81 10/17/81	.44	.37				.09	14009	23.9%	.83		.19
102		10/17/81	.61	.58		.41					.95	.67	
103		4/ 2/82	. 83					.12	19685		. 85	.70	.1!
104	4	4/ 2/82	.09								.72	.39	.3
105		4/ 2/82	1.06								.73	.73	.0
100		4/ 3/82	.22 .64			.12 .43					.50 .63	.54 .68	0
107		4/16/82 4/16/82	.12			.05					.78	.44	.34
109		5/11/82	.38								.43	.62	19
110		5/15/82	.17								.65	.50	.1
11		5/18/82	.05						615		.34	.26	.0
113		5/22/82	.96								.56		1
114		5/26/82	.17								.41	.50	09
11:		5/27/82 5/29/82	.12 .12								.70 .40	.44 .44	.2( 0
110		6/15/82	.92			.65					.68	.71	0
118		6/20/82	.19								.57		.0
119		6/25/82	.68				74226		-3054		.65	.68	0.
Minim	um •		.05	.01	1439	.01	2104	- 15	-24031		.15	.26	1
Maxim			3.24								.97		.34
Avera			.55						10297	14.6%	.71		.1
Std.D			.51	.49							.17		. 1
Count	٠, :		61						61		61		6
COV	:	•	.94						4204/4	1/, 40/	.24		7.00
Sum	:		33.38	26.87	4297529	22.94	3669388	3.93	628141	14.6%	43.39	36.39	

· 6 Wood Center Total Runoff — Predicted vs Observed Observed Total Runoff [in] <u>6</u> 5 9

Predicted Total Runoff [in]



3.5 Wood Center Total Runoff — Rain vs Residuals 2.5  $\frac{2}{\mathrm{Rain}}$  (in) 15 þ ġ ιÜ <u></u> -.50 -.20 -.30 -.40 .20 은. .50 .40 .30

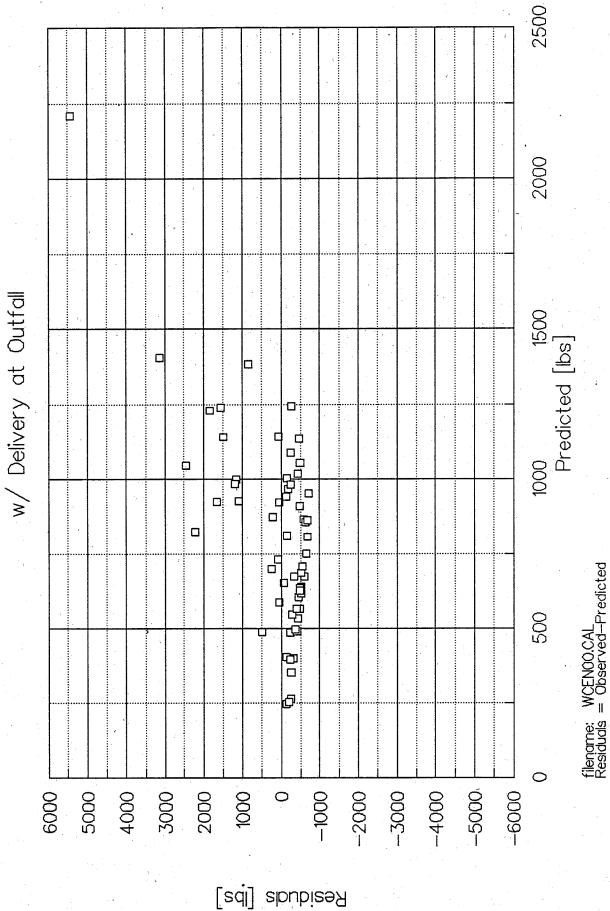
[ni] sloubiseA îtonuA lotoT

filename: WCENOD.CAL

10 11	filename:			N.		SS N.FILT. RESID.	w/o Del		SS Resid w/o Del	w/ Del	Outliers
12 13 14	CODE #	DATE	RAIN (in)		SID. g/l)	(lbs)	[lbs]	[lbs]	[lbs]	[lbs]	outtiers
15	53	3/15/80	.23		98			490		-342	
16	54	4/ 3/80	.16		132		953	605	-787	-439	
17	55 56	4/ 4/80 4/ 6/80	.34 .08		44 210		1028 682	638 353		-527 -263	
18 19	57	4/ 9/80	.29		38		997			-591	
20	60	5/28/80	.76		້ 532		1315	1230	1755	1840	
21	61	6/ 1/80	.30		38		910			-659	
22	62	6/ 2/80	.59 1.11		161 270	805 2801	1019 1326			-137 - 1561	
23 24	63 64	6/ 5/80 6/ 6/80	.66		438				1591	1666	
25	65	6/ 7/80	1.04		348		1121	1046	2381	2456	
26	66	6/19/80	.20		158			685		-505	
27	67	7/ 5/80	.70		438					1161 -240	
28 29	68 69	7/ 9/80 7/15/80	.72 .13		206 188		1165 761	534		-423	
30	70	7/16/80	.06		141					-251	
31	71	7/26/80	1.59		64					-256	
32	72	8/ 2/80	.18	18 8 - 18 - 18 - 18 - 18 - 18 - 18 - 18	244			546			
33 34	73 74	8/ 2/80 8/ 4/80	.17 3.24	>	72 246					5426	*
35	75	8/ 7/80	1.44		180					832	
36	76	8/ 7/80	.48		58	248	690	485	-442	-237	
37	78	8/16/80	.34		45					-504	
38 39	80 81	4/ 8/81 4/13/81	1.08 1.42		280 342					1500 3120	* *
40	82	4/22/81	.22		82		948			-681	
4.1	83	5/23/81	. 23		585	993	866	489	127	504	
42	84	5/29/81	.27		186					-332	*
43 44	85 86	6/ 8/81 6/13/81	.30 .59		336 56					50 -593	e.
45	88	6/20/81	.16		390					-136	
46	89	7/12/81	.44		290	935	958	. 699	-23	236	
47	90	7/17/81	.18		143					-476	
-48 49	91 92	7/20/81 7/27/81	.05 .39		442 57					, -124 -542	
.50	93	8/14/81	.65		49					-706	
51	94	8/15/81	.33		283	661	895	. 811	-234	-150 ·	
52		8/26/81	.68		120					-477	
53 54	96 97	8/29/81 8/31/81	.99 1.04		236 61					1190 -436	
55	98	9/ 7/81	.63		44			855		-621 .	
56	99	9/21/81	.46	8	53	188	985	862	-797	-674	
57	100	10/ 6/81	.69		204					75	
58 59	101 102	10/17/81	.44 .61		116 136		988 1034			-485 -182	
60	103	10/17/81 4/ 2/82	.83		288					1104	
61	104	4/ 2/82	.09		132	86	600	401	-514	-315	
62	105	4/ 2/82	1.06		125					48	
63 . 64	106 107	4/ 3/82 4/16/82	.22 .64		72 764					-413 2228	$p_{i,j} = e^{\frac{i}{2} (j+1)} e^{\frac{i}{2} (j+1)}$
65	108	4/16/82	.12		160			395	-425	-245	
66	109	5/11/82	.38		516	850	1088	1003	-238	- 153	
67	110	5/15/82	.17		524					-71	
68 69	111 113	5/18/82 5/22/82	.05 .96		256 137					-212 -248	
70	114	5/26/82	.17		204					-485	
71	115	5/27/82	.12		164					-358	
72	116	5/29/82	.12		322				-587		
73 77	117	6/15/82	.92		91 748					-487 83	
74 75	118 119	6/20/82 6/25/82	.19 .68		244					212	
76	• • • •	-,,					,-,	-			
77								= -			
78	Minimum :		.05		38 747						
79 80	Maximum : Average :		3.24 .55	22	764 22.738					5426 150	
81	Std.Dev.:		.51		0.147					1088	
82	Count :	:	61		61	61	61	61	61	61	
83	COV :	:	.94		.76					9151	
84 85	Sum : Sum-outli	iers:	33.38		13587	58156 45996				605	•
		· <del>-</del>									

Wood Center Suspended Solids: Observed vs Predicted 0000 w/ Delivery at Outfall Observed [bs] 9 filename: WCENDO.CAL 9 100 1000 Predicted [lbs]

Wood Center Suspended Solids: Predicted vs Residuals w/ Delivery at Outfall



4.00 Wood Center Suspended Solids: Rain vs Residuals w/ Delivery at Outfall 3.00 2.00 Rain [in] filename: WCENOO.CAL Residuals = Observed—Predicted 日 1.00 -2000 0009--4000 2000 4000 0 6000 [edl] albubise9

Hastings 1990 Study Area Results

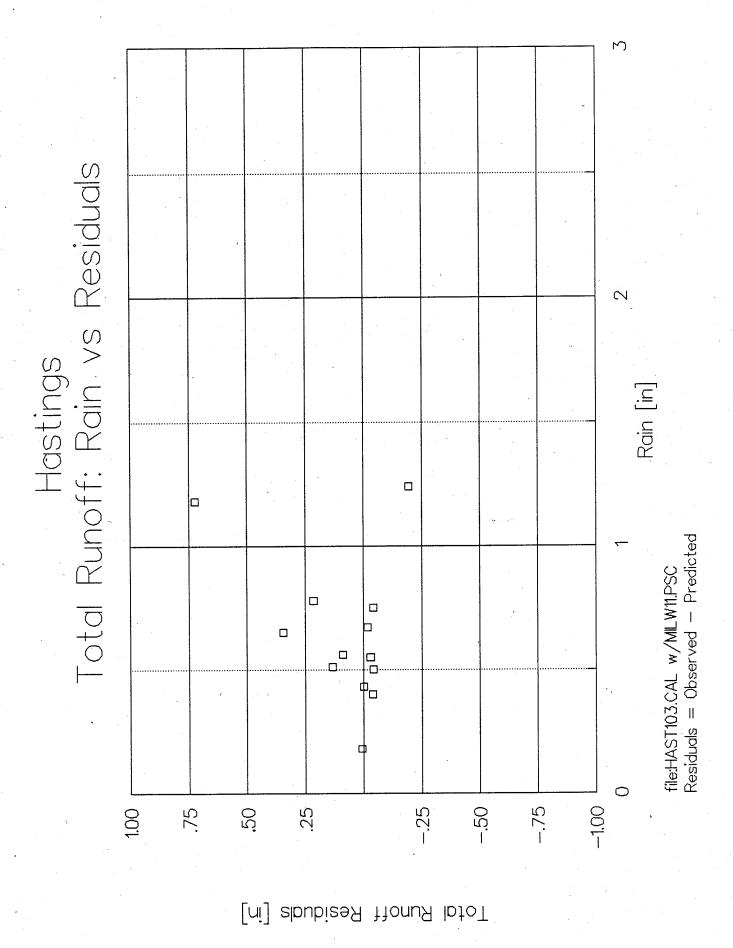
SLAMM Calibration Data Summary Sheet									
Site Data File Name: IHAS	TIOS, DAT	•							
Hastings 1990	Observed	Predicted	Residuals						
Runoff [in]									
Average	0.31	0.22	0.09						
Std Dev	0.29	0.12	<b></b> .						
COV	0.92	0.52	_						
Sum	4.00	2.91	1.14						
Count	13	÷							
Runoff - outliers [in]									
Average	0.21	0,20	0.01						
Std Dev	0.12	0.11							
COV	0.56	0.52							
Sum	2.32	2,24	0,08						
Count	11								
Rv									
Average	0.44	0.34	0.10						
Std Dev	0.25	0.04	-						
COV	0.56	0.11	_						
SS w/Delivery [lbs]									
Average	222	98	135						
Std Dev	367	48							
COV	1,45	0.55							
Sum	Z889	1138	1751						
Count	13								
SS w/Delivery - outliers [lbs]									
Average	68	78	-10						
Std Dev	62	43							
COV	0.92	0.55							
Sum	743	8 <i>5</i> 8	-115						
Count	11								

| A | B | C | D | E | F | G | H | I | J | K | L | M |
Hastings with 1990 Data and MMILW6.RSV,MILW11.PSC,DELIV2.PRR Per
file:HAST103.CAL w/MILW11.PSC Fit
Area [acres]: 32.40 Lin
Area Factor(ACF): 117612
Solids Conversion Factor (SCF): 7.34
[1kg/10^6mg\*2.204lbs/kg\*1liter/0.264gal\*1gal/0.1337ft^3\*1ft/12in\*area(acres)\*43560ft^2/acre] = .2266\*area 0 | Fit 10.00 Line

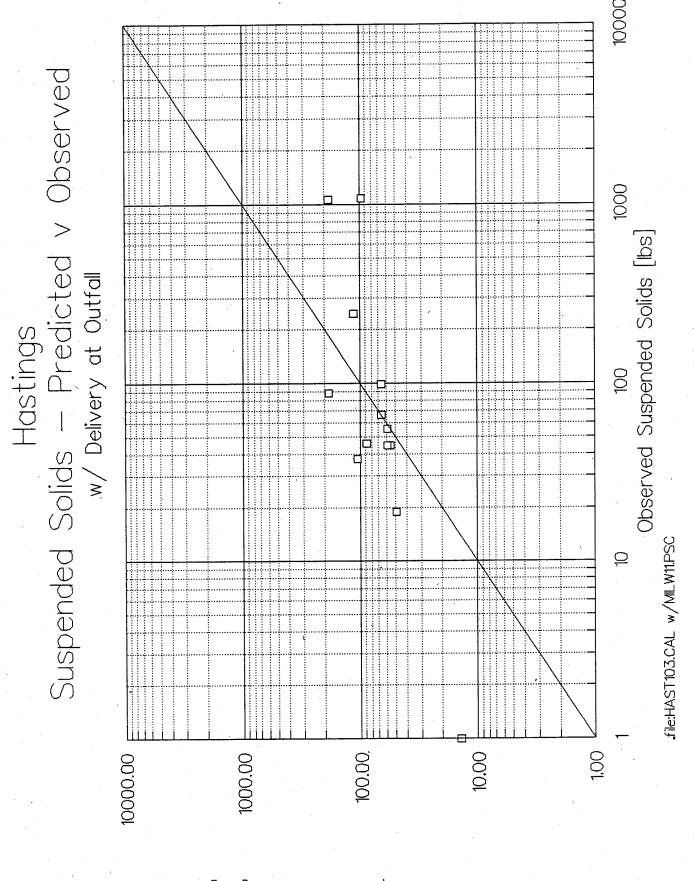
9		•												
10	file:HAST	103.CAL 1	/MILW11	.PSC	OBS	SLAMM	SLAMM	RESID	RESID	RESID/	OBS	SLAMM	RESID	RESID/
11				Obs Ttl	TOTAL	TOTAL '	TOTAL	TOTAL	TOTAL	OBS TTL	TOTAL	TOTAL	TOTAL	OBS TTL
12	CODE	DATE	RAIN	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RV	RV	RV	RV
13	. # .		(in)	(in)	(cu ft)	[in]	(cu ft)	[in]	(cu ft)	[]	(in/in)	(in/in)	(in/in)	.[]
14	2.1		1900											
15	1	3/11/90	.65	.57	66679	.22	26412	.34	40267		.87	.35	.52	
16	2	4/20/90	.75	.22	26049	.26	31058	04	-5009		.30	.35	05	
17	3	5/ 4/90	1.24	.28	32663	.47	55484	19	-22821		.22	.38	16	
18	4	5/ 9/90	.78	.49	57571	.28	32482	. 21	25089		.63	.36	.27	
19	5	5/16/90	.43	.13	15571	.13	15727		-156		.31	.31		01
20	6	5/19/90	.67	.21	25249	.23	27329	02	-2080		.32	.35	03	09
21	6.5	6/ 2/90	.18	.05	5642	.04	4868	.01	774		.27	.23	.04	
22	7	6/13/90	1.18	1.17	137382	.45	52399	.72			.99	.38	.61	.62
23	8	6/16/90	.55	. 15	17988	.18	21594	03	-3606		.28	.34	06	
24	. 9	6/19/90	.40	.08	9774	.12	14362	-:04	-4588		.21	.31	10	
25	10	6/22/90	.50	.12	14267	.16	19070	04	-4803		.24	.33	09	
26	11	6/22/90	.51	.30	35412	.17	19566	.13	15846		.59	.33	.26	
27	13	6/29/90	.56	.28	32829	.19	22112	.09	10717	.33	.50	.34	.16	.32
28														
29	Minimum :	•	.18		5642		4868	19		70	 .21	.23	16	
30	Maximum :		1.24	1.17	137382	.47	55484	.72			.99	.38	.61	.62
31	Average :		.65	.31	36698	.22	26343	.09			-44	.34	.10	
32	Std.Dev.:		.28	.29	33670		· 13716	.22			.25	.04	.24	
33	Count :	•	13	13	13		13	13	13	13	13	13	13	13
34	cov :	:	.44	.92	.92	.52	.52				.56	.11		
35	Sum :	:	8.40	4.06	477076	2.91	342463	1.14	134613	.58	5.72	4.36	1.36	.48

 $\bigcirc$ Hastings Predicted v Observed Observed Total Runoff [in] Total Runoff file:HAST103.CAL w/MILW11.PSC 2 <u>ة</u> 6. 1.00 Predicted Total Runoff [in]

Hastings Total Runoff Residuals vs Predicted Runoff . Predicted Total Runoff [in] file:HAST103.CAL W/MLW11.PSC -1.00 .75 .25 -.25 -.75 .50 -.50 Total Runoff Residuals [in]



```
C || P || Q || R || S || T || U ||
Data a .10
     | A || B || C ||
Hastings with 1990 Data a
                                                                                             || W
                                                                                                       ||X|| Y |
     file:HAST103.CAL w/MILW11 >>>>>>
2
3
     Area [acres]:
                          32.40
     Area Factor(ACF): 117612
4
5
     Solids Conversion Factor
       [1kg/10^6mg*2.204lbs/kg
                                                           Calc SS Calc SS SS Resid SS Resid SS Resid
                                            SS
                                                    SS
10
     file:HAST103.CAL w/MILW11
                                          N.FILT. N.FILT.
11
                 DATE
                          RAIN
                                          RESID. RESID. w/o Del w/o Del
                                                                                       w/ Del
                                                                                                 w/ Del
                                                                                                            Outliers
       CODE
12
                                                                    [lbs]
                                                                                       [lbs]
                                                            [lbs]
                                                                             [lbs]
                                                                                                  []
                                          (mg/l)
                                                   (lbs)
13
        . # .
                          (in)
14
                                                      1082
                                                                         97
                                                                                  857
                                                                                           985
                                                                                                   10.16
                             .65
                                              260
                                                                225
15
                3/11/90
         1
                                               23
                                                                                 -198
                                                                                            -68
                                                                                                    -.64
                                                        37
                                                                235
                                                                        105
16
         2
                4/20/90
                             .75
17
                5/ 4/90
                            1.24
                                               43
                                                        88
                                                                272
                                                                        186
                                                                                 -184
                                                                                            -98
                                                                                                    -.53
         3
                                               68
                                                                        113
                                                                                  23
                                                                                            131
                                                                                                    1.16
                                                                221
                5/ 9/90
                            .78
                                                       244
18
19
         5
                5/16/90
                             .43
                                               46
                                                        45
                                                                189
                                                                         55
                                                                                 -144
                                                                                           -10
                                                                                                    -.19
                                                                                 -159
                                                                                                    -.48
                                               29
                                                       . 46
                                                                205
                                                                         88
                                                                                            -42
20
                5/19/90
                             .67
         6
                                                                                                   -1.00
                                                                                           -14
        6:5
7
                                                0
                                                                169
                                                                         14
                                                                                 -169
21
22
23
24
25
26
27
                6/ 2/90
                             .18
                                                         0
                6/13/90
                            1.18
                                              124
                                                      1063
                                                                282
                                                                        183
                                                                                  781
                                                                                            880
                                                                                                    4.81
                                               59
                                                                                             0
                                                                                                    .004
                                                       66
                                                                206
                                                                         66
                                                                                 -140
        . 8
                6/16/90
                             .55
                                                                                            -30
                                                                                                    -.61
         9
                6/19/90
                             .40
                                               31
                                                        19
                                                                183
                                                                         49
                                                                                 -164
                                               50
25
                6/22/90
                             .50
                                                        45
                                                                183
                                                                         58
                                                                                 -138
                                                                                            -13
                                                                                                    -.23
         10
                                                                                            -3
                                                                                                    -.05
                                                        55
                                                                171
                                                                         58
                                                                                 -116
         11
                6/22/90
                             .51
                6/29/90
                                                                                            32
                                                                                                    .49
                             .56
                                               48
                                                                179
                                                                         66
                                                                                  -81
         13
28
29
30
                             .18
                                                                                 -198
                                                                                            -98
     Minimum:
                                               · / O
                                                         0
                                                                169
                                                                         14
                                              260
                                                      1082
                                                                282
                                                                        186
                                                                                  857
                                                                                            985
     Maximum:
                            1.24
31
32
33
                                                                         88
                                                                                   13
                                                       222
                                                                209
                                                                                            135
     Average:
                             .65
                                               62
     Std.Dev.:
                             .28
                                               64
                                                       367
                                                                35
                                                                         48
                                                                                  348
                                                                                            345
                                                                13
                                               13
                                                        13
                                                                         13
                                                                                   13
                                                                                             13
                              13
     Count
34
     COV
                             .44
                                             1.03
                                                      1.65
                                                                .17
                                                                         .55
                            8.40
                                              806
                                                      2889
                                                               2720
                                                                       1138
                                                                                  169
                                                                                           1751
35
     Sum
                                                                      .~.858
                                                       743
                                                                                           -115
     Less Outliers ==>
```



Predicted Suspended Solids [bs]

Hastings Suspended Solids: Residuals vs Rain w/ Delivery at Outfall Rain [in] file:HAST103.CAL w/MILW11.PSC 1000 -500 -1500500 -1000 1500 0 Suspended Solids Residuals [lbs]

Hastings Total Runoff: Rain vs Residuals Rain [in] file:HAST103.CAL w/MILW11.PSC Residuals = Observed — Predicted ф--.75 -1.00 -.25 .25 .75 .50

[ni] albubiseA flonuA lotoT

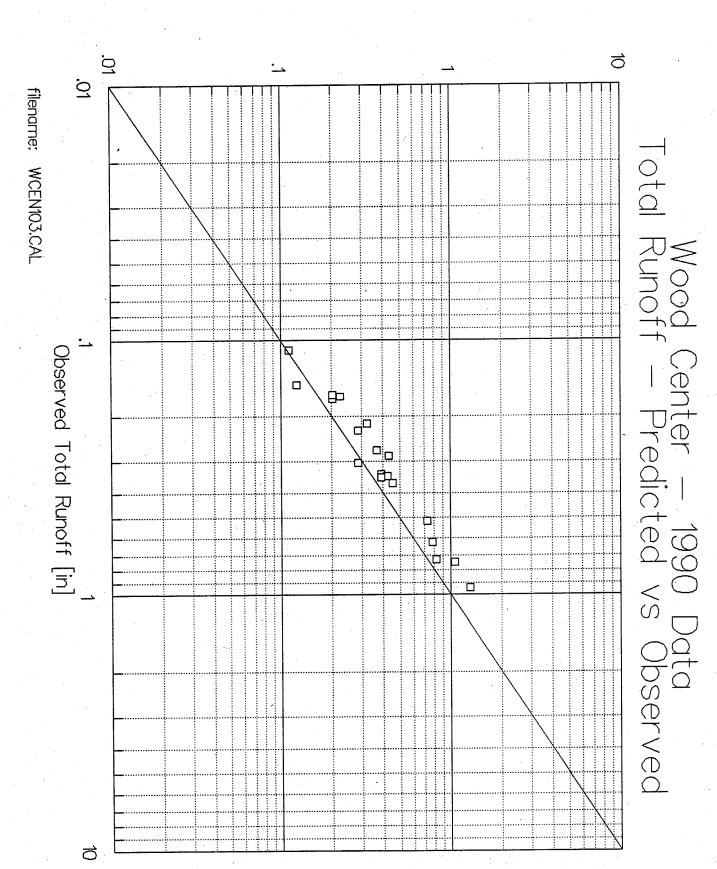
**B9** 

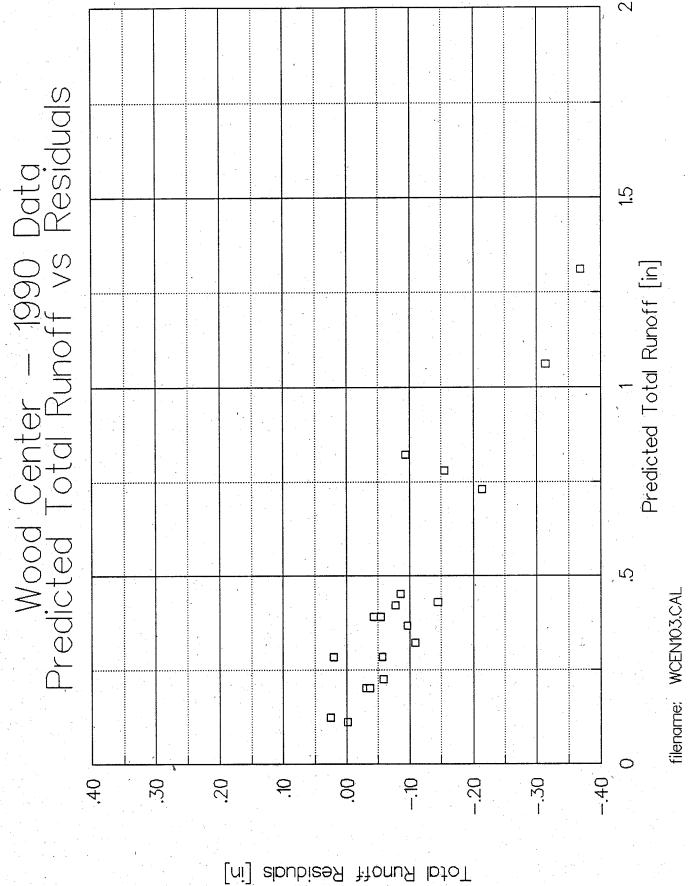
Wood Center 1990 Study Area Results

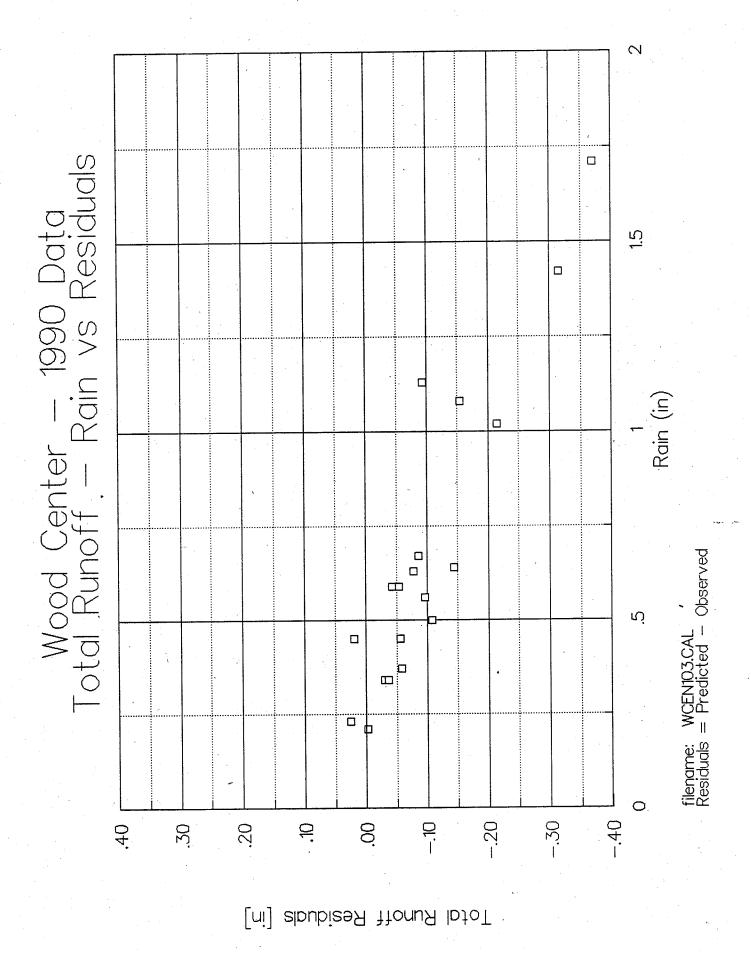
SLAMM Calibration Data Summary Sheet									
Site Data File Name: $\omega c$	EW 103. DA	Τ							
Wood Center - 1990	Observed	Predicted	Residuals						
Runoff [in]									
Average	0.37	0.47	-0.10						
Std Dev	0.23	0.32	-						
COV	0.62	0.68	-						
Sum	7.02	8.91	-1.89						
Count	19								
Runoff - outliers [in]			4						
Average	0.39	0.49	-0.09						
Std Dev	0.24	0.34	-						
COV	0,61	0.69	****						
Sum	5,89	7.32	-1.42						
Count	15								
Fiv									
Average	0.54	0.66	-0.12						
Std Dev	0.07	0.06	<u></u>						
COV	0.13	0.09	_						
SS w/Delivery [lbs]		1	,						
Average	85Z	1038	-186						
Std Dev	948	256							
COV	1.11	0.25							
Sum	13626	16066	-2980						
Count	16								
SS w/Delivery - outliers (lbs)									
Average	1078	1025	53						
Std Dev	996	207	_						
COV	0,92	0,20							
Sum	12936	12303	633						
Count	12								

filename: DATASUM.WK1

9			1						+					
10	filename:	WCEN103	.CAL		OBS	SLAMM	SLAMM	RESID	RESID	RESID/	OBS	SLAMM	RESID	RESID/
11				Obs Ttl	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	OBS TTL	TOTAL	TOTAL	TOTAL	OBS TTL
12	CODE	DATE	RAIN	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RV	RV	RV	RV
13	. # .		(in)	(in)	(cu ft)	[in]	(cu ft)	[in]	(cu ft)	(%)	(in/in)	(in/in)	(in/in)	(%)
14								i .						
15	1001	1/ 3/90	.34	.17	27265	.20	32241	03	-4976	-18.3%	.50		10	
16	1002	1/23/90	.23	. 15	23990	.12	19880	.03	4110	17.1%	.65		.11	17.2%
17	1003	3/ 8/90	.56	27	43467	.37	58843	10	-15376	-35.4%	.49		17	
18	1004	3/11/90	.45	.23	363 <u>8</u> 4	.28	45488	06	-9104	-25.0%	.51		13	
19	1005	3/13/90	.59	.34	54049	.39	62647	05	-8598	-15.9%	.57	.67	10	-17.0%
20	1006	4/ 1/90	.64	.29	45654	.43	68697	14	-23043	-50.5%	.45	.68	23	-52.5%
21	1007	4/ 9/90	.50	.21	34162	.32	51444	11	-17282	-50.6%	.43	.65	22	-52.2%
22	1008	4/20/90	1.02	.51	82363	.73	116621	21	-34258	-41.6%	.50	.72	22	-42.6%
23	1009	5/ 4/90	1.42	.75	119490	1.06	169789	31	-50299	-42.1%	.53	.75	22	-42.6%
24	1010	5/ 9/90	1.08	.62	99868	.78	124559	15	-24691	-24.7%	.58	.73	15	-26.3%
25	1011	5/19/90	.63	.34	55090	.42	67478	08	-12388	-22.5%	.55	.68	13	-24.4%
26	1012.1	6/ 2/90	.34	.16	26367	.20	32241	04	-5874	-22.3%	.48	.60	12	-23.7%
27	1012.2	6/14/90	.37	.17	26701	.22	35959	06	-9258	-34.7%	.45	.61	- 16	-35.2%
28	1013	6/17/90	.59	.35	55811	.39	62647	04	-6836	-12.2%	.59	.67	08	-13.3%
29	1014	6/19/90	.67	.37	58593	.45	72381	09	-13788	-23.5%	.55	.68	13	-24.4%
30	1015	6/22/90	.21	.11	17484	.11	17840	.00	-356	-2.0%	.52		02	-3.7%
31	1016	6/22/90	.45	.30	48689	.28	45488	.02	3201	6.6%	.68	-64	.04	5.4%
32	1017	6/28/90	1.71	.94	150501	1.31	209551	37	-59050	-39.2%	.55	.77	22	-39.9% ~
33	1018	6/28/90	1.13	.73	116296	.82	131266	09	- 14970	-12.9%	.64	.73	09	-13.4%
34								*						
35										•				
36	Minimum:		.21	.11	17484	.11	17840	37	-59050		.43	.54	23	
37	Maximum:		1.71	.94	150501	1.31	209551	.03	4110		.68	.77	.11	
38	Average :		.68	.37	59064	.47	75003	10	- 15939	-27.0%	.54	.66	12	
39	Std.Dev.:	*	.40	. 23		.32	50729	.10	16194		.07	.06	.09	
40	Count :		19	. 19		19	19	19	19		. 19	19	19	
41	COV :		.58	.62	.62	.68	.68				.13	.09	1	
42	Sum :		12.93	7.02		8.91	1425060	-1.89	-302836	-27.0%	10.21		-2.35	-23.0%







42

Sum.

12.93

3856

13626

19673

16606

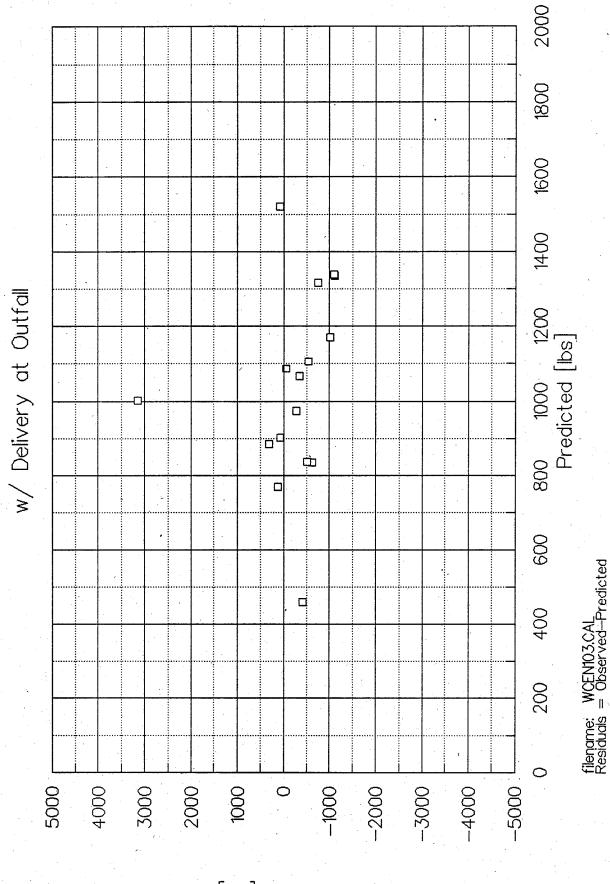
-6047

-2980

Wood Center — 1990 Data Suspended Solids: Observed vs Predicted w/ Delivery at Outfall Observed [bs] 

Predicted [bs]

Wood Center — 1990 Data Suspended Solids: Predicted vs Residuals



Residuals [bs]

4.00 Wood Center — 1990 Data Suspended Solids: Rain vs Residuals w/ Delivery at Outfall 3.00 2.00 Rain [in] filename: WCEN103.CAL Residuals = Observed-Predicted 0009--4000 -20000 2000 0009 4000

Residuals [lbs]

**B10** 

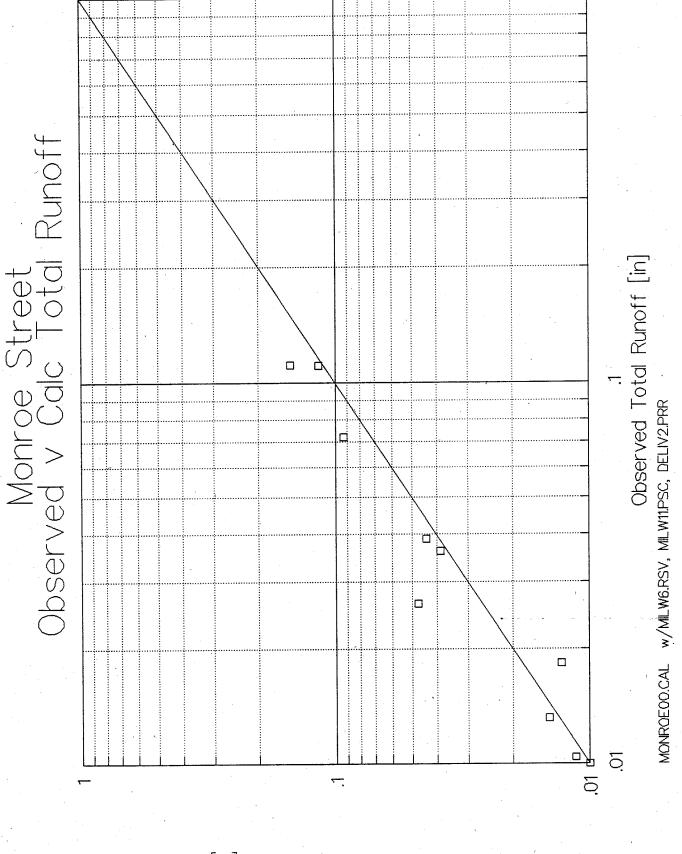
Monroe Street Study Area Results

SLAMM Calibration Data Summary Sheet										
Site Data File Name: MONROEダダ. DAT										
Momoc St.	Observed	Predicted	Residuals							
Runoff (in)										
Average	0.04	0.05	-0.01							
Std Dev	0.04	0.05								
COV	0.87	०.८१								
Sum	0,44	0,53	-0.09							
Count	10									
Runoff - outliers (in)										
Average	0.04	0.04	-0.01							
Std Dev	0.03	0.04	<del></del>							
COV	0.90	0.86	-							
Sum	0.33	0.38	-0.05							
Count	9									
Flv			·							
Average	0.12	0.14	-0.02							
Std Dev	0,04	0.03								
COV	0.32	0,20	_							
SS w/Delivery [lbs]										
Average	1018	1057	-39							
Std Dev	1242	389								
COV	1.22	0,37								
Sum	8142	8452	-310							
Count	8									
SS w/Delivery - outliers (lbs)										
Average	1126	1020	106							
Std Dev	1292	403								
COV	1.15	0,39	_							
Sum	7882	7139	743							
Count	7									

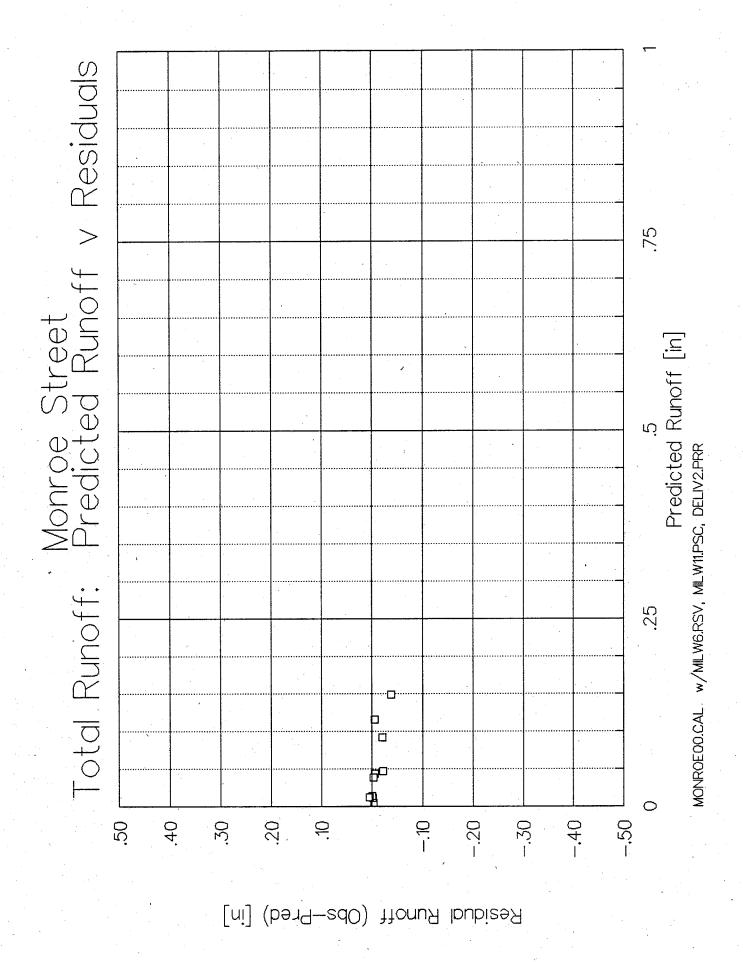
filename: DATASUM.WK1

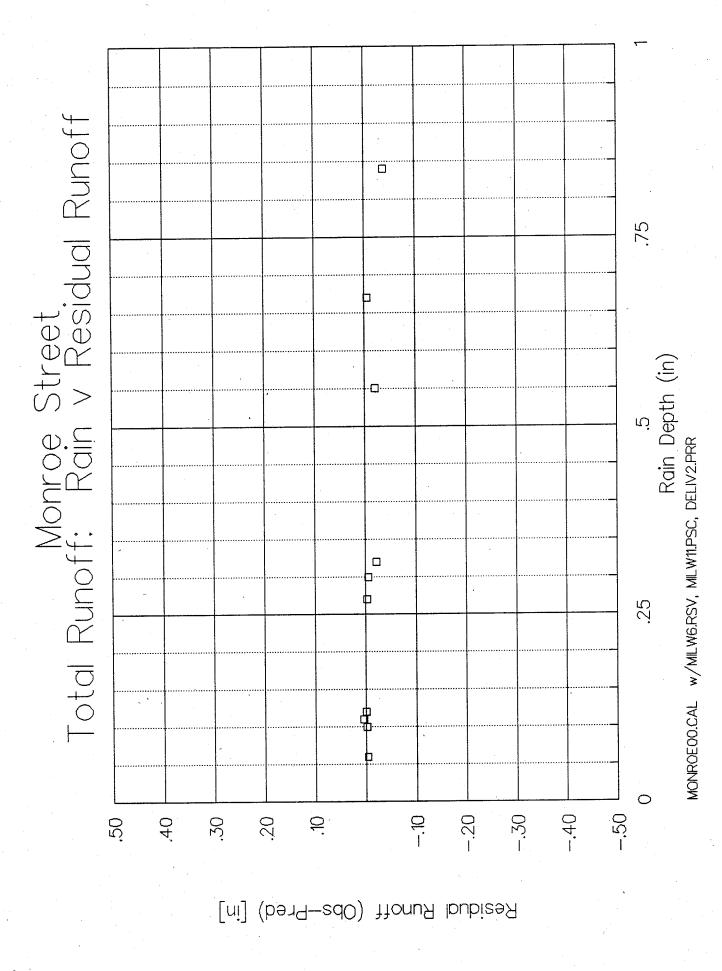
JGV/RTB

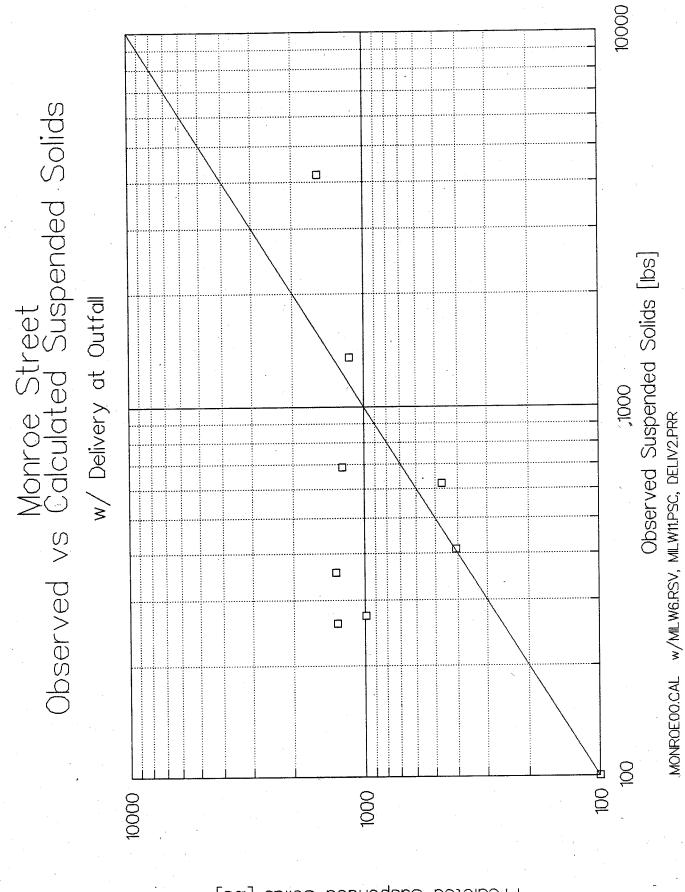
8														
0.														
10	MONROEOO.	CAL w/	MILW6.	RSV, MILI	W11.PSC.	DELIV2.	PRR	RESID	RESID	RESID/	OBS	CALC	RESID	RESID/
11					Obs Ttl			TOTAL	TOTAL	OBS TTL	TOTAL	TOTAL	TOTAL	OBS TTL
12	CODE	DATE	RAIN	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF		R∨.	R√	R∨	
13	. # .		(in)	(in)	(cu ft)	[in]	(cu ft)		(cu ft)	(%)	(in/in)	(in/in)	(in/in)	[frac]
14	• " •		X,	<b>、,</b>	(02,			• • • • • • • • • • • • • • • • • • • •		4	• • • • • • • • • • • • • • • • • • • •			
15	1 .	910505	.84	.111	98857	. 15	132743	04	-33886	34	.13	.18	05	36
16	3	910521	.06	.002	1448	.01	4702	.00	-3254	-2.25	.03	.09	06	-2.32
17	· 4	910525	.1Ò	.010	9242	.01	10146	.00	-904	10	.10	.11	01	06
18	5	910530	.12	.013	11699	.01	12878	.00	-1179	10	.11	.12	01	09
19	6	910530		.018	16317	.01	11497	.01	4820	.30	.17	.12	.05	.28
20	7	910610	.30		34633	.04	39007	.00	-4374	13	.13	.15	02	16
21	8	910612	.55		64144	.09	82267	02	-18123	28		.17	04	30
22	. 9	910613	.32		23412	.05	42223	02			.08	.15	07	82
23	10	910701	.27		32234	.04	34328	.00		06	.13	.14	01	04
24	11	910707			98512		103312	01		05	.17	.17	005	03
25												·		•
26									ı	,				
27	Maximum:		.84	.11	98857	.15	132743	.01	4820	.30	.17	.18	.05	.28
28	Minimum	=	.06		1448	.01	4702				.03	.09	07	-2.32
29	Average :	-	.33			.05	47310			38	.12	. 14	02	39
30	Count		10		10	10	10				10	10	10	10
31	Std.Dev.		. 25		34088	.05	41935	.01	11094	.68	.04	.03	.03	.70
32 <sub>\</sub>	Sum	• •	3.34		390498	.53	473103				1.18	1.40		
33	COV	•	.76		.87	.89	.89				.33	.20		
34	Outlier A	Adi:				.07	,							
J-4 .	outer /	·~] .												



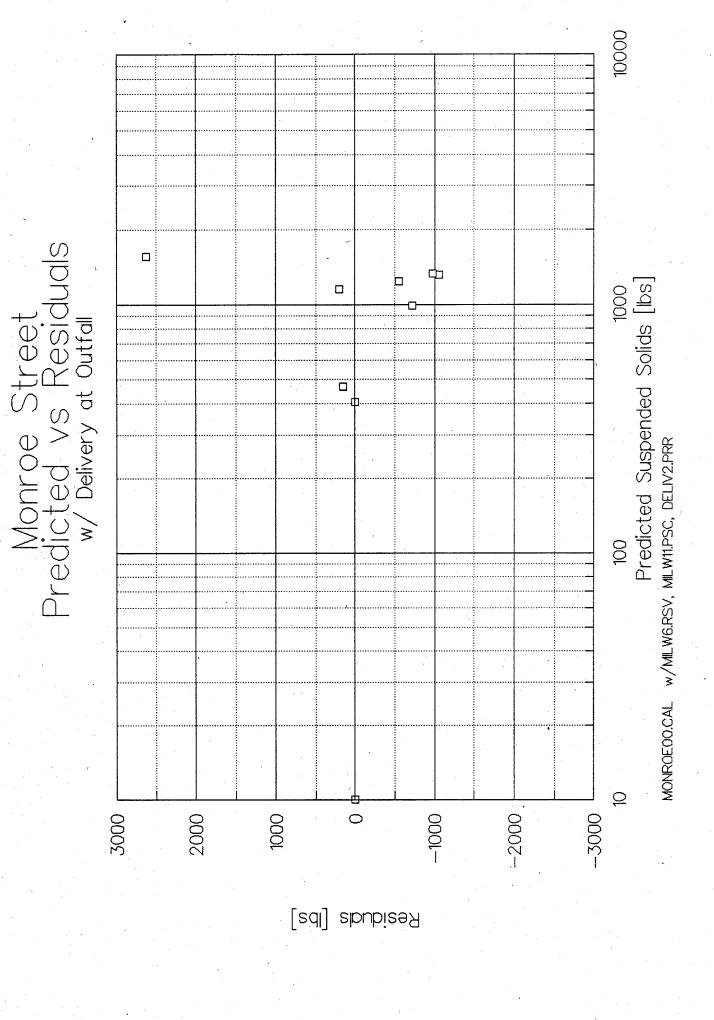
Calculated Total Runoff [in]







Predicted Suspended Solids [bs]



Monroe Street Suspended Solids Rain vs Residuals W/ Delivery at Outfall .75 .5 Rain [in] MONROE00.CAL w/MLW6.RSV, MLW11.PSC, DELIV2.PRR -3000 -1000-20000 1000 2000 3000

Residuals [lbs]

```
| A || B || C || D || F || G || H || I || J || K || L || M || N || O |
Monroe Street Copper Analysis
     Filename: MONROE4.CAL
3
     Area(ac 244.95
     Total Area Fac 889169
     Solids Conv Factor(SCF):
                                     6.2E-8
     6
8
     TOTAL RECOVERABLE COPPER CONCENTRATIONS, UG/L, at OUTFALL
9.
10
                             Obsrvd Obsrvd
                                                     Pred
                                                                 0bsrvd
                                                                                  Pred
                                                   Ttl Cu
                                                                 Ttl Cu
                                                                                Ttl Cu
       CODE DATE
                      RAIN
                             Runoff
                                     Ttl Cu
11
                                                   [ug/L]
                                                                   [lbs]
                                                                                 [lbs]
12
      . # .
                     INCHES
                             [ft^3]
                                     [ug/L]
13
                                                                   .0309 -1.51
                                                                                  .072 -1.14
                              98857
                                          5
                                               .70
14
            5/5/91
                        .84
15
            5/17/91
        2
                         .1
                        .06
                               1448
        3
            5/21/91
16
                                                                   .0254
                                                                                  .024
                                                                                        -1.62
                                                       38
                                                                         -1.60
17
        4
            5/25/91
                         .1
                               9242
                                          44
                                              1.64
                              11699
                                              1.38
                                                       22
                                                                   .0175
                                                                          -1.76
                                                                                 .018
                                                                                        -1.74
        5
            5/30/91
                        .12
                                          24
18
                                              1.32
                                                       21
                                                                   .0214
                                                                          -1.67
                                                                                  .015
                                                                                        -1.82
                              16317
19
        6
            5/30/91
                        .11
                                          21
             6/10/91
                              34633
                                          4
                                               .60
                                                       19
                                                                   .0086
                                                                         -2.06
                                                                                  .046
                                                                                        -1.34
20
        7
                         .3
                        .55
                              64144
                                          12
                                              1.08
                                                       12
                                                                   .0481
                                                                          -1.32
                                                                                   .06
                                                                                       -1.22
21
            6/12/91
        8
                                                                                  .041
                                                                                        -1.39
                              32234
                                                                   .0664
                                                                          -1.18
22
        10
            7/1/91
                        .27
                                         33
                                              1.52
                                                       19
23
            7/7/91
                              98512
                                          20
                                              1.30
                                                       11
                                                                   .1230
                                                                          -.91
                                                                                   .07
                                                                                        -1.15
                        .67
24
                                                                                     8
25
                         10
                                          8
     Count
                                          4
                                                                   .0086
                                                                                 .0150
     Minimun
                        .06
26
                                                                   .1230
                                                                                 .0720
                                          44
27
     Maximum
                        .84
                        .31
                                          20
                                                                   .0427
                                                                                  .0433
28
     Average
                                          13
                                                                   .0349
                                                                                 .0213
     Stnd Dev
29
                        .26
                                                                                   .49
     COV
                        .85
                                         .63
                                                                     .82
                                                                   .0316
                                                                                  .0372
31
     Geo Mean
                                                                   .3413
                                                                                 .3460
32
     Sum
33
34
35
     DISSOLVED COPPER, UG/L, at OUTFALL
                                                                                  Pred
                             Obsrvd Obsrvd
                                                     Pred
                                                                  0bsrvd
36
                                                                                Dis Cu
                                                   Dis Cu
                                                                 Dis Cu
37
       CODE DATE
                       RAIN
                             Runoff
                                     Dis Cu
       . # .
                             [ft^3]
                                                   [ug/L]
                                                                   [lbs]
                                                                                 [lbs]
38
                     INCHES
                                     [ug/L]
39
                                                                                  .035
                              98857
                                               .48
                                                                   .0185 -1.73
                                                                                       -1.46
40
             5/5/91
                        .84
                                          3
41
             5/17/91
        2
                         .1
42
                               1448
        3
             5/21/91
                        .06
43
             5/25/91
                         .1
                               9242
                                          11
                                              1.04
                                                                   .0063
                                                                         -2.20
                                                                                  .003
                                                                                        -2.52
             5/30/91
                                                                   .0073
                                                                          -2.14
                                                                                  .003
                                                                                        -2.52
                              11699
                                          10
                                              1.00
44
        5
                        .12
                                                                         -1.95
                                                                                  .003
                                                                                        -2.52
                                              1.04
                                                        4
                                                                   .0112
45
             5/30/91
                        .11
                              16317
                                          11
                                          2
                                               .30
                                                        4
                                                                   .0043
                                                                          -2.36
                                                                                   .01
                                                                                        -2.00
46
        7
             6/10/91
                              34633
                         .3
                                                                   .0240
                                                                         -1.62
                                                                                  .021
                              64144
                                                        4
                                                                                        -1.68
                        .55
                                           6
                                               .78
47
         8
             6/12/91
         10 `
            7/1/91
                        .27
                              32234
                                           8
                                               .90
                                                                   .0161
                                                                          -1.79
                                                                                  .009
                                                                                        -2.05
48
                                              ..30
                                                                   .0123
                                                                          -1.91
                                                                                . .027
                                                                                        -1.57
           7/7/91
                        .67
                              98512
                                           2
49
         11
50
51
                         10
                                          8
     Count
                                                                   .0043
                                                                                  .0030
                                           2
52
     Minimun
                        .06
53
     Maximum
                        .84
                                          11
                                                                   .0240
                                                                                 .0350
                                          7
                                                                   .0125
                                                                                  .0139
                        .31
54
     Average
55
     Stnd Dev
                        .26
                                           4
                                                                   .0063
                                                                                  .0115
                                         .55
```

5

56

57

58

59 60 COV

Sum

Geo Mean

.85

.50

.0109

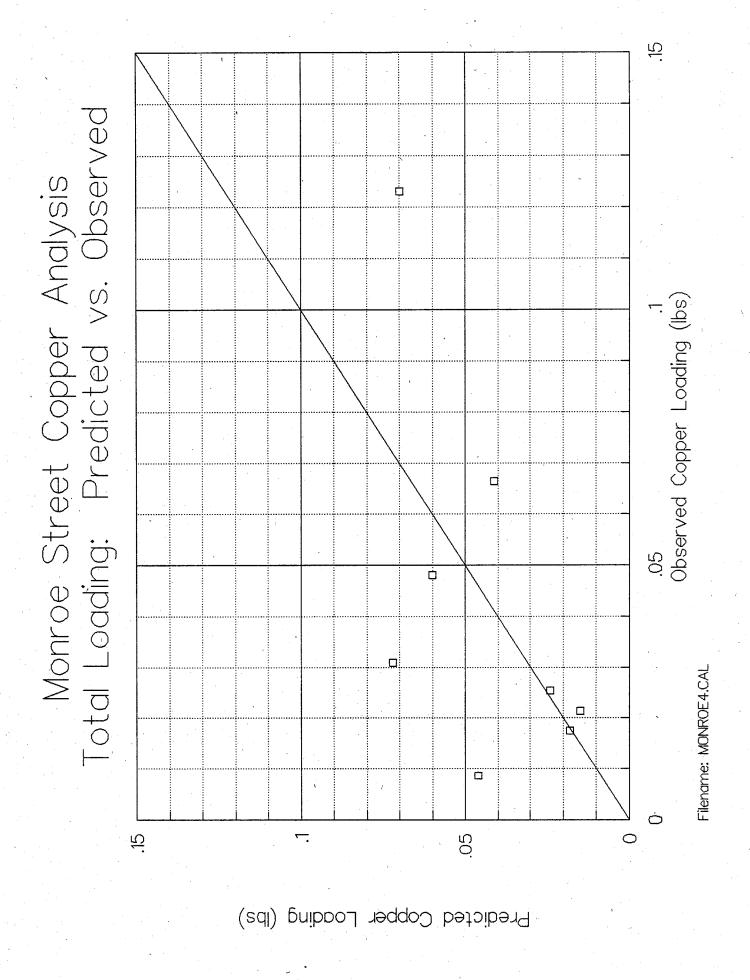
.1001

.83

.0091

.1110

01							-				
62	PARTIC	ULATE CO	PPER, UG	/L, at 0	DUTFALL						
63			•		Obsrvd Obsrvd		Pred	0bsrvd		Pred	
64	CODE DATE		CODE DATE RAIN RU		Part Cu	Pa	rt Cu	Part Cu	Pa	art Cu	
65	. # .		INCHES	[ft^3]	[ug/L]	[	[ug/L]	[lbs]		[lbs]	:
66											
67	1	5/5/91	.84	98857	`2	.30	5	.0123	-1.91	.037	-1.43
68	2	5/17/91	.1		0						
69	3	5/21/91	.06	1448	0						
70	4	5/25/91	.1.	9242	33	1.52	34	.0190	-1.72	.021	-1.68
71	5	5/30/91	.12	11699	14	1.15	18	.0102	-1.99	-014	-1.85
72	6	5/30/91	.11	16317	10	1.00	17	.0102	-1.99	.012	-1.92
73	7	6/10/91	.3	34633	2	.30	15	.0043	-2.36	.036	-1.44
74	8	6/12/91	.55	64144	6	.78	8	.0240	-1.62	.038	-1.42
75	10	7/1/91	.27	32234	25	1.40	15	.0503	-1.30	.032	-1.49
76	11	7/7/91	.67	98512	18	1.26	7	.1107	96	.043	-1.37
77											
78	Count		10		10			8		8	
79	Minimu	ın	.06		0			.0043		.0120	
80	Maximu	ım	.84		33			.1107		.0430	
81	Averag	je	.31		11			.0301		.0291	
82	Stnd D	ev	.26		11			.0332		.0111	
83	COV		85		.98			1.10		.38	
84	Geo Me	ean			9			.0186		.0265	
85	Sum							.2412		.2330	



## B11

**Syene Road Study Area Results** 

SLAMM Calibration Data Summary Sheet											
Site Data File Name: S YE	Site Data File Name: SYEVE ゆゆ、DAT										
Syene Rd.	Observed	Predicted	Residuals								
Runoff [in]											
Average	0,37	0.27	0.10								
Std Dev	0.36	0.23	_								
cov	0.96	0.84	_								
Sum	4.12	2.97	1.15								
Count											
Runoff - outliers (in)											
Average	•		,								
Std Dev											
COV											
Sum											
Count											
Rv											
Average	0.55	0.43	0.12								
Std Dev	0.20	0.11									
COV	0.37	0.25	-								
SS w/Delivery [lbs]			·								
Average	958	1032	-74								
Std Dev	809	609	·								
COV	0.84	0.59									
Şum	10536	11,351	-815								
Count	11,										
SS w/Delivery – outliers (lbs)											
Average											
Std Dev		,									
COV											
Sum	1										
Count											

filename: DATASUM.WK1

JGV/RTB

| A || B || C || D || E || F || G || H || I || J || K|| L || M || N || O | Syene Road Data Analysis SYENEOD.CAL w/MILLW11.PSC

Area [acres]: 115.72
Area Factor: 420064
Solids Conversion Factor (SC 26.23
[1kg/10^6mg\*2.204lbs/kg\*1liter/0.264gal\*1gal/0.1337ft^3\*1ft/12in\*area(acres)\*43560ft^2/acre] = .2266\*area

9														
10	O SYENEOO.CAL W/MILW11.PSC				OBS	SLAMM	SLAMM	RESID	RESID	RESID/	OBS	SLAMM	RESID	RESID/
.11				Obs Ttl	TOTAL	TOTAL	TOTAL	TOTAL ;	TOTAL	OBS TTL	TOTAL	TOTAL	TOTAL	OBS TTL
12	CODE	DATE	RAIN	RUNOFF	RUNOFF :	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RUNOFF	RV	RV	RV	RV
13	. # .		(in)	(in)	(cu ft)	[in]	(cu ft)	[in]	(cu ft)	[ ]	(in/in)	(in/in)	(in/in)	[]
. 14									2			-		
15	11	910408	1.22	.79	331567	.64	270475	. 15	61092	.18	.65	.53	.12	.18
16	13	910412	1.27	1.15	482944	.67	282349	.48	200595	.42	.91	.53	.38	.41
17	14	910413	.89	.75	315722	.45	190960	.30	124762	.40	.84	.51	.33	.40
18	16	910505	.60	.37	154708	.30	124813	.07	29895	.19	.61	.50	11	.19
19	16	910517	.07	.02	8372	.02	8013		359	.04	.28	.27	.01	.05
20	17	910518	.71	.46	194658	.36	149700	11	44958	.23	.65	.50	. 15	.23
21	18	910521	.15	.07	29274	.05	23099	.01	6175	.21	.46	.37	.09	.20
22	19	910525	.04	.01	3215	.01	3121		94	.03	.19	.19		.01
23	21	910610	.34	.15	64231	.15	64510		-279		.45	.45		
24	22	910612	.40	.20	82234	.19	78826	.01	3408	.04	.49	.47	.02	.04
25	23	610613	.28	.15	62979	.12	50969	.03	12010	.19	.54	.43	.11	.20
26														
27	Minimu	m :	.04	.01	3215	.01	3121		-279		.19	.19		
28	Maximu	m :	1.27	1.15	482944	.67	282349	.48	200595	.42	.91	.53	.38	.41
29	Averag	e :	.54	.37	157264	.27	113349	.10	43915	.18	.55	.43	.12	.17
30	Std.De	v.:	.42	.36	150278	.23	95148	.15	61372	.13	.20	.11	.12	.·14
31	Count	:	11	11	- 11	11	11	11	11	11	11	11	11	11
32	COV	:	.77	.96	.96	.84	.84				.37	.25		
33	Sum	:	5.97			2.97		1.15	483069	1.93				

 $\bigcirc$ v Observed Syene Road - Predicted v Observed Total Runoff [in] Total Runoff — ₫▫ SYENEDOLCAL W/MLW11.PSC 5 . 日 10.00 100 9

Predicted Total Runoff [in]

Syene Road Total Runoff Residuals vs Predicted Runoff . Predicted Total Runoff [in] SYENEDO.CAL W/MLW11PSC -.50 -.25 .50

Total Runoff Residuals [in]

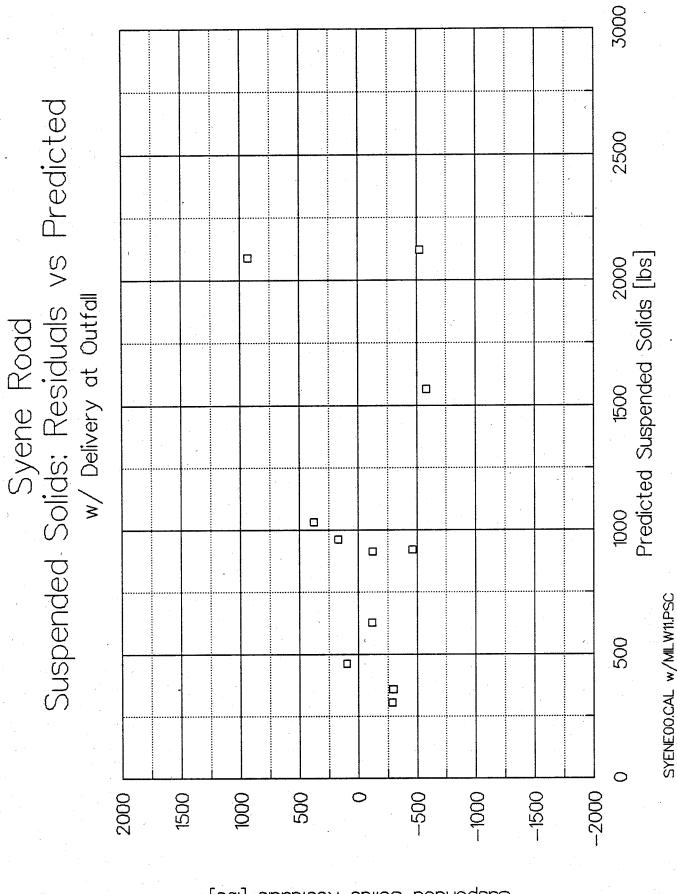
Syene Road Total Runoff: Rain vs Residuals Rain [in] Ŋ SYENEOO.CAL w/MLW11PSC Residuds = Observed - Predicted Ö -.50 **Q** -.40 .20 <u>-</u>.9 -.20 -.30 .40 .30

Total Runoff Residuals [in]

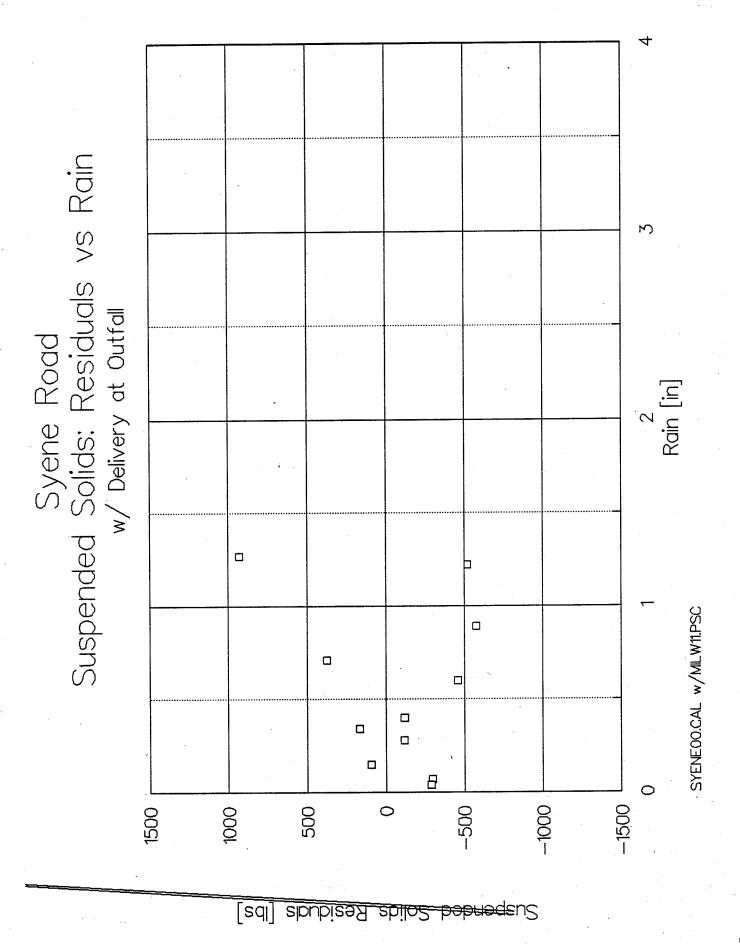
1 2 3 4 5 6 7 8	SYENEO Area [ Area F Solids	Road Da O.CAL w acres]:	/MILW1 >>>> >>>> sion F	S	<b>T</b>	<b>  U  </b>  -	v	<b>w</b>	<b>x</b> [	Y	<b>z   </b>	AB
9	SYENEO	O.CAL W	/MILW1			-	Calc SS	Calc SS	SS Resid	SS Resid	SS Resid	
11					0bsrvd	Obsrvd						
12	CODE	DATE	RAIN		TSS	TSS	w/o Del		w/o Del	w/ Del	w/ Del	Outliers
13	. # .		(in)		(mg/l)	(lbs)	[lbs]	[lbs]	[lbs]	[lbs]	[ ]	
14	44	040/00	4 00		-	7 150/	2457	2118	-559	-524	.75	
15	11	910408			77				898	929	1.44	
16	13	910412			100				-632	-578	.63	
17	14	910413			50					-458	.50	
18	16	910505	.60		48				-536	-436		
19	16	910517			120				-495	378	.17	
20	17	910518			110				317		1.37	
21	18	910521	.15		304			461	-65 -65	95	1.21	
22	19	910525			86				-487	-289	.05	•
- 23	21	910610			28		1134		-3	168	1.17 .87	
24	. 22	910612			154			, 912	-244 -256	-121 -116	.87 .82	
25	23	610613	.28		130	511	767	627	-230	-110	.02	
26			•			•	FA7	705	-632	-578		
27	Minimu		.04		41				-632 898	929		
28	Maximu		1.27		304				-188	-74		
29	Averag		.54		133							
30	Std.De	:	.42		87				440	426 11		
31	Count		11		1:			11	11	11		
32	COV	•	.77		.6				2011	045	*	
33	Sum	:	5.97		146	1 10536	12600	11351	-2064	-815		

Syene Road Suspended Solids — Predicted v Observed w/ Delivery at Outfall Observed Suspended Solids [lbs] þ SYENEGO.CAL W/MILW11.PSC

Predicted Suspended Solids [bs]



Suspended Solids Residuals [lbs]

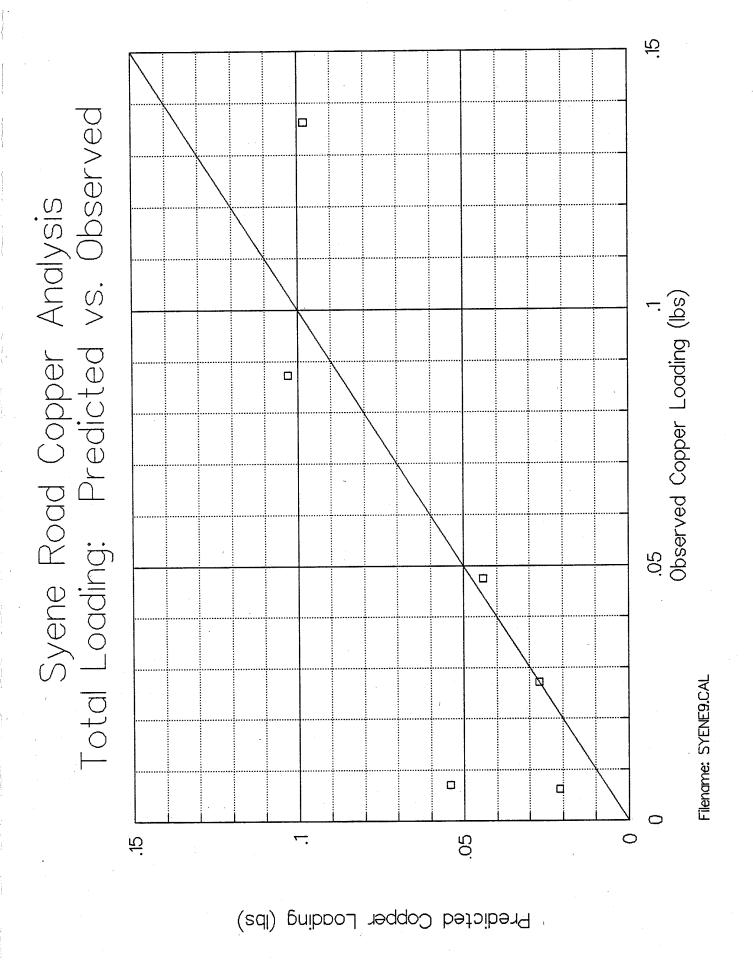


```
| A | | B | | C | | D | | F | | G | | H | | I | | J | | K | | L | | M |
         Syene Road Copper Analysis
         Filename: SYENE9.CAL
         Area(ac):
                                        .000
         Total Area Fac
                                                                    6.2E-8
         Solids Conv Factor(SCF):
         [1kg/10^9ug*2.204lbs/kg*1liter/0.264gal*1gal/0.1337ft^3*runoff[ft^3]*conc[ug/liter] = [1kg/10^9ug*2.204lbs/kg*1liter/0.264gal/0.134b] = [1kg/10^9ug*2.204b] = [1kg/10^9ug*2.004b] = [1kg/10^9ug*2.004b
                      = 6.244E-08*runoff[ft^3]*conc[ug/L] =>[lbs]
         TOTAL RECOVERABLE COPPER CONCENTRATIONS, UG/L, at OUTFALL
10
                                                                                                                       0bsrvd
                                                                                                Pred
                                                                                                                                                      Pred
11
                                                     Obsrvd Obsrvd
                                         RAIN Runoff Ttl Cu
                                                                                             Ttl Cu
                                                                                                                        Ttl Cu
                                                                                                                                                  Ttl Cu
            CODE DATE
12
                                                                                                                                                     [lbs]
                                                                                                                          fibsi
                                     INCHES
                                                     [ft^3]
                                                                                              [ug/L]
13
           . # .
                                                                    [ug/L]
14
                                                                                                                                                       .027
                                            .07
                                                         8372
                                                                            52 1.72
                                                                                                                          .0272 -1.57
             16.5 5/17/91
15
                                                                                                    30
                                                                                                                          .0475
                                                                                                                                                       .044
                                                                                                                                                                 -1.36
                                                                                                                                      -1.32
16
              18 5/21/91
                                            .15
                                                       29274
                                                                            26
                                                                                  1.41
                     5/25/91
                                                                                   1.49
                                                                                                   106
                                                                                                                          .0062
                                                                                                                                       -2.21
                                                                                                                                                       .021
                                                                                                                                                                 -1.68
               19
                                            -04
                                                        3215
                                                                            31
17
                                                                                                    24
                                                                                                                                        -.87
                                                                                                                                                       .098
                                                                                                                                                                 -1.01
                                                                                   1.53
                                                                                                                          . 1364
                                            .34
                                                                            34
18
              21
                      6/10/91
                                                       64231
                                                                                                                                                       .103
                                                                                                                                                                  -.99
              22
                      6/12/91
                                            .40
                                                       82234
                                                                            17
                                                                                   1.23
                                                                                                     21
                                                                                                                          .0873
                                                                                                                                      -1.06
19
                                                                                   1.74
                                                                                                     32
                                                                                                                           .0070
                                                                                                                                       -2.15
                                                                                                                                                       .054
                                                                                                                                                                  -1.27
                                                         2051
                                            .17
                                                                            55
20
                      7/1/91
21
                                                                              6
                                               6
22
         Count
                                                                                                                          .0062
                                                                                                                                                       .021
23
         Minimun
                                            .04
                                                                            17
                                            .40
                                                                            55
                                                                                                                          .1364
                                                                                                                                                       .103
24
         Maximum
                                                                            36
                                                                                                                          .0519
                                                                                                                                                       .058
25
         Average
                                            .20
         Stnd Dev
                                            .13
                                                                            14
                                                                                                                          .0468
                                                                                                                                                       .032
26
                                                                                                                              .90
                                                                                                                                                        .55
                                                                           .38
27
         COV
                                            .68
                                                                                                                                                       .049
28
         Geo Mean
                                                                            33
                                                                                                                           .0296
                                                                                                                          .3116
                                                                                                                                                       .347
29
         Sum
30
31
         DISSOLVED COPPER, UG/L, at OUTFALL
32
                                                     Obsrvd Obsrvd
                                                                                                 Pred
                                                                                                                        0bsrvd
                                                                                                                                                      Pred
33
                                                     Runoff Dis Cu
                                                                                             Dis Cu
                                                                                                                        Dis Cu
                                                                                                                                                  Dis Cu
                                          RAIN
34
             CODE DATE
                                                                                                                          [lbs]
                                                                                                                                                     [lbs]
                                                                                              [ug/L]
35
                                      INCHES
                                                      [ft^3]
                                                                     [ug/L]
            .#.
36
                                                                                    1.52
                                                                                                                          .0173
                                                                                                                                                       .006
                                                                                                                                                                 -2.22
                                            .07
                                                         8372
                                                                                                     13
                                                                                                                                     -1.76
                                                                            33
37
             16.5 5/17/91
                                                                                                                                                       .016
                                                                                                                                                                 -1.80
                                            .15
                                                       29274
                                                                              9
                                                                                     .95
                                                                                                     11
                                                                                                                           .0165
                                                                                                                                      -1.78
38
               18 5/21/91
                                            .04
                                                        3215
                                                                                   1.08
                                                                                                                           .0024
                                                                                                                                       -2.62
                                                                                                                                                       .003
                                                                                                                                                                 -2.52
                      5/25/91
                                                                            12
                                                                                                     14
39
               19
                                                                                                                                                       .044
                                                                                                                           .0481
                                                                                                                                                                 -1.36
                                                                                                                                      -1.32
                      6/10/91
                                            .34
                                                        64231
                                                                            12
                                                                                  1.08
                                                                                                     11
40
               21
                                            .40
                                                                                      .78
                                                                                                                           .0308
                                                                                                                                      -1.51
                                                                                                                                                       .053
                                                                                                                                                                 -1.28
                      6/12/91
                                                       82234
                                                                              6
                                                                                                     11
41
               22
                                                                                                                           .0018 -2.75
                                                                                                                                                       .019
                                                                                                                                                                 -1.72
                                                                                   1.15
                                                                            14
                                                                                                     11
42
               24
                      7/1/91
                                            .17
                                                         2051
43
                                                                              6
                                                                                                                                 6
                                                                                                                                                            6
                                               6
44
         Count
                                                                                                                                                       .003
                                                                                                                           .0018
                                            .04
                                                                              6
45
         Minimun
                                                                                                                                                       .053
                                            .40
                                                                            33
                                                                                                                           .0481
46
         Maximum
                                                                                                                           .0195
                                                                                                                                                       .024
                                            .20
                                                                             14
47
         Average
                                                                              9
                                                                                                                           .0162
                                                                                                                                                       .019
48
         Stnd Dev
                                            .13
                                                                                                                              .83
                                                                                                                                                         .79
49
          COV
                                            .68
                                                                           .61
         Geo Mean
                                                                             12
                                                                                                                           .0110
                                                                                                                                                       .015
50
                                                                                                                                                       .141
                                                                                                                          .1168
51
          Sum
52
.53
54
          PARTICULATE COPPER, UG/L, at OUTFALL
                                                      Obsrvd Obsrvd
                                                                                                 Pred
                                                                                                                        Obsŕvá
                                                                                                                                                       Pred
55
56
             CODE DATE
                                          RAIN
                                                     Runoff Part Cu
                                                                                            Part Cu
                                                                                                                      Part Cu
                                                                                                                                                 Part Cu
                                                                                                                           [lbs]
                                                                                                                                                      [lbs]
57
                                      INCHES
                                                      [ft^3] [ug/L]
                                                                                              [ug/L]
            . # .
58
                                                         8372
                                                                             19
                                                                                                     41
                                                                                                                           .0099
                                                                                                                                       -2.00
                                                                                                                                                       .021
                                                                                                                                                                 -1.68
59
              16.5 5/17/91
                                             .07
                                                                                    1.28
                                                                                                                                                                  -1.57
                                                        29274
                                                                             17
                                                                                    1.23
                                                                                                     19
                                                                                                                           .0311
                                                                                                                                       -1.51
                                                                                                                                                       .027
                     5/21/91
                                             . 15
60
               18
                                                                                                                                                       .018
                      5/25/91
                                                         3215
                                                                             19
                                                                                  1.28
                                                                                                     93
                                                                                                                           .0038
                                                                                                                                       -2.42
                                                                                                                                                                 -1.74
61
                19
                                             .04
                                            .34
                                                                                                     13
                                                                                                                           .0882
                                                                                                                                                       .054
                                                                                                                                                                 -1.27
               21 6/10/91
                                                        64231
                                                                            22 1.34
                                                                                                                                       -1.05
62
                                                                                                                           .0565
                                                                                                                                       -1.25
                                                                                                                                                       .050
                                                                                                                                                                  -1.30
63
                22
                       6/12/91
                                             .40
                                                        82234
                                                                             11
                                                                                    1.04
                                                                                                     10
                      7/1/91
                                             .17
                                                         2051
                                                                             41
                                                                                    1.61
                                                                                                                           .0053
                                                                                                                                                       .035
                                                                                                                                                                  -1.46
                24
64
65
                                                                                                                                                             6
66
          Count
                                               6
                                                                              6
                                                                                                                           .0038
                                                                                                                                                       .018
67
          Minimun
                                             .04
                                                                             11
                                                                                                                            .0882
                                                                                                                                                        .054
                                             .40
                                                                             41
68
          Maximum
                                                                                                                           .0325
                                                                                                                                                       .034
                                             .20
                                                                             22
69
          Average
                                                                                                                                                       .014
70
          Stnd Dev
                                            . 13
                                                                              0
                                                                                                                           .0310
                                                                                                                              .95
                                                                                                                                                         .40
71
                                             .68
                                                                           .43
          COV
                                                                                                                            .0177
                                                                                                                                                        .031
                                                                             20
72
          Geo Mean
                                                                                                                           .1948
                                                                                                                                                       .205
 73
          Sum
```

2 3

5

7 8 9



### Appendix C

**Application Site Description Files and Results** 

Data file name: LILLYC.DAT Rain file name: RAIN81.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 01/01/81

Date: 12-12-1991

Fraction of each type of Drainage System serving study area:

1. Grass Swales .3

Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in:

Poor condition (or very flat) 0

4. Fair condition .7

5. Good condition (or very steep) 0

Site information: LILLY CREEK, MIXED LAND USES, SOURCE AREA LOADINGS FOR CALIB. Areas for each Source (acres)

Particulate Solids Concentration file name: MILW11.PSC

Pollutant Relative Concentration file name: MILW3.POL

Freeway Source Area

Large Turf Areas Undeveloped Areas Other Pervious Areas

Total

Paved Lane & Shoulder Area 1 Paved Lane & Shoulder Area 2 Paved Lane & Shoulder Area 3 Paved Lane & Shoulder Area 4 Paved Lane & Shoulder Area 5

Other Directly Connected Imperv Area Other Partially Connected Imperv Area

Area (

Study period ending date: 12/31/81

Time: 11:13:03

Source Area	Resi- dential Areas	Institu- tional Areas	Commercial Areas	Industrial Areas	Open Spaces Areas
Roofs 1	2.01	0.00	2.75	17.42	0.00
Roofs 2	5.29	0.00	0.37	0.98	0.00
Roofs 3	0.00	0.00	0.00	0.09	0.00
Roofs 4	0.00	0.00	0.00	0.00	0.00
Roofs 5	0.00	0.00	0.00	0.00	0.00
Paved Parking/Storage	0.09	0.00	5.47	24.60	0.00
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00
Unpaved Parking/Storag	0.09	0.00	0.20	3.88	0.00
Unpaved Parking/Storag	0.00	0.00	0.00	1.80	0.00
Playground 1	0.00	0.00	0.00	0.00	0.00
Playground 2	0.00	0.00	0.00	0.00	0.00
Driveways 1	2.01	0.00	0.25	1.63	0.00
Driveways 2	2.10	0.00	0.00	0.18	0.00
Driveways 3	0.00	0.00	0.00	0.14	0.00
Sidewalks/Walks 1	0.32	0.00	0.57	0.49	0.09
Sidewalks/Walks 2	0.32	0.00	0.00	0.49	0.09
Street Area 1	2.01	0.00	1.19	6.14	1.11
Street Area 2	3.83	0.00	1.50	1.50	0.00
Street Area 3	0.55	0.00	0.00	0.00	0.00
Lrg Lndscpd Area 1	0.00	0.00	0.00	2.49	0.18
Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00
Undeveloped Area	4.01	0.00	0.03	3.30	27.26
Smil Lndscpd Area 1	68.11	0.00	0.78	6.58	0.00
Smil Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00
Smll Lndscpd Area 3	0.00	0.00	0.00	0.00	0.00
Isolated Area	0.18	0.00	0.00	0.00	0.29
Other Pervious Area	0.27	0.00	0.25	2.26	0.18
Other Directly Connect	0.00	0.00	0.00	0.00	0.00
Other Partially Connec	0.00	0.00	0.00	0.00	0.00
Total	91.19	0.00	13.36	73.97	29.20
Total of All Source Area	2		207.72		

Total of All Source Areas

207.72

Total of All Source Areas less All Isolated Areas

207.25 ========

Source Area Control Practice Information

Residential Areas

Roofs 1 Source area number: 1

The roof is pitched

The Source Area is directly connected or draining to a directly conntected area

Roofs 2 Source area number: 2

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is low

Paved Parking/Storage 1 Source area number: 6

The Source Area is directly connected or draining to a directly connected area

Source area number: 9 Unpaved Parking/Storage 1

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is low

Driveways 1 Source area number: 13

The Source Area is directly connected or draining to a directly connected area

Driveways 2 Source area number: 14

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

```
The building density is low
  Sidewalks/Walks 1
                       Source area number: 16
        The Source Area is directly connected or draining to a directly connected area
  Sidewalks/Walks 2 Source area number: 17
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is C/D
        The building density is low
                   Source area number: 18
  Street Area 1
           1. Street Texture: smooth

    Total study area street length (curb-miles): 1.36
    Initial Street Dirt Loading (lbs/curb-mi): default value

           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 04/01/81
                                               Schedule: Every 12 weeks (Wed)
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Light
           4. Parking controls imposed? No
           5. Equation coefficient M (slope): .45
           6. Equation coefficient B (intercept): 125
                   Source area number: 19
  Street Area 2
           1. Street Texture: intermediate
           2. Total study area street length (curb-miles): 2.55

    Initial Street Dirt Loading (lbs/curb-mi): default value

           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 04/01/81
                                               Schedule: Every 12 weeks (Wed)
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Light
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept): 450
                  Source area number: 20
  Street Area 3
           1. Street Texture: rough
           2. Total study area street length (curb-miles): .18
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
               Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning

    Street cleaning schedule:

                                               Schedule: Every 12 weeks (Wed)
                Begin cleaning on: 04/01/81
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Light
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept):
  Undeveloped Area
                    Source area number: 23
         The SCS Hydrologic Soil Type is C/D
  Smll Lndscpd Area 1
                         Source area number: 24
         The SCS Hydrologic Soil Type is C/D
                         Source area number: 28
  Other Pervious Area
        The SCS Hydrologic Soil Type is C/D
Commercial Areas
  Roofs 1
             Source area number: 61
         The roof is flat
         The Source Area is directly connected or draining to a directly conntected area
            Source area number: 62
         The roof is pitched
         The Source Area is directly connected or draining to a directly conntected area
                             Source area number: 66
  Paved Parking/Storage 1
         The Source Area is directly connected or draining to a directly conntected area
  Unpaved Parking/Storage 1
                               Source area number: 69
         The Source Area is draining to a pervious area (partially connected impervious area)
         The SCS Hydrologic Soil Type is C/D
  Driveways 1 Source area number: 73
        The Source Area is directly connected or draining to a directly conntected area
  Sidewalks/Walks 1
                     Source area number: 76
         The Source Area is directly connected or draining to a directly conntected area
                   Source area number: 78
   Street Area 1
           1. Street Texture: smooth
           2. Total study area street length (curb-miles): .47
           Initial Street Dirt Loading (lbs/curb-mi): default value
```

4. Street Dirt Accumulation:

616614.21

```
Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                                              Schedule: Every 12 weeks (Wed)
                Begin cleaning on: 04/01/81
               Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Medium
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept): 70
                Source area number: 79
  Street Area 2
           1. Street Texture: smooth
          2. Total study area street length (curb-miles): .58
              Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                                               Schedule: Every 12 weeks (Wed)
                Begin cleaning on: 04/01/81
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Medium
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept):
                      Source area number: 83
  Undeveloped Area
        The SCS Hydrologic Soil Type is C/D
                       Source area number: 84
  Smil Lndscpd Area 1
        The SCS Hydrologic Soil Type is C/D
                        Source area number: 88
  Other Pervious Area
        The SCS Hydrologic Soil Type is C/D
Industrial Areas
  Roofs 1
             Source area number: 91
        The roof is flat
        The Source Area is directly connected or draining to a directly conntected area
             Source area number: 92
  Roofs 2
        The roof is flat
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is C/D
        The building density is low
             Source area number: 93
        The roof is flat
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is C/D
        The building density is medium or high
        Alleys are not present
                             Source area number: 96
  Paved Parking/Storage 1
        The Source Area is directly connected or draining to a directly conntected area
                               Source area number: 99
  Unpaved Parking/Storage 1
         The Source Area is draining to a pervious area (partially connected impervious area)
         The SCS Hydrologic Soil Type is C/D
        The building density is low
                               Source area number: 100
   Unpaved Parking/Storage 2
         The Source Area is draining to a pervious area (partially connected impervious area)
         The SCS Hydrologic Soil Type is C/D.
         The building density is medium or high
         Alleys are not present
   Driveways 1
                Source area number: 103
        The Source Area is directly connected or draining to a directly conntected area
                 Source area number: 104
   Driveways 2
         The Source Area is draining to a pervious area (partially connected impervious area)
         The SCS Hydrologic Soil Type is C/D
         The building density is low
   Driveways 3
                Source area number: 105
         The Source Area is draining to a pervious area (partially connected impervious area)
         The SCS Hydrologic Soil Type is C/D
         The building density is medium or high
         Alleys are not present
   Sidewalks/Walks 1
                      Source area number: 106
         The Source Area is directly connected or draining to a directly conntected area
   Sidewalks/Walks 2 Source area number: 107
         The Source Area is draining to a pervious area (partially connected impervious area)
         The SCS Hydrologic Soil Type is C/D
         The building density is low
                    Source area number: 108
   Street Area 1
            1. Street Texture: intermediate
            2. Total study area street length (curb-miles): 2.9

    Initial Street Dirt Loading (lbs/curb-mi): default value
    Street Dirt Accumulation:
```

```
Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 04/01/81
                                              Schedule: Every 12 weeks (Wed)
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Medium
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept): 220
  Street Area 2 Source area number: 109
           1. Street Texture: smooth
           2. Total study area street length (curb-miles): .62
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
              Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 04/01/81
                                               Schedule: Every 12 weeks (Wed)
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Medium
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept):
                       Source area number:
  Lrg Lndscpd Area 1
  The SCS Hydrologic Soil Type is C/D
Undeveloped Area Source area number: 113
        The SCS Hydrologic Soil Type is C/D
  Smil Lndscpd Area 1
                        Source area number: 114
        The SCS Hydrologic Soil Type is C/D
                       Source area number: 118
  Other Pervious Area
        The SCS Hydrologic Soil Type is C/D
Open Space Areas
   Sidewalks/Walks 1
                      Source area number: 136
        The Source Area is directly connected or draining to a directly connected area
   Sidewalks/Walks 2 Source area number: 137
        The Source Area is draining to a pervious area (partially connected impervious area)
        The SCS Hydrologic Soil Type is C/D
   Street Area 1
                   Source area number: 138
           1. Street Texture: smooth
           Total study area street length (curb-miles): .67
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 04/01/81
                                               Schedule: Every 12 weeks (Wed)
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Light
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           Equation coefficient B (intercept):
   Lrg Lndscpd Area 1
                       Source area number:
        The SCS Hydrologic Soil Type is C/D
   Undeveloped Area Source area number: 143
        The SCS Hydrologic Soil Type is C/D
                        Source area number: 148
   Other Pervious Area
        The SCS Hydrologic Soil Type is C/D
Catchbasin or Drainage Controls
     Control Practice 1: Grass Swale
        1. Swale infiltration rate (inches per hour)= .25
        2. Swale density (feet per acre)=
        3. Wetted swale width (feet)= 3
        4. Area served by swales (acres)= 62.175
```

### Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name Pollutant Type
Residue Particulate

717717

Pala Files LULICC.BAT Rain Files Rathril.Rah Dates 12-22-1991 Times 23:03:53 Site description: LULY CREEF, MIKED LAND USES, SOURCE AREA LOADINGS FOR CALIF.

Residential Areas - Runoff Voluse (cu. ft)

Calculated	93.7	4 60				
Total Lesses (in.) 4	9.63		=	6.3		
&	0.63		3	0.73		
Land Use Potals	781	10001	11117	32613	2479578	
Ether Fervious Area	-		-	\$	\$243	
Undevel- Saall ( oped Area Ladscaped fr Area Area l A	•		70411	17401	1322466	
Undevel- oped Area Area	<	• 35.	26.73	1024	77862	
Street Area 3	•	•	9000	524	39797	
Street Area 2	<b>.</b>	2 6	200	3673	171175	
Street Area 1	2	? ;	11/20	2092	158203	
idenalks Sidenalks Talks I /Halks I	•	- :	33	<b>æ</b>	6213	
Sidenalks Walks 1	=	2 ;	202	4	31656	
brive-	4	•	3339	33	40776	
Drive- nays 1	3	3	12783	2616	198839	
Uppaved Farking/ Storage 8	•	-	125	2	1748	
Paved Farking/ Storage 1		- ;	22	113	8903	
Roofs 2	Events	•	9168	1352	102716	
Roofs 1 Roofs	Producing	<b>~</b>	13323	2897	204980	
Rain Total (inches)	or Arnoff	6.63	 3:	9.4	30.38	
Start Rain Roofs 1 Roofs 2 Date Total (inches)	Senary t		Hazi bung	Average	Tele!	

Consercial Areas - Runoff Volune (cu. ft)

v	
Calculated CN	4.8 4.8 4.8
Losses (in.) 1	0.25
2 3	0.75
Land Use Totals	347 77655 14980 1138499
Other Pervious Area	421 64 64 6854
Seall Lndscaped Area 1	1315
Undevel- Seall Other oped Area Undscaped Pervious Area Area I Area	° 7 ° E
	.44 8773 1553 118062
Street Area 1	35 6960 1232 93662
Sideualks Street Walks 1 Area 1	24 3625 742 56307
45 30	1590 325 24731
Unpaved Parking/ Storage 1	111 165 12531
Paved Parking/ Storage 1	227 34787 7128 \$41120
Roofs 2 Events	2452 494 37733
	16510 3675 233681
Rain Jotal (inches) or Runoff P	30.45
Start Date Sunary f	Minimus Parimus Averages Totals

Industrial Areas - Runoff Yoluve (cu. ft)

and Kv Totai Calculated ie Losses CN ils (in.) t	6.16 0.03 94.8 0.71 0.53 99.4 1 0.63 0.15
Olher Land Pervious Use Area Totals	0 1285 3809 354550 577 67234 13822 5109770
Undevel- Spall Oli d oped Area Lndscaped Per Area Area 1 Are	0 11090 1681 127763
Undevel- id oped Area Area	5552 843 64076
targe Indscaped Area I	4197 636 48548
Street Area 2	44 8773 1553 118062
Sidewalks Sidewalks Street Walks I / Walks 2 Area I	0 132 826 34139 125 5889 9514 447558
Sidenalks Walks 1	3116 538 638 48473
Brive- nays 3	232 2822
Drive- nays 2	303 345 345
brive- nays 1	68 10366 2122 161248
Unpaved Parking/ 1 Storage	
Unpaved Parking/ 1 Storage	6539 1991 75538
Paved Parking/ Storage	1021 15644 32020 243357
Roofs 3	141 20 1505
Roofs 2	Events 0 1652 250 19029
Roofs 1	Suaaary for Renoff Producing Events Ninisua: 0.03 0 0 Nations: 1.85 104381 1652 Average: 0.40 15427 230 19421: 30.36 1480263 19029
Rain Total (inches)	for Reneft 0.03 1.85 0.46 30.36
Start	Susary Minious: Mariaus: Average: Total:

in Space Areas - Runoff Volune (cu. ft)

Rain	Rain Sidenalks	Sidenalks Sidenalks Street	Street	Large	Jadeve]-	Olher O	2	2	55 .	Calculated	•
3	Valks 1	/Walks ?	Area 1	Ludscaped	oped Area	Pervious	25		Losses	3	
(inch	<u>33</u>			Area 1	125	Å723	Totals		(in.)		
for Run.	off Producing	Events									
0.0	-	-	ë	•	-	-	*	9.0		91.0	
	5 572		6492	303	45944	303	53767	0.38	.3	98.8	
Average: 0.4(	(11)	2	22	<b>%</b>	\$969	7	8346	0.30			
30.3	6 8903		87366	3495	529305	3495	634312				

Start Rain Total Total Controls - Runoff Volume (cu. ft)

Start Rain Total Total Catch- Total Rv Total Calculatd Peak Flushing Detention Basin
bate Total Without With basin With Losses CK Reduction Ratio Outlet Structure
(inches) Prainage Prainage Volume Outfall (in) 8 Factor Factor
Controls Controls 2 Fall Controls
Summary for Runoff Producing Events
Wanher of Runoff Producing Events
we have a famouf Producing Events

Sussary for Renoff Producing Events

Namber of Ranoff Producing Events

using Rains: 7 A 76 76 76 76 76 76 76 89.4

Minimus 0.03 1959 1371 0.0 1371 0.06 0.03 89.4

Mainmus 1.85 685946 662242 0.0 652242 0.48 0.97 99.2

Average: 0.49 123173 120007 0.0 120007 0.40 0.24

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events	
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Ξ	Events										į		: :	:
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	ä	<b>E</b>	\$	378	7.7	2	2	3938	12209	3555	250	13	128	2256
	~	2	395	3	2	드	27	124	#	23	520		22	133

## Concercial Areas - Concentration of PARTICULATE RESIBUE (Ag/L)

per)	use Totals		126	6219	*
Other	Pervious Area		95	520	230
Seall	oped Area Lnoscapes Area Area i		300	300	200
Undevel-	oped Area		600	3274	787
Street	Ares 2		302	32513	1881
s Street	1 2 1		308	33210	1717
Sidenelks	Valks 1		**	z	23
Prive-	4375			2	138
Unpaved	Parking/ Storage 1		69	2584	807
Paved	Parking/ Storage 1		£	8191	153
Roofs 2		Events	~	٠.,	·
Roofs 1		Producing	-	<b>.</b>	<b>-</b>
Rain	Total (inches)	or Runoff	0.03	.83	9.49
Start	=======================================	Successy 4	Minister.	Hari eus:	fl H Ave:

## Industrial Areas - Concentration of PARTICULATE RESIDUE (49/L)

Start .	lain Otal inches)	Roofs 1	Roofs 2	Reofs 3	Paved Parking/ Storage 1	Unpaved U Parking/ P	nooved arking/ torage 2	Drive- nays l	Brive- uays 2	Brive- Hays 3	Sidewalks Sidewalks Street Walks I /Walks 2 Arez 1	Sidewalks i		Street Area 2	large Indsciped Area i	Large Undevel- E Indscrped oped Area L Area i Area A	Seall Ledscape Frea 1	Other id Pervious Area	iand USP Potris
Minimum 0.03 S S S S S Mariuma 1.88 S S S S S S S S S S S S S S S S S S	5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	# S S S S S S S S S S S S S S S S S S S	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	***	95 1618 163	300	300 1492 389	238	149	00 1	001 065 108	9 6 6 9	382 53338 2297	323 34785 1796	300 300 300	222	900	888	124 7851 347

# Open Space Areas - Concentration of PARTICULATE RESIDUE (ag/L)

Undevel- Other	ed oped Area Fervious Use	Area Area		500 250	500 250 7149	250
					300	
Street	Area 1				1872	
Sidenalks	/Balks 2		Events	2	2	
Sidewalks	ialks i		Producing	8	2	3
=======================================	Total	(inches)	r Rusoff	0.03	 8:	9
	ž		Sussary fo	Hiniaun:	Kariaum	F1 Mt Ave:

Total Area, with Drainage and Guffall Controls - Concentration of FARTICULATE RESIDUE (mg/L)

Start Rain Total Total Catch Total Flow-utd

Date Total Without With bessp With Min. Part.

(inches) Drainage Drainage Volume Outfall Size

Controls Controls Controls 2 Full Controlled

Susaary for Runoff Producing Events

Minimus: 0.03 Mediabs: 1.95 Fl W Ave: 0.40

### Residential Areas - Yield of PARTICULATE RESIDUE (16s)

9.00	Jse	otals		×	9
	_	2			916
O!her	Pervious	Area		~	-
Seall	Lndscaped	krea 1		•	105 (5)
Undevel-	oped Area Indscaped Pervious	Area		•	193
Street Undevel- Seall Other	Area 3			~	<u>ب</u>
Street	Area 2			r,	961
Street	Area 1			~	፷
Sidewalks	/Walks 2 Area 1			•	0
Sidenalks Sidenalks Street	Falks 1			•	~
Prive-	usys 2			<b>-</b>	:: ::
Prive-	ways 1 . ways 2			-	¥
Unpaved	Parking/ Parking/ ways 1	Storage 1		•	-
Paved	Parking/	Storage 1 S		•	~-
Roofs 2			Events	•	۲.
Roofs &			roducing	•	9
Rain	lotal	(inches)	r Runoff P	9.03	 S
Start	P.te		Susaary for Runoff Producing	Hinion:	Hariene:
		1			

Consercial Areas - Yield of FARTICYLATE KESIDUE (185)

9 11 200 24 2 2 2 3 63 63 63 63 63 63 63 63 63 63 63 63 6	61 247 185			
200 247 2 25 7 625 10029 12576 _ 29 283	247 185 12376	•	•	0 0 81
Land Bise  Both  B	12378	= ~	- m	* 22
Drive- Drive- Side-aalks Sidemaalks Street Street  1 uays 2 uays 3 Walks 1 (Maiks 2 Area 1 Area 2  1 0 0 0 301 65  65 2 1 1 9 2 923 199  1051 22 16 316 59 61625 13230  1470  6 1470  6 16415  6 1470  6 1655  1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		2	213	213
Land				(94)
Land Use 19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Drive- Drive- ways 1 ways 2	paved rking/ brage	Unpaved Un Farking/ Fa Storage 1 St	Paved Unpaved Unpaved Parking/ Farking/ Storage 1 Storage 1 Storage 2
Land Land Use lotals  65 2 1 19 5 1236 234 79 193  1051 22 16 316 59 61625 13230 965 1199 2391  1470 676 198737  (1b5)	. 0	•	•	ę.
Land Use 1 1 1 7 5 1525 965 1798 2391 1875 16415	1 2 59	25	122	
		909	54 2338	458 54 24772 2338
			,	(185)
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	lotais	2	Area Ar	
- =	8 1470	~ ~	0 22.81	0 0
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	18757	s	16509	65 16509
		31015	ARTICULATE SE	rial Area, with Brainage and Cuttell Controls - Yield of PARTICULATE RESIBUE
			Flow-std Nis. Part.	lotal Flou-std with Min. Part.
			Size	= :
		,	משנג פו זהפ	CORTFOLS CONTROLLED
				7,4
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				2598

Land Bsé Totals 148 2736 1946

Residential Areas - Concentration of 1618, COPPER inicrograms (1)

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Areas	
Consercial A	

Start	Rain Total (inches)	Reefs 1 K	. see s	aved Perking/ Storage 1	Unpaved Parking/ Storage 1	Drive- nays i	Sideralks :	Area 1	Area ?	unoeve:- oped Arca Area	Indscaped Area 1	Pervious Area	iee Jee Jelals		•				
itus: iies: Il Ave:		0.000 0.000 0.007 0.003 0.096	6.000 0.001 0.001 0.001 0.016	9.092 9.027 9.013	9.000 0.010 0.005	0.000 0.001 0.001 0.003	6.000 0.001 0.001	0.003 0.015 0.012 0.749	0.004 0.018 0.015 0.925	0.000 0.000 0.000	0.000	0.000 0.000 0.000 0.000	0.009 0.077 0.049 2.592						
órstria	l Areas -	Yield of 1	Industrial Areas - Yield of 1814L COPFER	(185)									٠						
Start	Rain Total (inches)	Roofs 1	? sjos	Koofs 3	Faved Facking/ Storage 1	Unpaved Parking/ Sterage 1	Unpaved Parking/ Storage 2	Prive-	Drive-	Prive-	Sidenalki Halks I	Sidenalks Sidenalks Street Walks I /Walks 2 Area I	Street Area 1	Street Area 2	Large Laúscaped Area 1	Undevel- Small O d oped Area Endscaped P Area Area 1 A	Snall Indscaped Area 1	Other Fervious Grea	
tues.	or Runoff	Preducing	Events	:		•	400		900	0.00	0.00	0.00	0.019	0.094	9.000	000.0	0.000	0.000	
Hinious: Harines:	2.8	iteue: 0.03 0.000	0.000	0.000	0.202	9.013	0.000	0.038	0.00	6.6	0.017	0.005	0.00	0.021	0.003	6.639	0.907	706.0	
H. We	0.40	9.007	000.6	9.00	0.094	0.00	0.003	0.304	0.000	0.000	6.603	0.00	0.070	9.916	9.6	6.018	0.405	0.003	_
17	30.36	0.233	0.003	0.000	3.764	9.211	6,063	0.137	6.003	0.003	0.277	0.023	4.0.7	9.700	. D. D	7.44	600.0	200.4	_

6.927 6.431 9.234 16.362

1111	e i	Sidenalks	Sidewalks	Street		Undevel-	Other	, es
	Total (inches)	_	•	Area L	Ladscaped Area 1	bed area	Fervious Area	USE Totals
Sanary for	Runoff	-	Events					
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Tarina.	.83		0.00	6.019	0.00	0.10	000.0	6.115
F) Wt Ave:	9.	9.000	0.000	0.012	0.00	9.047	0.000	0.039
lotali	30.34		0.005	0.778	0.003	1.205	0.003	1.003

Data file name: LILLYG.DAT Rain file name: RAIN81.RAN

Runoff Coefficient file name: MILW6.RSV

Particulate Residue Delivery file name: DELIV2.PRR

Study period starting date: 01/01/81

Study period ending date: 12/31/81 Time: 11:14:18 Date: 12-12-1991

Fraction of each type of Drainage System serving study area:

1. Grass Swales .3

2. Undeveloped roadside 0

Curb and Gutters, 'valleys', or sealed swales in: 3. Poor condition (or very flat) 0

Fair condition .7
 Good condition (or very steep) 0

Site information: LILLY CREEK, LOW DENSITY RES., SOURCE LOADINGS FOR MODEL CALIB.

Areas for each Source (acres)

Source Area	Resi- dential Areas	Institu- tional Areas	Cómmercial Areas	Industrial Areas	Open Spaces Areas	Freeway Source Area	Area
Roofs 1	1.43	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 1	
Roofs 2	3.77	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 2	
Roofs 3	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 3	
Roofs 4	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 4	
Roofs 5	0.00	0.00	0.00	0.00	0.00	Paved Lane & Shoulder Area 5	
Paved Parking/Storage	0.06	0.00	0.00	0.00	0.00	Large Turf Areas	
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Undeveloped Areas	
Paved Parking/Storage	0.00	0.00	0.00	0.00	0.00	Other Pervious Areas	
Unpaved Parking/Storag	0.06	0.00	0.00	0.00	0.00	Other Directly Connected Imperv Area	i
Unpaved Parking/Storag	0.00	0.00	0.00	0.00	0.00	Other Partially Connected Imperv Are	a
Playground 1	0.00	0.00	0.00	0.00	0.00		
Playground 2	0.00	0.00	0.00	0.00	0.00	Total	
Driveways 1	1.50	0.00	0.00	0.00	0.00	•	
Driveways 2	1.43	0.00	0.00	0.00	0.00		
Driveways 3	0.00	0.00	0.00	0.00	0.00		
Sidewalks/Walks 1	0.23	0.00	0.00	0.00	0.01		
Sidewalks/Walks 2	0.23	0.00	0.00	0.00	0.01		
Street Area 1	1.43	0.00	0.00	0.00	0.08		
Street Area 2	2.73	0.00	0.00	0.00	0.00		
Street Area 3	0.39	0.00	0.00	0.00	0.00	•	
Lrg Lndscpd Area 1	0.00	0.00	0.00	0.00	0.01		
Lrg Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00		
Undeveloped Area	2.86	0.00	0.00	0.00	1.87		
Smil Lndscpd Area 1	48.56	0.00	0.00	0.00	0.00		•
Smll Lndscpd Area 2	0.00	0.00	0.00	0.00	0.00		
Smil Lndscpd Area 3	0.00	0.00	0.00	0.00	0.00	•	
Isolated Area	0.13	0.00	0.00	0.00	0.02	•	
Other Pervious Area	0.20	0.00	0.00	0.00	0.01		
Other Directly Connect	0.00	0.00	0.00	0.00	0.00		
Other Partially Connec	0.00	0.00	0.00	0.00	0.00		
Total	65.02	0.00	0.00	0.00	2.00		,

Particulate Solids Concentration file name: MILW11.PSC

Pollutant Relative Concentration file name: MILW3.POL

Total of All Source Areas

67.02

Total of All Source Areas

less All Isolated Areas

66.87

### Source Area Control Practice Information

Residential Areas

Roofs 1 Source area number: 1

The roof is pitched

The Source Area is directly connected or draining to a directly connected area

Roofs 2 Source area number: 2

The roof is pitched

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is low

Paved Parking/Storage 1 Source area number: 6

The Source Area is directly connected or draining to a directly connected area

Source area number: 9 Unpaved Parking/Storage 1

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is low

Driveways 1 Source area number: 13

The Source Area is draining to a pervious area (partially connected impervious area)

The SCS Hydrologic Soil Type is C/D

The building density is low

Driveways 2 Source area number: 14

```
The Source Area is directly connected or draining to a directly conntected area
                      Source area number: 16
 Sidewalks/Walks 1
       The Source Area is directly connected or draining to a directly conntected area
 Sidewalks/Walks 2 Source area number: 17
       The Source Area is draining to a pervious area (partially connected impervious area)
       The SCS Hydrologic Soil Type is C/D
       The building density is low
                  Source area number: 18
 Street Area 1

    Street Texture: smooth
    Total study area street length (curb-miles): .98

          Initial Street Dirt Loading (lbs/curb-mi): default value
          4. Street Dirt Accumulation:
                Default value used
    Control Practice: Street Cleaning
           1. Street cleaning schedule:
                                               Schedule: Every 12 weeks (Wed)
                Begin cleaning on: 04/01/81
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Light
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept): 125
                 Source area number: 19
  Street Area 2
           1. Street Texture: intermediate

    Total study area street length (curb-miles): 1.82
    Initial Street Dirt Loading (lbs/curb-mi): default value

           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                                               Schedule: Every 12 weeks (Wed)
                Begin cleaning on: 04/01/81
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Light
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept):
  Street Area 3
                 Source area number: 20
           1. Street Texture: rough
           Total study area street length (curb-miles): .13
           3. Initial Street Dirt Loading (lbs/curb-mi): default value
           4. Street Dirt Accumulation:
                 Default value used
     Control Practice: Street Cleaning
           1. Street cleaning schedule:
                Begin cleaning on: 04/01/81
                                               Schedule: Every 12 weeks (Wed)
                Final cleaning period ending date: 10/30/81
           2. Street cleaner productivity: Default
           3. Parking density: Light
           4. Parking controls imposed? No
           5. Equation coefficient M (slope):
           6. Equation coefficient B (intercept):
                                                     450
                     Source area number: 23
  Undeveloped Area
         The SCS Hydrologic Soil Type is C/D
   Smil Lndscpd Area 1
                       Source area number: 24
        The SCS Hydrologic Soil Type is C/D
                         Source area number: 28
   Other Pervious Area
         The SCS Hydrologic Soil Type is C/D
Open Space Areas
                       Source area number: 136
   Sidewalks/Walks 1
         The Source Area is directly connected or draining to a directly conntected area
   Sidewalks/Walks 2 Source area number: 137
         The Source Area is draining to a pervious area (partially connected impervious area)
         The SCS Hydrologic Soil Type is C/D
                   Source area number: 138
   Street Area 1
            1. Street Texture: smooth
            2. Total study area street length (curb-miles): .05
            3. Initial Street Dirt Loading (lbs/curb-mi): default value
            4. Street Dirt Accumulation:
                  Default value used
      Control Practice: Street Cleaning
            1. Street cleaning schedule:
                                               Schedule: Every 12 weeks (Wed)
                 Begin cleaning on: 04/01/81
                 Final cleaning period ending date: 10/30/81
            2. Street cleaner productivity: Default
            3. Parking density: Light
            4. Parking controls imposed? No
            5. Equation coefficient M (slope):
```

6. Equation coefficient B (intercept): 125

Source area number: 141 Lrg Lndscpd Area 1 The SCS Hydrologic Soil Type is C/D Undeveloped Area Source area number: 143 The SCS Hydrologic Soil Type is C/D
Other Pervious Area Source area number: 148
The SCS Hydrologic Soil Type is C/D

- Catchbasin or Drainage Controls
  Control Practice 1: Grass Swale
  1. Swale infiltration rate (inches per hour)= .25
  2. Swale density (feet per acre)= 160
  3. Wetted swale width (feet)= 3
  4. Area served by swales (acres)= 20.0616

### Outfall Controls

Pollutants to be Analyzed and Printed:

Pollutant Name

Pollutant Type

Residue

Particulate

Data File: LILLFG.DAT Rain File: Rathal.Rah Date: 12-22-1991 - Time: 23:20:39 Site description: LILLY CREEK, ION DENSITY RES., SOURCE LOADINGS FOR MODEL CALID.

lesidential Areas - Runoff Volune (cu. ft)

0.03 0.33 0.25 207 142539 23245 1766602 Undevel- Stall Other oped Area Ludscaped Fervious Area Area I Area 81843 12406 942386 Street Area 3 2168 371 28220 Street Area 2 Sidewalks Sidewalks Street Walks 1 / Walks 2 Area 1 42 8364 1481 112552 16453 299 22753 Pared Unpared Brive- Brive-Parking/ Parking/ usys 1 usys 2 Storage 1, Storage 1 2528 383 29125 Asin Rob.

16 1041

(inches)
Sunary for Rupoff Producing Events

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41,1001

6,40

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73202 . i s s s

Calculated CN

Tetal Losses (in.) 4

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Open Space Areas - Runoft Volune (cu. fl)

3

Start	Rain Total (inches)	Sidewalks Walks 1	Sidevalks /Valks 2	Streel Area 1	Large Ladscaped Area 1	Undevel- oped Area Area	Other Pervious Area	Land Use Totals	<b>a</b> .	Total Losses (in.) t	Calculated CN	
arry to	r Runoff	Producing	Evenis						;			
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	2	*	=	<b>89</b>	1	3125	=	3262	<b>6.</b> 28	<u></u>	8.8	
3	9	_	~	=	;	24	~	\$15	<b>6</b> .20			
Totals	30.34	36	Ξ	(629)	161	36310	6	43705				

Detention Basin Outlet Structure Failed (land use D-source area A) Calculatd Peak Flushing
CM Reduction Ratio
Factor Total Losses (in) # Total Area, with Brainage and Detfall Controls - Runoff Volume (co. ft) Start Rain Total Folial File. Hith Outfall Controls Rain Total fotal Catch-Total Without With basin (inches) Prainage Prainage Volume Controls Controls 2 Full Sunnery for Runoff Producing Events

Maber of Runoff Prod-

4 Total losses are sumarized for all events, not for runoff producing events alone.

Residential Areas - Concentration of PARTICULATE RESIDUE (19/L)

Land Use Totals 5455 138 Undevel- Shall bither oped Area Lndscaped Pervious Area Area I Area ಜ ಜ ಜ 222 Street Area 3 3521 126 126 Street Area 2 86 12225 481 Sidemalks Sidemalks Street Walks 1 /Walks 2 Area 1 55 EFF Prive-57 276 87 Paved Unpaved Brive-Parking/ Parking/ ways 1 Storage 1 Storage 1 2 2 2 373 440 395 2 2 8 Roofs 1 Roofs 2 === (inches) Sweary for Runoff Producing Events 6 21 2 21 . Minista: 0.03 Nationa: 1.85 Fl Mt Ave: 0.40

(1/b) gen Space Areas - Concentration of PARTICULATE RESIDUE

Land Use Totals 3 5 5 Sidewalks Sidewalks Street Large Undevel- Other Walks I /Walks 2 Area I Indscaped oped Area Pervious Area I Area Area 8255 394 Start Rain Sidewalks Sidewalks
Date Total Walks I /Walks 2
(Inches)
Susaary for Rusoff Producing Events Riniana: 0.03 Kariana: 1.85 Fl Mt Ave: 0.40

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	(inches)	Prainage	Drainage	207		5:2		•								
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ž	Total (inches)			Parking/ Storage 1	Parking/ Storage 1	l stem	mays 2	Halks i	/Walks 2 Area 1	Area 1	Area 2	Area 3	oped Area	oped Area Indscaped Pervious Grea	Pervious	lise Totale
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                                                                                                                                                                              Residential Areas - Yield of TOTAL COPPER (16s)
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Walks 1 /Walks 2 Area 1
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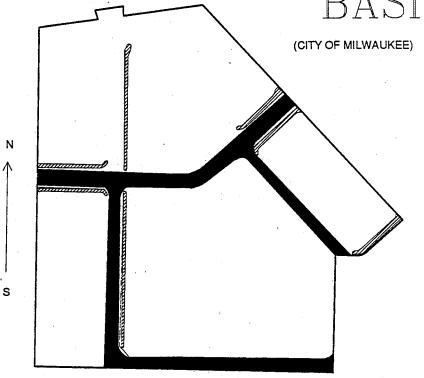
Appendix D

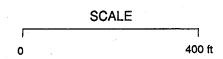
Digitized Site Area Maps

These maps were created by the U.S. Geological Survey for inclusion in this report. They are intended to qualitatively illustrate the general layout of each study area. The Monroe Street study area was not available when this report was prepared.

[mad-603-34g]

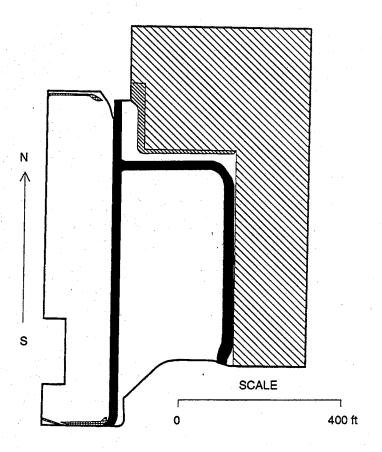
### POSTOFFICE BASIN



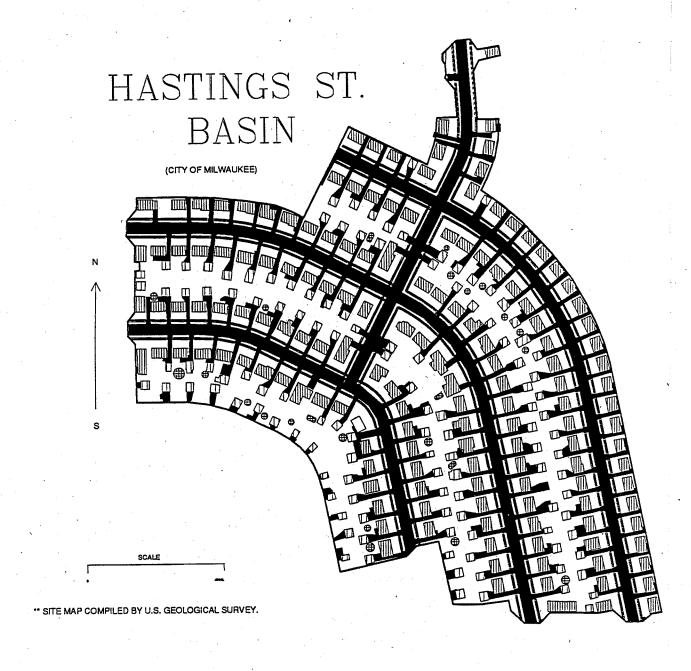


\*\* SITE MAP COMPILED BY U.S. GEOLOGICAL SURVEY.

### RUSTLER BASIN



\*\* SITE MAP COMPILED BY U.S. GEOLOGICAL SURVEY.



# SCALE CITY OF MILWAUKEE)

\*\* SITE MAP COMPILED BY U.S. GEOLOGICAL SURVEY.

